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**CUSTOMER DEDICATED FACILITIES AND INVENTORY SHARING IN  
INTEGRATED NETWORK DESIGN AND INVENTORY OPTIMIZATION**

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by

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# **CUSTOMER DEDICATED FACILITIES AND INVENTORY SHARING IN INTEGRATED NETWORK DESIGN AND INVENTORY OPTIMIZATION**

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Shrinking profit margins in the high technology industry has led companies to attempt to increase profits through an increased focus on after-market services. As part of that effort, service parts logistics, which manages the post-sales distribution of spare parts needed to maintain and repair products in use, has gained importance. In an effort to improve Service Parts Logistics (SPL) operations, we integrate facility location and inventory stocking decisions while classifying facilities based on their assignment; dedicated facilities that are assigned solely to individual customers (located on-site of the customer, serving only that customer), and shared facilities that are assigned to a subset of customers.

The introduction of dedicated facilities simplifies the overall problem formulation in certain special cases. In one such special case where there is only one facility and none of the customers are within its service time window, the overall problem reduces to a binary knapsack formulation. This can be solved in pseudo-polynomial time through the

dynamic programming algorithm for such problems. Nonetheless, even in the general case, we identify conditions under which a dedicated facility will always be opened. Computational results show that this observation is used by solvers as a preprocessing step, thus loosening some hard constraints. As a result, some of these problems are solved in less time than the corresponding problems without the dedicated facilities. However, dedicated facilities become advantageous mainly in sparse networks as opposed to dense networks. Apart from low network density, low holding cost and relatively high demand are two other system parameters that encourage the opening of dedicated facilities.

SPL can be further improved by sharing inventory across shared facilities, which is already a common practice in real SPL systems. In this case, Markov chains can be used to estimate fill rates, but the process is iterative. However, under the low demand assumption of parts in SPL, we derive analytical formulae of estimating fill rates and thus incorporate inventory sharing within the network design and inventory optimization model. Special cases of this problem can be solved by an alternative binary knapsack formulation. Computational results show that large instances can be solved instantaneously, and we also identify a greedy heuristic that provides bounds on average within 0.12% of the optimal solution. We observe maximum benefit from inventory sharing when there exists large demand in the area overlapping the time window of both shared facilities and when inventory replenishment rates are high. However, we also identify conditions on the system parameters where inventory sharing could increase cost and/or decrease service in comparison with not-sharing.

The combined problem of inventory sharing with customer dedicated facilities is formulated based on a binary knapsack structure. However, the problem size increases exponentially with solution time. Therefore, we construct another greedy heuristic by combining the inventory sharing heuristic and a special case algorithm for a single dedicated facility. A large size problem that takes almost a minute to be solved by

conventional branch and bound is solved in less than a second using the greedy heuristic. We also show that for a given demand network, the combined problem achieves 40-60% reduction in total cost within 1% of the time taken by the problem without inventory sharing and without dedicated facilities. Another interesting result is that in some cases, adding new customers to a given inventory sharing system helps to reduce the cost and/or increase service.

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## **Chapter 1: Introduction**

Responding to pressures from competition to keep shrinking profit margins under control is a major effort in any industry today, but it is especially true in the high technology industry. The high-tech manufacturers experiencing diminishing profit margins from product sales emphasize after-sales service as one area to increase revenues and profits, keep existing customers loyal and attract new customers who may have experienced service problems with other manufacturers.

In a survey study, the Aberdeen group (2005) reported that profit margins for aftermarket service and parts range from 25% to 1000% higher than margins for initial products. In this study, three quarters of the companies recognized that effective service parts logistics (SPL) is critical to the company's success. This study also reported that the SPL software application market accounted for approximately \$105 million in 2005 with a growth rate of 20%.

Even from a profit point of view, the supply of aftermarket parts is a \$400 billion business, and many of the Fortune 100 companies rely on the aftermarket service for up to 40% of their profits (Gallagher et al. (2005)). Another research study indicated that customers will spend five to 20 times the initial sales price on subsequent services and consumables (AMR Research (2002)).

The Aberdeen group (2005) also identified six primary areas affected by SPL:

- i. Service parts planning
- ii. Service parts forecasting
- iii. Inventory management
- iv. Service parts pricing
- v. Service contract management/design
- vi. Service parts execution and analytics

In this dissertation, we approach SPL from a strategic point of view by primarily focusing on the first and third application areas, i.e., service parts planning and inventory management, respectively, not only because of the costs savings potential, but also the inherent interaction between these areas in SPL systems, which motivates our integrated approach at the two areas. In SPL systems, the customers do not worry about where a needed part is supplied from or whether the part is available at a specific location or not. The main concern is to have the customer's system up and running with the proper part within a short time window, usually measured in hours. Hence, as long as the company is able to deliver the part within the time window spelled out in the customer service contracts, service is deemed to be good. This is where the two areas of network planning and inventory stocking interact: The network must have at least one stocking location close to the customer (within the time window) and one of the locations must have at least one unit of the needed part.

Hence, the *location* of the service facilities is crucial in SPL planning as well as in determining the inventory levels. With fewer locations, the company could take advantage of inventory pooling, but the service level would go down because it would be harder to reach customers within the committed time windows. Therefore we will focus on an integrated network design and inventory optimization model in Chapter 2. Previous models have had only one type of facilities, called "shared": all stocking locations in the network serve more than one customer and the stock level available at the location can be used to satisfy the demand of all customers that are assigned to that location. In our model, we allow more than one type of facility, "dedicated" along with shared facilities: Dedicated facilities in fact represent stocking locations at customer sites. The stock available at a dedicated facility can only be used to serve demand from the respective customer on-site. As actual SPL systems already have stocking rooms co-located at select customer sites, this extension of the original models is more consistent from a practical point of view.

Another common practice in SPL is inventory sharing among close-by neighboring stocking locations. This is especially true when the main location responsible from satisfying a certain customer is out of stock and another facility close enough to the customer to be within the time window has the part in stock. This way, time-based service does not have to suffer due to unavailability of the stock at the main location. The overall effect of this is potential reduction in the system-wide inventory levels to provide a given target time-based service level. For example, in a case study on Saturn's after-market service, Cohen et al. (2000) reported that Saturn organized "pooling groups" for the purposes of inventory sharing. If a part is out of stock, the retailer may fulfill the order through a lateral transshipment from nearby Saturn retailers. This has helped Saturn to have the highest parts availability among all other car manufacturers, and Saturn customers are more loyal for repair services as compared to the industry average.

Although practiced heavily in real SPL systems, almost all the location, network design, and inventory models (integrated or otherwise, used in practice or proposed in the literature) in SPL systems do not incorporate inventory sharing as part of the process, hence models have room to be more precise and to actually obtain solutions that reflect the operational practice. In Chapter 3, we research the idea of inventory sharing between shared facilities. This should potentially decrease the overall inventory, but modeling this is an iterative process. For example, if facility A cannot satisfy demand of one of the customers assigned to it, then that customer could be satisfied by a direct shipment from another facility B. This may or may not count towards the overall customer service, depending on the time window considerations, but the reduction in inventory at facility B could adversely affect the customers of facility B if facility B runs out of that same part. Hence, the iterative process takes into account the potentially increased demand due to inventory sharing and potentially decreased fill rates of local customers, and the fill rates (local or due to inventory sharing) iteratively converge to their actual values. As the iterative process cannot be made part of a monolithic optimization model easily, we

initially plan to formulate an analytic method of obtaining these optimal fill rates for given base stock levels.

The ultimate goal in this dissertation is to use the analytic formulae (from the third chapter) within the optimization model from Chapter 2 to allow inventory sharing in the overall decision process of designing the network and determining the stock levels, among shared and dedicated facilities. This is the topic of Chapter 4. We then compare the performance of the models in each of the chapters for a given demand network.

The research done for this dissertation contributes to the existing literature by formulating more general problems and identifying procedures to solve them and/or obtain bounds for them in much less time. In Chapter 2, we allow customers to have potential dedicated facilities on-site. Using this general formulation, we isolate special cases that provide insight into the problem. For example, we are able to study the benefit of risk pooling, and identify cases where complete centralization or complete decentralization are optimal. Similarly, in Chapter 3 we provide a framework to incorporate inventory sharing within the overall decision process. The first challenge here is fill rate estimation. Based on some theoretical results, the problem is formulated as a binary knapsack problem. Combining the results of Chapters 2 and 3, the problem with dedicated facilities and inventory sharing is also formulated based on a binary knapsack structure, and we identify a greedy heuristic that provides good upper bounds to the overall problem.

A comparison of the models in the literature and Chapter 4 using the same demand network shows that we can obtain better solutions in much less time using the model in Chapter 4.

## **Chapter 2: Dedicated Facilities**

This chapter extends the works of Candas and Kutanoglu (2007a) as well as Jeet (2006) by allowing different types of facilities to be installed in the SPL network. In addition to the original facilities (now called shared facilities), some customers may have “dedicated facilities” on their own premises which are committed to them and are not (practically) permitted to stock-out. With this generalization, we identify special cases of this problem to help with the overall solution procedure. Finally, we perform a computational study to identify network parameters that favor dedicated facilities in the optimal solution. Furthermore, the introduction of dedicated facilities helps us analyze the benefits of risk pooling in SPL. Computational results show us that it is most often optimal to completely centralize or completely decentralize inventory.

### **1 Literature review**

When dealing with service parts, the physical locations of stocking facilities relative to the customer locations are crucial for efficient planning and inventory management. In service parts logistics, we encounter companies that have to setup stocking facilities across the country and hold spare parts inventory for existing customers. Customers have contracts with the company that require the stocking facilities to serve them within a given time window.

Cohen et al. (2002) report that in the North American computer industry, many companies face multiple market segments with very different perceptions of service criticality. At one extreme, there are corporate customers who are willing to pay a good price for on-site, same day service to maintain their mission critical computer systems. At the other extreme are consumers who do not mind a three day waiting period and are not willing to pay a very high price for service. With the introduction of dedicated facilities, each customer in the network could be satisfied in one of two ways; either from a shared facility along with many other customers, or from an on-site, dedicated facility.

As such, critical customers with high service level requirements have the option of being served by dedicated facilities.

The problem of interest is to identify a subset of feasible locations where dedicated facilities need to be installed, as well as a subset of other feasible locations where shared facilities need to be installed. Along with facility location and allocation decisions, we also need to assign (base) stock levels at each facility to maintain an overall service level. The objective is to minimize the total facility installation cost, transportation cost, and inventory holding cost.

A review of the literature includes papers by Nozick (2001), Nozick and Turnquist (2001), Daskin et al. (2002), and Barnhart and Cohn (2002). However, all these papers model the fill-rate-based service level as a parameter, whereas Candas and Kutanoglu (2007a) as well as Jeet (2006) allow each facility to have its own fill rate variable such that the overall required (or target) time-based service level is satisfied. All the above papers assume only one type of facility.

However, there are many cases in which companies may prefer to have a variety of facilities. Facilities can be classified based on product differentiation, sales volume, and service capabilities. In the field of environmental engineering and policy studies, decision makers have an option between choosing facilities with different technological capabilities. In such cases, Harkness and Reville (2002) formulate the basic capacitated facility location problem with mixed facilities having different cost and operating profiles based on a staircase cost structure. After formulating the problem as a mixed integer program, they adapt general Lagrangian relaxation techniques for solving the problem.

Similarly, Curtin and Church (2006) solve the problem of dispersing nuclear power plants and fossil fuel power plants such that security is maximized. Therefore, facilities are classified based on the source of power generation but they include constraints on the



feasibility of locating both types of facilities at the same location. For example, if both power plants were located in the same location, then a military strike against one location may cripple both power plants simultaneously. Performance metrics now include competitive market advantage and security. The computational results show that in a problem with 25 facility locations, instances with more than five types of facilities can take more than 10,000 seconds. Both Harkness and Reville (2002) and Curtin and Church (2006) do not include inventory decisions in their problem formulations.

We extend the works of Candas and Kutanoglu (2007a) and Jeet (2006) to allow multi-type facilities. This proposition is very practical since companies focusing on after-market service have high-priority customers, and these customers could benefit from service outlets (dedicated facilities) located on their own premises. Nevertheless, although we have multiple types of facilities in this problem, it is realistic to assume that if a dedicated facility is installed at a specific customer location, then this dedicated facility needs to dedicate all of its service only to that customer, and the customer can be served only by this dedicated facility for a specific part. Moreover, if a dedicated facility is installed, it is stocked in such a way that it does not stock out (has the parts that the customer needs) to provide truly high service level associated with having the stocking room on-site.

In Section 2 of this chapter, we model and analyze the integrated network design and inventory optimization problem with time-based service level constraints, but even after using an approximation scheme for the nonlinear fill rate function, large scale problems are not tractable even for a single part. This provides the motivation to look for special cases of these models that could be solved efficiently (Section 3). Next, we use computational results to identify network parameters that encourage the opening of dedicated facilities in Section 4. Finally in Section 5, we study the benefits of risk pooling by looking at a special case of the original problem.

## 2 Integrated problem with dedicated facilities

In this section, we model the integrated network design and inventory optimization problem for a single part.

### 2.1 Notation/Assumptions

Let  $I$  be the set of facilities and  $J$  be the set of customers. The set of facilities  $I$  is given by  $I = I' \cup I''$  where  $I'$  is the set of dedicated facilities (indexed by  $i'$ ) at customer locations ( $I' \subseteq J$ ), and  $I''$  is the set of shared facilities (indexed by  $i''$ ) at customer locations as well as other locations. The decision variables can be defined as follows: let  $Y_i$  be a binary variable such that  $Y_i = 1$  if facility  $i$  is chosen to be opened, and 0 otherwise, and let  $X_{i'j}$  be another binary variable such that  $X_{i'j} = 1$  if customer  $j$ 's demand is satisfied by shared facility  $i''$ , and 0 otherwise. For each facility  $i$ ,  $f_i$  denotes the fixed cost of opening and operating the facility (per unit time, say a week), and for each customer  $j$ ,  $d_j$  denotes the customer's mean demand rate per unit time ( $d_j > 0 \forall j$ ) for the part. Moreover,  $c_{i''j}$  denotes the unit transportation cost from shared facility  $i''$  to customer  $j$ , and  $\delta_{i''j}$  is 1 if customer  $j$  is within the time window of shared facility  $i''$ , i.e., facility  $i''$  can deliver the part to customer  $j$  within the time window (provided that the shared facility has the part in stock). We assume that dedicated facilities are always within the time window of the respective on-site customers and the cost of transportation in this case is negligible. Cost is directly proportional to the distance (closest shared facility is the cheapest in terms of transportation cost).

Customers can be grouped into customer-accounts such that each customer-account has its own service level. This enables large corporations with multiple customer locations to be satisfied with some target service level based on contractual agreements. Suppose the set of customer-accounts  $R$  is indexed by  $r$ . Then, let  $\alpha_r$  be the target service level in customer-account  $r$ , which determines the minimum fraction of the total demand in customer account  $r$  that needs to be satisfied within the time window. Assuming that

every customer belongs to exactly one customer-account, we now have a set  $J_r$ , which represents the set of customers that belong to customer-account  $r$   $\left(J = \bigcup_{r \in R} J_r\right)$ .

If a customer is assigned to a shared facility, then this facility should have a positive stock level. We also assume that whenever customer demand cannot be satisfied by the assigned shared facility, it is satisfied by a direct shipment from the central warehouse (CW). The central warehouse has infinite supply of inventory, and it is already installed (no fixed cost). None of the customers are within the time window of the central warehouse. In this chapter we assume that there is no direct shipment cost from the central warehouse to customers. However, customers cannot be “assigned” to the central warehouse. (This assumption will be relaxed in some special case problems).

## 2.2 Formulation with dedicated facilities

As a first step, we begin by formulating the service level constraint. The service level constraint formulation depends upon the distribution of the demand process. When dealing with service parts, customer demand is almost always exactly one unit. This is because the probability of more than one part failing at the same time is effectively zero. Therefore, it is safe to assume that demand occurs according to a Poisson process, which is also very common in service parts literature (see, for example, Muckstadt (2005), which is now a reference source in this area).

Suppose  $D \sim \text{Poisson}(\lambda)$  is the demand satisfied within the time window, and  $\tilde{D} \sim \text{Poisson}(\tilde{\lambda})$  is the demand satisfied after the time window. The long run probability that demand is satisfied within the time window is  $E\left(\frac{D}{D + \tilde{D}}\right) = \frac{E(D)}{E(D + \tilde{D})}$  since demand follows a Poisson distribution. The service level requirement states that at least  $\alpha\%$  of

the demand should be satisfied within the time window, i.e.  $\frac{E(D)}{E(D) + E(\tilde{D})}$

$$= \frac{E(D)}{E(D) + E(\tilde{D})} \geq \alpha.$$

The numerator can be calculated as  $E(D) = \sum_{\substack{i' \in I', \\ j \in J, \\ i' = j}} d_j Y_{i'} + \sum_{i'' \in I''} \sum_{j \in J} \delta_{i''j} d_j X_{i''j}$  because the

demand satisfied by dedicated facilities is always within the time window, and the rest of the demand may or may not be satisfied within the time window based on the parameters  $\delta_{ij}$ 's. Since we assume that all demand has to be satisfied, the denominator is  $E(D) + E(\tilde{D}) = \sum_{j \in J} d_j$ .

Based on the above formulae, the service level constraint for a single customer-account is given by

$$\sum_{\substack{i' \in I', \\ j \in J, \\ i' = j}} d_j Y_{i'} + \sum_{i'' \in I''} \sum_{j \in J} \delta_{i''j} d_j X_{i''j} \geq \alpha \sum_{j \in J} d_j \quad (2.1)$$

We can now formulate the overall network design optimization problem (NDP) with multiple customer-accounts (ignoring the inventory decisions for now) as follows:

**P<sub>1</sub>:** Minimize

$$\sum_{i' \in I'} f_{i'} Y_{i'} + \sum_{i'' \in I''} f_{i''} Y_{i''} + \sum_{i'' \in I''} \sum_{j \in J} c_{i''j} d_j X_{i''j} \quad (2.2a)$$

subject to

$$Y_{i'} + \sum_{i'' \in I''} X_{i''j} = 1 \quad \forall j \in I' \quad (2.2b)$$

$$\sum_{i'' \in I''} X_{i''j} = 1 \quad \forall j \in J \setminus I' \quad (2.2c)$$

$$X_{i''j} \leq Y_{i''} \quad \forall i'' \in I'', j \in J \quad (2.2d)$$

$$\sum_{\substack{i' \in I', \\ j \in J_r, \\ i' = j}} d_j Y_{i'} + \sum_{i'' \in I''} \sum_{j \in J_r} \delta_{i''j} d_j X_{i''j} \geq \alpha_r \sum_{j \in J_r} d_j \quad \forall r \in R \quad (2.2e)$$

$$X_{i''j} \in \{0,1\} \quad \forall i'' \in I'', j \in J \quad (2.2f)$$

$$Y_{i'} \in \{0,1\} \quad \forall i' \in I' \quad (2.2g)$$

$$Y_{i''} \in \{0,1\} \quad \forall i'' \in I''. \quad (2.2h)$$

The first term in the objective function is the fixed cost of opening dedicated facilities, followed by the fixed cost of opening shared facilities and the transportation cost of allocating customers to shared facilities. It is not necessary to calculate the transportation cost of allocating customers to dedicated facilities because they both are in the same location (assuming transportation cost is negligible). Constraint (2.2b) assigns a customer having a potential dedicated facility on-site either to itself (opening a dedicated facility) or to another shared facility, and constraint (2.2c) assigns the rest of the customers to shared facilities. Constraint (2.2d) forces a shared facility to be open if customers are allocated to it, and constraint (2.2e) ensures that the total assigned demand satisfies the target service level in each customer-account. The rest are binary constraints.

The main economic tradeoff in the above model is between the fixed cost of opening facilities and the cost of transporting parts to the customer. If we incorporate inventory decisions into the NDP model, we encounter another tradeoff, between holding cost of inventory and fill rate within the time window. If we open more facilities and stock them with parts, then more customers will be served within the time window. On the other hand, we can take advantage of inventory pooling by opening and stocking fewer facilities, but customers would be farther away, and fewer customers would be served within the time window. Therefore, another motivation of including inventory decisions in the model is to benefit from inventory pooling opportunities.

We now begin formulating the NDP problem with inventory (NDIP). As mentioned earlier, demand can be modeled as a Poisson process. Suppose  $t_{i''}$  is the lead time for replenishment at shared facility  $i''$ . Then the mean demand during lead time at shared facility  $i''$  is given by

$$\lambda_{i''} = t_{i''} \sum_{j \in J} d_j X_{i''j} \quad \forall i'' \in I'' . \quad (2.3)$$

There are two new decision variables  $S_{i''}$  and  $\beta_{i''}$  for each shared facility  $i''$ , where  $S_{i''}$  denotes the base stock level and  $\beta_{i''}$  is the corresponding fill rate at shared facility  $i''$ .

As mentioned earlier, whenever a shared facility stocks-out for a customer's demand, the customer is served by a direct delivery from the central warehouse, but it is considered to be a case of lost sales for the shared facility under consideration, and does not count towards the target service level. With this assumption, the fill rate is a nonlinear function of the mean demand during lead time and the base stock level as follows:

$$\beta_{i''}(S_{i''}, \lambda_{i''}) = 1 - \frac{\frac{\lambda_{i''}^{S_{i''}}}{S_{i''}!}}{\sum_{k=0}^{S_{i''}} \frac{\lambda_{i''}^k}{k!}} \quad \forall i'' \in I'' , \quad (2.4)$$

where  $\frac{\lambda_{i''}^{S_{i''}}}{S_{i''}!} / \sum_{k=0}^{S_{i''}} \frac{\lambda_{i''}^k}{k!}$  is the Erlang blocking formula. The Erlang blocking formula gives us the

long run probability of stocking out in a continuous time Markov chain where each state corresponds to the on-hand inventory level at shared facility  $i''$  (Zipkin (2000)).

Note that we do not need base stock level variables and fill rate variables for dedicated facilities. This is because of the assumption we made that dedicated facilities should provide practically 100% service to their respective customers. Moreover, due to the low demand rate characteristic of customers in the service parts industry, this could be further

simplified to say that a stock of one unit is always sufficient for essentially 100% service (at that customer location). Figure 1 shows that when mean lead time demand is up to 0.01 units, a base stock level of one unit provides 100% service for all practical purposes. Therefore, the open/close location variable of dedicated facilities ( $Y_{i'}$ ) additionally serves as the fill rate variable as well as the base stock level variable.

We mentioned previously that the service level requirement states that at least  $\alpha$  % of the total demand should be satisfied within the time window, i.e.  $\frac{E(D)}{E(D) + E(\tilde{D})} \geq \alpha$  where the denominator is  $E(D) + E(\tilde{D}) = \sum_{j \in J} d_j$ . Now that shared facilities are allowed to stockout, the service level constraint has to include part availability (or fill rate).

In order to estimate the numerator, suppose  $D_i \sim \text{Poisson}(\lambda_i)$  is the demand during the lead time that is satisfied within the time window at facility  $i$  and  $Z_i$  is the on-hand inventory level at facility  $i$ . By linearity of expectation,  $E(D) = \sum_{i \in I} E(D_i)$ . Using the “law of total probability for expectations” on the numerator,  $\sum_{i \in I} E(D_i) = \sum_{i \in I} E(D_i | Z_i = 0)P(Z_i = 0) + E(D_i | Z_i > 0)P(Z_i > 0)$ , the first term of which is equal to 0. Therefore,  $E(D) = \sum_{i \in I} E(D_i) = \sum_{i \in I} E(D_i | Z_i > 0)P(Z_i > 0) = \sum_{i \in I} E(D_i)\beta_i$ . As a result,  $E(D) = \sum_{i' \in I'} E(D_{i'})Y_{i'} + \sum_{i'' \in I''} E(D_{i'')}\beta_{i''}$  since  $Y_{i'}$  serves as the fill rate variable for dedicated facilities. The service level constraint for a single customer-account with Poisson demand is given by

$$\sum_{\substack{i' \in I', \\ j \in J, \\ i' = j}} d_j Y_{i'} + \sum_{i'' \in I''} \beta_{i''} \sum_{j \in J} \delta_{i''j} d_j X_{i''j} \geq \alpha \sum_{j \in J} d_j. \quad (2.5)$$

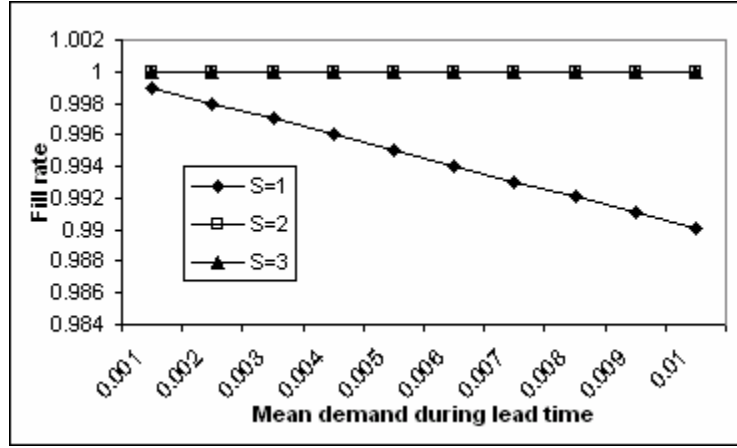


Figure 1. Fill rate function

Suppose  $h_i$  is the unit holding cost per unit time at facility  $i$ . We can now formulate the NDIP problem by adding equations (2.3) and (2.4) to  $\mathbf{P}_1$ , replacing constraint (2.2e) with equation (2.5), and simultaneously modifying the objective function.

**P<sub>2</sub>:** Minimize

$$\sum_{i \in I'} (f_i + h_i) Y_i + \sum_{i \in I''} (f_i Y_i + h_i S_i) + \sum_{i \in I''} \sum_{j \in J} c_{ij} d_j X_{ij} \quad (2.6a)$$

subject to

$$Y_i + \sum_{i \in I''} X_{ij} = 1 \quad \forall j \in I' \quad (2.6b)$$

$$\sum_{i \in I''} X_{ij} = 1 \quad \forall j \in J \setminus I' \quad (2.6c)$$

$$X_{ij} \leq Y_i \quad \forall i \in I'', j \in J \quad (2.6d)$$

$$\lambda_i = t_i \sum_{j \in J} d_j X_{ij} \quad \forall i \in I'' \quad (2.6e)$$

$$\beta_i = 1 - \frac{\frac{\lambda_i^{S_i}}{S_i!}}{\sum_{k=0}^{S_i} \frac{\lambda_i^k}{k!}} \quad \forall i \in I'' \quad (2.6f)$$

$$S_i \leq s_{\max} Y_i \quad \forall i \in I'' \quad (2.6g)$$



$$\sum_{\substack{i' \in I' \\ j \in J_r \\ i=j}} d_j Y_{i'} + \sum_{i'' \in I''} \beta_{i''} \sum_{j \in J_r} \delta_{i''j} d_j X_{i''j} \geq \alpha_r \sum_{j \in J_r} d_j \quad \forall r \in R \quad (2.6h)$$

$$Y_{i''} \leq S_{i''} \quad \forall i'' \in I'', j \in J \quad (2.6i)$$

$$X_{i''j} \in \{0,1\} \quad \forall i'' \in I'', j \in J \quad (2.6j)$$

$$Y_{i'} \in \{0,1\} \quad \forall i' \in I' \quad (2.6k)$$

$$Y_{i''} \in \{0,1\} \quad \forall i'' \in I'' \quad (2.6l)$$

$$S_{i''} \in \bar{S} \quad \forall i'' \in I'' \quad (2.6m)$$

$$\lambda_{i''} \geq 0 \quad \forall i'' \in I'' \quad (2.6n)$$

$$\beta_{i''} \geq 0 \quad \forall i'' \in I'', \quad (2.6o)$$

where  $\bar{S} = \{0,1,2,\dots,s_{\max}\}$  is the set of feasible base stock levels.

Since the location variable of dedicated facilities also represents the base stock level, the fixed cost and holding cost of dedicated facilities are combined in the first term of the objective function. The only other change in the objective function is the inclusion of the holding costs at shared facilities. Constraints (2.6b), (2.6c), and (2.6d) are the same as those in the NDP formulation. The new inventory constraints (2.6e) and (2.6f) calculate the mean demand during lead time at each shared facility and the corresponding fill rate, respectively. Constraint (2.6g) ensures that shared facilities can be stocked only if they are opened, and no more than  $s_{\max}$  units of inventory can be stocked at any shared facility. A generalized version of equation (2.5) for multiple customer-accounts is given in constraint (2.6h), and constraint (2.6i) forces each opened shared facility to be stocked with at least one unit. Constraints (2.6j) through (2.6o) are non-negativity and integrality constraints.

We can manipulate the above NDIP formulation to obtain special cases of this problem. The problem solved by Candas and Kutanoglu (2007a) and Jeet (2006) is a special case with no dedicated facilities ( $I'=\emptyset$ ), and with a system-wide service level

( $|R|=1$  and  $J_1 = J$ ). Another special case is where each customer is a customer-account by itself and has its own target service level ( $R = J$  and  $J_j = \{j\}$ ), collectively called customer-centric service levels (Candas and Kutanoglu (2007b)).

An important theoretical result is that there are certain conditions in which a dedicated facility will always be open in any optimal solution. However, we cannot make any statements about the conditions when a dedicated facility will be closed in any optimal solution because regardless of the parameters in the problem, a dedicated facility may always have to be opened to satisfy the service level constraint.

**Theorem 2.1.** *Dedicated facility  $i'$  is open in any optimal solution if*

$$f_{i'} + h_{i'} \leq \min_{i''} \{c_{i'i''} d_{i'}\}.$$

**Proof:** Suppose all shared facilities are already open. Then dedicated facility  $i'$  is opened only if the total cost of opening and holding inventory is less than the transportation cost and the marginal inventory holding cost ( $\bar{h}_{i''}$ ) at the closest shared facility:

$$f_{i'} + h_{i'} \leq c_{i'i''} d_{i'} + \bar{h}_{i''},$$

since  $\bar{h}_{i''} \geq 0 \forall i'' \in I''$ , and  $f_{i'} + h_{i'} \leq c_{i'i''} d_{i'} \leq \min_{i''} \{c_{i'i''} d_{i'}\}$ . ■

Since the main focus of this chapter is to identify theoretical results and derive intuitions about the problem as opposed to finding better ways to solve the problem, we adapt a previously developed formulation by Jeet (2006) where special ordered sets of type 2 variables (sos2) are used in the approximation of the fill rate function. During the progress of this research, there have been improvements in the formulation where a better lower bounding approach is used to solve the problem and sos2 variables need not be used anymore (Jeet (2006)). However, all the results in this chapter are based on the sos2 variable formulation (Appendix A).

### 3 Special cases

In this section, we identify special cases of the NDIP based on the number of shared facilities as well as some other special cases based on the number of customer-accounts.

#### 3.1 Special cases based on the number of shared facilities

The NDIP problem can be partitioned into four cases; no shared facilities among multiple dedicated facilities, only one shared facility among multiple dedicated facilities, multiple shared facilities among multiple dedicated facilities, and all shared facilities with no dedicated facilities. In each of these cases, parameters such as the fixed cost ( $f_i$ ) and the holding cost ( $h_i$ ) can be varied to identify potentially easy problems. Table 1 shows sub-cases under each partition as well as the computational complexity of the problem.

Table 1. Special cases based on the number of shared facilities

Case	Sub-case	Complexity	Problem type
No shared facilities ( $ I'  \geq 0,  I''  = 0$ )	Allow customers to be assigned to CW	Weakly NP-Hard	Binary knapsack
One shared facility ( $ I'  \geq 0,  I''  = 1$ )	$I' = J$ $f_{i'} = 0 \ \forall i', f_{i''} = 0 \ \forall i'',$ $h_{i'} = h \ \forall i', h_{i''} = h \ \forall i''$ $d_j = d \ \forall j, c_{i'j} = c \ \forall j, \delta_{i'j} = 1 \ \forall j$ Allow customers to be assigned to CW	Trivial	
Multiple shared facilities ( $ I'  \geq 0,  I''  \geq 0$ )	$f_{i'} = 0 \ \forall i', f_{i''} = 0 \ \forall i'',$ $h_{i'} = 0 \ \forall i', h_{i''} = 0 \ \forall i''$	Trivial	
	$f_{i'} \geq 0 \ \forall i', f_{i''} \geq 0 \ \forall i'',$ $h_{i'} = 0 \ \forall i', h_{i''} = 0 \ \forall i''$	Strongly NP-Hard	NDP
All shared facilities ( $ I'  = 0,  I''  \geq 0$ )	$f_{i''} = 0 \ \forall i'', h_{i''} = 0 \ \forall i''$	Trivial	
	$f_{i''} \geq 0 \ \forall i'', h_{i''} = 0 \ \forall i''$	Strongly NP-Hard	NDP

Note that an NP-Hard problem is “Weakly NP-Hard” if there exists a pseudo-polynomial time algorithm to solve the problem. On the other hand, if no such algorithm exists, then the problem is “Strongly NP-Hard”.

### *No shared facilities*

In the case where customers can be assigned to the central warehouse, the problem turns out to have a binary knapsack formulation for each customer-account. All those customers that do not have dedicated facilities are assigned to the central warehouse, thus reducing the set of customers to the set of customers with dedicated facilities  $I'$ . Also  $X_{i'j} \forall j \in I'$  can be replaced by  $(1 - Y_{i'})$ . Since the central warehouse has infinite supply, and none of the customers are within the time window of the central warehouse, we eliminate the inventory decision variables completely from the model resulting in the following formulation in terms of the  $Y_{i'}$  variables alone (for each customer-account  $r$ ):

**P<sub>2</sub>**:Minimize

$$\sum_{\substack{i' \in I', \\ j \in J_r, \\ i'=j}} (f_{i'} + h_{i'}) Y_{i'} \quad (2.6a')$$

subject to

$$\sum_{\substack{i' \in I', \\ j \in J_r, \\ i'=j}} d_j Y_{i'} \geq \alpha_r \sum_{j \in J_r} d_j \quad \forall r \in R \quad (2.6h')$$

$$Y_{i'} \in \{0,1\} \quad \forall i' \in I'. \quad (2.6k')$$

For each customer-account  $r$ , this is the binary knapsack formulation, by inspection. Those customers with  $Y_{i'}^* = 0$  in the optimal solution are assigned to the central warehouse.

### ***One shared facility***

Allowing customers to be assigned to the central warehouse, the case with free fixed cost ( $f_{i'} = 0 \forall i', f_{i''} = 0 \forall i''$ ), and constant values for holding cost, demand, and transportation cost ( $h_{i'} = h \forall i', h_{i''} = h \forall i'', d_j = d \forall j, c_{i'j} = c \forall j$ ) is trivial when all customers are within the time window of the single shared facility. This special case is trivial because for a given stock level at the shared facility all the remaining variables are trivial. Therefore, this special case can be solved by simply evaluating the objective value at each level of stock at the shared facility. This special case is discussed in detail in Section 5.

### ***Multiple shared facilities***

In the case where  $f_{i'} = 0, f_{i''} = 0, h_{i'} = 0$ , and  $h_{i''} = 0 \forall i' \in I', i'' \in I''$ , the optimal solution is to open all dedicated facilities, assign each customer to its own dedicated facility, and stock each dedicated facility with  $S_{i'} = 1$  unit. Open all shared facilities, and assign each remaining customer to the closest shared facility. Any feasible  $\beta$  vector could be used to solve for  $S_{i''}$ . For example, we can set  $\beta_{i''} = \max_{r \in R} \{\alpha_r\} \forall i'' \in I''$  and calculate the corresponding  $S_{i''}$  values based on equation (2.4). As a result, this solution is trivial. The case with  $h_{i'} = 0$ , and  $h_{i''} = 0 \forall i' \in I', i'' \in I''$  is basically the NDP problem which is NP-Hard.

### ***All shared facilities***

The case with  $f_{i'} = 0$ , and  $h_{i''} = 0 \forall i'' \in I''$  is trivial. The solution is to open all shared facilities, and assign each customer to the closest shared facility. Any feasible  $\beta$  vector could be used to solve for  $S_{i''}$ . The case with  $h_{i''} = 0 \forall i'' \in I''$  is the NDP problem which is again NP-Hard.

In all the above cases, whenever holding cost is negligible, any  $\beta$  vector satisfying constraint (2.6h) could be used to calculate the base stock level  $S_{i^*}$  because there is no motivation to decrease inventory. In the extreme case, we can set  $\beta$  for each shared facility to be equal to the target service level. Another way to obtain a feasible  $\beta$  vector is by sorting shared facilities in non-increasing order of assigned demand and assigning  $\beta_{i^*} = 1$  for each shared facility in this order until the target service level is achieved.

### 3.2 Special cases based on the number of customer accounts

Based on the number of customer accounts, the NDIP problem can be partitioned into three cases; system-wide service level, customer-account service levels, and customer-centric service levels. The customer-account service levels case is the general case. For the other two special cases, we now compare the relative complexity of the problems in Table 2.

Table 2. Special cases based on the number of customer accounts

Case	Sub-case	Complexity	Problem type
System-wide service level ( $ R =1$ )		Strongly NP-Hard	NDIP
Customer-centric service levels ( $R=J$ )	( $ I'  \geq 0,  I''  = 0$ ), Allow customers to be assigned to CW	Trivial	
	$\alpha_j = \alpha$	Strongly NP-Hard	CFL

#### *System-wide service level*

When there exists only one customer-account, we can modify the service level constraint as follows.

$$\sum_{\substack{i \in I', \\ j \in J, \\ i'=j}} d_j Y_{i'} + \sum_{i' \in I''} \beta_{i'} \sum_{j \in J} \delta_{i'j} d_j X_{i'j} \geq \alpha \sum_{j \in J} d_j \quad (2.7)$$

Replacing constraint (2.6h) with equation (2.7) as the service level constraint, we can solve the NDIP problem with a system-wide service level.

### *Customer-centric service levels*

Suppose  $\alpha_j$  is the target service level for customer  $j$ , the  $d_j$  term drops out from both sides of the service level constraint resulting in the following equations as the modified service level constraints:

$$Y_{i'} + \sum_{i'' \in I''} \beta_{i''} \delta_{i''j} X_{i''j} \geq \alpha_j \quad \forall j \in I', \quad (2.8)$$

$$\sum_{i'' \in I''} \beta_{i''} \delta_{i''j} X_{i''j} \geq \alpha_j \quad \forall j \in J \setminus I'. \quad (2.9)$$

In the case where  $|I'| \geq 0, |I''| = 0$ , and we allow customers to be assigned to the central warehouse, the binary knapsack formulation  $\mathbf{P}_2'$  becomes trivial because the  $d_j$  term drops out from both sides of constraint (2.6h') resulting in the following formulation:

$\mathbf{P}_2''$ : Minimize

$$\sum_{\substack{i' \in I', \\ j \in J, \\ i' = j}} (f_{i'} + h_{i'}) Y_{i'} \quad (2.6a'')$$

subject to

$$Y_{i'} \geq \alpha_j \quad \forall j \in I' \quad (2.6h'')$$

$$Y_{i'} \in \{0,1\} \quad \forall i' \in I'. \quad (2.6k'')$$

The solution is that for every  $i'$  such that  $\alpha_j = 0 \quad \forall j \in I'$  and  $f_{i'} + h_{i'} > c_{i'j} d_j \quad \forall j \in I'$ , we close dedicated facility  $i'$ . Otherwise, it is optimal to open dedicated facility  $i'$ .

Candas and Kutanoglu (2007b) formulate the NDIP problem with customer-centric service levels but without any dedicated facilities. Based on the critical observation that

each customer has to be assigned to a shared facility that has a higher fill rate than the customer's target service level, they report that the problem formulation resembles a capacitated facility location (CFL) problem. If the assignment constraints are relaxed, the resulting subproblem decomposes by shared facility. In addition, if each customer has the same demand, then each subproblem reduces to a knapsack problem.

Appendix B shows their formulation modified to include dedicated facilities. This problem also resembles a CFL. By extending the observation made by Candas and Kutanoglu (2007b), if we relax both sets of assignment constraints (i.e. one set for customers with dedicated facilities, and the other set for the rest of the customers) then the resulting subproblem again decomposes by shared facility. When all customers have the same demand, the problem once again reduces to a knapsack problem with an additional set of variables for opening/closing dedicated facilities.

## 4 Computational results

Consider a 10 shared facility, 50 customer service parts network in a circular region of diameter 100 units. Customer and shared facility locations are generated by randomly assigning polar coordinates for each customer and shared facility. Suppose there are five customer-accounts with 10 customers each, and let the time window for service be 30 units. In order to analyze the tradeoff between the benefit of opening dedicated facilities and the benefits of inventory pooling, let us also suppose that shared facilities are free to install. All costs are fixed and constant across facilities and customers except for transportation cost which depends on the physical locations of the customers and the facilities. We can now identify those parameters that contribute to the benefit of using dedicated facilities by running a design of experiments with the following factors.

- $f_i = \{0, 0.2, 0.4\}$
- $h_i = \{0, 0.1, 0.2\}$
- $\alpha_r = \{0.6, 0.8\}$



- $d_j = \{0.005, 0.01\}$

Each of the 36 instances is replicated four times with no dedicated facilities ( $\{|I'| = 0, |I''| = 10\}$ ), with half of the customer locations as potential dedicated facilities ( $\{|I'| = 25, |I''| = 10\}$ ), with all the customer locations as potential dedicated facilities with no shared facilities ( $\{|I'| = 50, |I''| = 0\}$ ), and with all customer locations as dedicated facilities and all shared facilities ( $\{|I'| = 50, |I''| = 10\}$ ).

The formulation in Appendix A is used to obtain the computational results. As mentioned in Section 2.2, the formulation in Appendix A is a modification of the sos2 variable formulation by Jeet (2006). The modifications are listed as follows. First of all we generate a set of feasible dedicated facility locations among all the customer locations ( $I'$ ), and then for every dedicated facility  $i'$  we define a new set of variables ( $Y_{i'}$ ), and we also estimate fixed cost ( $f_{i'}$ ) and holding cost ( $h_{i'}$ ) parameters.

The new objective function now has to reflect the relevant costs of dedicated facilities given by  $\sum_{i' \in I'} (f_{i'} + h_{i'}) Y_{i'}$  which is added to the objective function.

In terms of constraint modification, we need a new set of assignment constraints that allows a customer to either be assigned to a dedicated facility (if there exists one on-site) or to a shared facility. Therefore, we add  $Y_{i'} + \sum_{i'' \in I''} X_{i'j} = 1 \ \forall j \in I'$  to the set of constraints.

In addition, we need to assign 100% fill rate to all the demand satisfied by dedicated facilities. This is done by adding  $\sum_{\substack{i' \in I', \\ j \in J_r \\ i' = j}} d_j Y_{i'}$  to the existing service level constraint. These

modifications are sufficient to include dedicated facilities into the sos2 variable formulation by Jeet (2006). This modified sos2 formulation (Appendix A) is modeled in MOSEL and solved using Branch and bound with Xpress MP as the solver (provided by

Dash Optimization) using a Pentium 4 700 MHz processor with 1GB RAM, and the results are given in Table 3.

The input parameters are organized as follows.

- Fixed cost of opening a dedicated facility – denoted by “ $f_i$ ”
- Holding cost of inventory at each facility – denoted by “ $h_i$ ”
- Target service level of each customer-account – denoted by “ $\alpha_r$ ”
- Demand of each customer – denoted by “ $d_j$ ”
- Percentage of customers with dedicated facilities  

$$\left( \frac{|I'|}{50} \times 100 \right) \text{ – denoted by “\% ded”}$$
- Percentage of shared facilities that are feasible to be opened and stocked  

$$\left( \frac{|I''|}{10} \times 100 \right) \text{ – denoted by “\% shd”}$$

The output is organized as follows.

- Number of dedicated facilities opened – denoted by “# ded”
- Number of shared facilities opened – denoted by “# shd”
- Units of inventory stocked at shared facilities – denoted by “s shd”
- Total cost – denoted by “Obj Val”
- Solution time – denoted by “Sol Time”
- Status of solution at termination – denoted by “Status”
- Number of branch and bound nodes at termination – denoted by “B&B nodes”
- Optimality gap at termination – denoted by “Opt Gap”

Table 3. Computational results – dedicated facilities

Exp	INPUT						OUTPUT							
	$f_i$	$h_i$	$\alpha$	$d_j$	% ded	% shd	# ded	# shd	s shd	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
1	0	0	0.6	0.005	0	100	0	10	50	3.275	11.02	Opt	108	0
2	0	0	0.6	0.005	50	100	25	9	45	1.731	5.368	Opt	12	0
3	0	0	0.6	0.005	100	0	50	0	0	0	0.2	Opt	1	0
4	0	0	0.6	0.005	100	100	50	0	0	0	0.281	Opt	1	0
5	0	0	0.6	0.01	0	100	0	10	50	6.55	16.49	Opt	337	0
6	0	0	0.6	0.01	50	100	25	9	45	3.462	5.468	Opt	14	0
7	0	0	0.6	0.01	100	0	50	0	0	0	0.261	Opt	1	0
8	0	0	0.6	0.01	100	100	50	0	0	0	0.28	Opt	1	0
9	0	0	0.8	0.005	0	100	0	10	50	3.275	14.96	Opt	280	0
10	0	0	0.8	0.005	50	100	25	9	45	1.731	4.997	Opt	21	0
11	0	0	0.8	0.005	100	0	50	0	0	0	0.22	Opt	1	0
12	0	0	0.8	0.005	100	100	50	0	0	0	0.301	Opt	1	0
13	0	0	0.8	0.01	0	100	0	10	50	6.55	8.862	Opt	69	0
14	0	0	0.8	0.01	50	100	25	9	45	3.462	6.089	Opt	19	0
15	0	0	0.8	0.01	100	0	50	0	0	0	0.211	Opt	1	0
16	0	0	0.8	0.01	100	100	50	0	0	0	0.29	Opt	1	0
17	0	0.1	0.6	0.005	0	100	0	7	7	4.098	6.81	Opt	26	0
18	0	0.1	0.6	0.005	50	100	4	7	7	3.957	7.711	Opt	29	0
19	0	0.1	0.6	0.005	100	0	50	0	0	5	0.21	Opt	1	0
20	0	0.1	0.6	0.005	100	100	11	7	7	3.662	6.059	Opt	16	0
21	0	0.1	0.6	0.01	0	100	0	8	8	7.448	11.47	Opt	84	0
22	0	0.1	0.6	0.01	50	100	14	8	8	6.445	2.693	Opt	7	0
23	0	0.1	0.6	0.01	100	0	50	0	0	5	0.221	Opt	1	0
24	0	0.1	0.6	0.01	100	100	31	4	4	4.728	3.385	Opt	23	0
25	0	0.1	0.8	0.005	0	100	0	7	7	4.098	12.32	Opt	141	0
26	0	0.1	0.8	0.005	50	100	4	7	7	3.957	8.653	Opt	60	0
27	0	0.1	0.8	0.005	100	0	50	0	0	5	0.22	Opt	1	0
28	0	0.1	0.8	0.005	100	100	11	7	7	3.662	6.9	Opt	34	0
29	0	0.1	0.8	0.01	0	100	0	8	8	7.448	10.9	Opt	105	0
30	0	0.1	0.8	0.01	50	100	14	8	8	6.446	5.788	Opt	5	0
31	0	0.1	0.8	0.01	100	0	50	0	0	5	0.22	Opt	1	0
32	0	0.1	0.8	0.01	100	100	31	4	4	4.728	2.944	Opt	1	0
33	0	0.2	0.6	0.005	0	100	0	7	7	4.798	4.596	Opt	10	0
34	0	0.2	0.6	0.005	50	100	0	7	7	4.798	7.091	Opt	6	0
35	0	0.2	0.6	0.005	100	0	50	0	0	10	0.23	Opt	1	0
36	0	0.2	0.6	0.005	100	100	0	7	7	4.798	10.83	Opt	105	0
37	0	0.2	0.6	0.01	0	100	0	7	7	8.196	11.45	Opt	61	0
38	0	0.2	0.6	0.01	50	100	4	7	7	7.915	9.494	Opt	70	0
39	0	0.2	0.6	0.01	100	0	50	0	0	10	0.23	Opt	1	0
40	0	0.2	0.6	0.01	100	100	11	7	7	7.323	6.559	Opt	58	0
41	0	0.2	0.8	0.005	0	100	0	7	7	4.798	8.302	Opt	73	0
42	0	0.2	0.8	0.005	50	100	0	7	7	4.798	12.59	Opt	123	0
43	0	0.2	0.8	0.005	100	0	50	0	0	10	0.23	Opt	1	0
44	0	0.2	0.8	0.005	100	100	0	7	7	4.798	13.37	Opt	64	0
45	0	0.2	0.8	0.01	0	100	0	7	7	8.196	11.65	Opt	105	0
46	0	0.2	0.8	0.01	50	100	4	7	7	7.915	12.3	Opt	111	0
47	0	0.2	0.8	0.01	100	0	50	0	0	10	0.22	Opt	1	0
48	0	0.2	0.8	0.01	100	100	11	7	7	7.323	13.41	Opt	166	0

Exp	INPUT						OUTPUT							
	$f_i$	$h_i$	$\alpha$	$d_j$	% ded	% shd	# ded	# shd	s shd	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
49	0.2	0	0.6	0.005	0	100	0	10	50	3.275	10.29	Opt	108	0
50	0.2	0	0.6	0.005	50	100	0	10	50	3.275	8.472	Opt	43	0
51	0.2	0	0.6	0.005	100	0	50	0	0	10	0.221	Opt	1	0
52	0.2	0	0.6	0.005	100	100	0	10	50	3.275	9.924	Opt	50	0
53	0.2	0	0.6	0.01	0	100	0	10	50	6.55	16.41	Opt	337	0
54	0.2	0	0.6	0.01	50	100	4	10	50	6.276	13.59	Opt	209	0
55	0.2	0	0.6	0.01	100	0	50	0	0	10	0.23	Opt	1	0
56	0.2	0	0.6	0.01	100	100	10	10	50	5.817	9.184	Opt	65	0
57	0.2	0	0.8	0.005	0	100	0	10	50	3.275	14.73	Opt	280	0
58	0.2	0	0.8	0.005	50	100	0	10	50	3.275	8.402	Opt	44	0
59	0.2	0	0.8	0.005	100	0	50	0	0	10	0.23	Opt	1	0
60	0.2	0	0.8	0.005	100	100	0	10	50	3.275	10.93	Opt	79	0
61	0.2	0	0.8	0.01	0	100	0	10	50	6.55	9.173	Opt	69	0
62	0.2	0	0.8	0.01	50	100	4	10	50	6.276	9.804	Opt	48	0
63	0.2	0	0.8	0.01	100	0	50	0	0	10	0.241	Opt	1	0
64	0.2	0	0.8	0.01	100	100	10	10	50	5.817	12.54	Opt	262	0
65	0.2	0.1	0.6	0.005	0	100	0	7	7	4.098	6.589	Opt	26	0
66	0.2	0.1	0.6	0.005	50	100	0	7	7	4.098	7.291	Opt	56	0
67	0.2	0.1	0.6	0.005	100	0	50	0	0	15	0.23	Opt	1	0
68	0.2	0.1	0.6	0.005	100	100	0	7	7	4.098	6.419	Opt	5	0
69	0.2	0.1	0.6	0.01	0	100	0	8	8	7.448	10.69	Opt	84	0
70	0.2	0.1	0.6	0.01	50	100	1	8	8	7.43	9.333	Opt	70	0
71	0.2	0.1	0.6	0.01	100	0	50	0	0	15	0.241	Opt	1	0
72	0.2	0.1	0.6	0.01	100	100	3	7	7	7.354	9.193	Opt	95	0
73	0.2	0.1	0.8	0.005	0	100	0	7	7	4.098	11.28	Opt	141	0
74	0.2	0.1	0.8	0.005	50	100	0	7	7	4.098	9.293	Opt	79	0
75	0.2	0.1	0.8	0.005	100	0	50	0	0	15	0.24	Opt	1	0
76	0.2	0.1	0.8	0.005	100	100	0	7	7	4.098	6.84	Opt	19	0
77	0.2	0.1	0.8	0.01	0	100	0	8	8	7.448	10.33	Opt	105	0
78	0.2	0.1	0.8	0.01	50	100	1	8	8	7.43	12.53	Opt	141	0
79	0.2	0.1	0.8	0.01	100	0	50	0	0	15	0.26	Opt	1	0
80	0.2	0.1	0.8	0.01	100	100	3	7	7	7.354	9.233	Opt	49	0
81	0.2	0.2	0.6	0.005	0	100	0	7	7	4.798	4.587	Opt	10	0
82	0.2	0.2	0.6	0.005	50	100	0	7	7	4.798	6.239	Opt	6	0
83	0.2	0.2	0.6	0.005	100	0	50	0	0	20	0.24	Opt	1	0
84	0.2	0.2	0.6	0.005	100	100	0	7	7	4.798	9.153	Opt	92	0
85	0.2	0.2	0.6	0.01	0	100	0	7	7	8.196	9.184	Opt	61	0
86	0.2	0.2	0.6	0.01	50	100	0	7	7	8.196	11.67	Opt	139	0
87	0.2	0.2	0.6	0.01	100	0	50	0	0	20	0.251	Opt	1	0
88	0.2	0.2	0.6	0.01	100	100	0	7	7	8.196	10.24	Opt	78	0
89	0.2	0.2	0.8	0.005	0	100	0	7	7	4.798	7.11	Opt	73	0
90	0.2	0.2	0.8	0.005	50	100	0	7	7	4.798	10.43	Opt	123	0
91	0.2	0.2	0.8	0.005	100	0	50	0	0	20	0.25	Opt	1	0
92	0.2	0.2	0.8	0.005	100	100	0	7	7	4.798	12.07	Opt	145	0
93	0.2	0.2	0.8	0.01	0	100	0	7	7	8.196	10.75	Opt	105	0
94	0.2	0.2	0.8	0.01	50	100	0	7	7	8.196	7.962	Opt	53	0
95	0.2	0.2	0.8	0.01	100	0	50	0	0	20	0.25	Opt	1	0
96	0.2	0.2	0.8	0.01	100	100	0	7	7	8.196	10.03	Opt	129	0

Exp	INPUT						OUTPUT							
	$f_i$	$h_i$	$\alpha$	$d_j$	% ded	% shd	# ded	# shd	s shd	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
97	0.4	0	0.6	0.005	0	100	0	10	50	3.275	9.744	Opt	108	0
98	0.4	0	0.6	0.005	50	100	0	10	50	3.275	7.992	Opt	43	0
99	0.4	0	0.6	0.005	100	0	50	0	0	20	0.31	Opt	1	0
100	0.4	0	0.6	0.005	100	100	0	10	50	3.275	11.19	Opt	246	0
101	0.4	0	0.6	0.01	0	100	0	10	50	6.55	15.81	Opt	337	0
102	0.4	0	0.6	0.01	50	100	0	10	50	6.55	6.92	Opt	36	0
103	0.4	0	0.6	0.01	100	0	50	0	0	20	0.261	Opt	1	0
104	0.4	0	0.6	0.01	100	100	0	10	50	6.55	8.262	Opt	35	0
105	0.4	0	0.8	0.005	0	100	0	10	50	3.275	14.26	Opt	280	0
106	0.4	0	0.8	0.005	50	100	0	10	50	3.275	7.821	Opt	44	0
107	0.4	0	0.8	0.005	100	0	50	0	0	20	0.261	Opt	1	0
108	0.4	0	0.8	0.005	100	100	0	10	50	3.275	11.3	Opt	127	0
109	0.4	0	0.8	0.01	0	100	0	10	50	6.55	8.452	Opt	69	0
110	0.4	0	0.8	0.01	50	100	0	10	50	6.55	10.6	Opt	282	0
111	0.4	0	0.8	0.01	100	0	50	0	0	20	0.271	Opt	1	0
112	0.4	0	0.8	0.01	100	100	0	10	50	6.55	10.5	Opt	211	0
113	0.4	0.1	0.6	0.005	0	100	0	7	7	4.098	6.619	Opt	26	0
114	0.4	0.1	0.6	0.005	50	100	0	7	7	4.098	7.59	Opt	56	0
115	0.4	0.1	0.6	0.005	100	0	50	0	0	25	0.271	Opt	1	0
116	0.4	0.1	0.6	0.005	100	100	0	7	7	4.098	6.639	Opt	5	0
117	0.4	0.1	0.6	0.01	0	100	0	8	8	7.448	10.97	Opt	84	0
118	0.4	0.1	0.6	0.01	50	100	0	8	8	7.448	11.31	Opt	189	0
119	0.4	0.1	0.6	0.01	100	0	50	0	0	25	0.271	Opt	1	0
120	0.4	0.1	0.6	0.01	100	100	0	8	8	7.448	12.06	Opt	122	0
121	0.4	0.1	0.8	0.005	0	100	0	7	7	4.098	11.42	Opt	141	0
122	0.4	0.1	0.8	0.005	50	100	0	7	7	4.098	9.473	Opt	79	0
123	0.4	0.1	0.8	0.005	100	0	50	0	0	25	0.261	Opt	1	0
124	0.4	0.1	0.8	0.005	100	100	0	7	7	4.098	7.1	Opt	19	0
125	0.4	0.1	0.8	0.01	0	100	0	8	8	7.448	10.39	Opt	105	0
126	0.4	0.1	0.8	0.01	50	100	0	8	8	7.448	9.163	Opt	85	0
127	0.4	0.1	0.8	0.01	100	0	50	0	0	25	0.281	Opt	1	0
128	0.4	0.1	0.8	0.01	100	100	0	8	8	7.448	10.83	Opt	130	0
129	0.4	0.2	0.6	0.005	0	100	0	7	7	4.798	4.687	Opt	10	0
130	0.4	0.2	0.6	0.005	50	100	0	7	7	4.798	6.379	Opt	6	0
131	0.4	0.2	0.6	0.005	100	0	50	0	0	30	0.271	Opt	1	0
132	0.4	0.2	0.6	0.005	100	100	0	7	7	4.798	9.473	Opt	92	0
133	0.4	0.2	0.6	0.01	0	100	0	7	7	8.196	9.504	Opt	61	0
134	0.4	0.2	0.6	0.01	50	100	0	7	7	8.196	7.901	Opt	15	0
135	0.4	0.2	0.6	0.01	100	0	50	0	0	30	0.281	Opt	1	0
136	0.4	0.2	0.6	0.01	100	100	0	7	7	8.196	10.04	Opt	43	0
137	0.4	0.2	0.8	0.005	0	100	0	7	7	4.798	7.431	Opt	73	0
138	0.4	0.2	0.8	0.005	50	100	0	7	7	4.798	10.7	Opt	123	0
139	0.4	0.2	0.8	0.005	100	0	50	0	0	30	0.291	Opt	1	0
140	0.4	0.2	0.8	0.005	100	100	0	7	7	4.798	12.62	Opt	145	0
141	0.4	0.2	0.8	0.01	0	100	0	7	7	8.196	11.12	Opt	105	0
142	0.4	0.2	0.8	0.01	50	100	0	7	7	8.196	8.712	Opt	53	0
143	0.4	0.2	0.8	0.01	100	0	50	0	0	30	0.291	Opt	1	0
144	0.4	0.2	0.8	0.01	100	100	0	7	7	8.196	9.453	Opt	70	0

As mentioned earlier, each set of four consecutive rows represents a single instance with varying number of shared and dedicated facilities. The first, second and fourth rows of each instance correspond to having 0%, 50%, and 100% dedicated facilities respectively. As expected, we notice that the objective function potentially increases (and never decreases) from the first to the second row and from the second to the fourth row. The third row is always solved instantaneously since each customer is assigned to the dedicated facility on-site.

Among the four major factors being considered in this DOE ( $f_i$ ,  $h_i$ ,  $\alpha_r$ , and  $d_j$ ), an overview of the results shows that that when fixed cost increases, fewer dedicated facilities are opened, and when holding cost increases, fewer dedicated facilities are opened (Figure 2). However, the effect of increasing fixed cost at dedicated facilities is analogous to increasing holding cost since they are summed up together in the objective function coefficient.

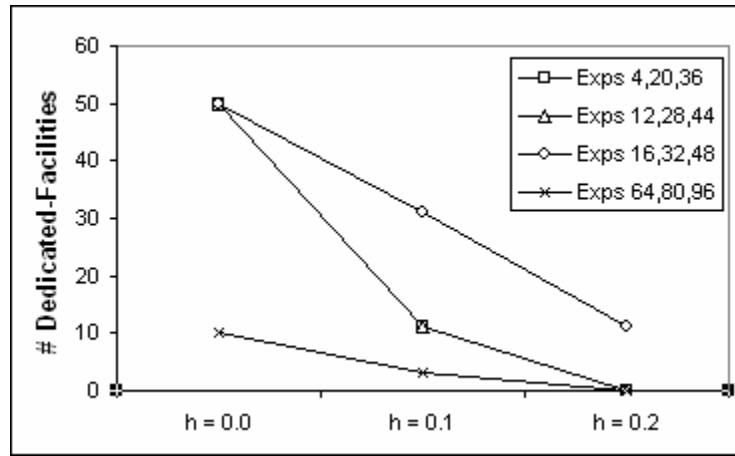


Figure 2. Effect of holding cost on the number of dedicated facilities opened

The effect of the target service level does not seem to be significant. In each of the 144 experimental settings, an increase in the target service level did not change the number of

dedicated facilities opened. Note that we assume all customer-accounts have the same target service level to obtain comparable results across experiments.

On the other hand, demand seems to be the most significant factor in the number of opened dedicated facilities. Many more dedicated facilities are opened when customer demand is relatively high (Figure 3). Again, note that we assume all customers have the same demand rate. Initially we ran the experiments with demand varying across customers, but the results were comparable to the case with constant demand across all customers. Keeping the demand constant across all customers also helps to eliminate any unusual behavior in the results due to randomness.

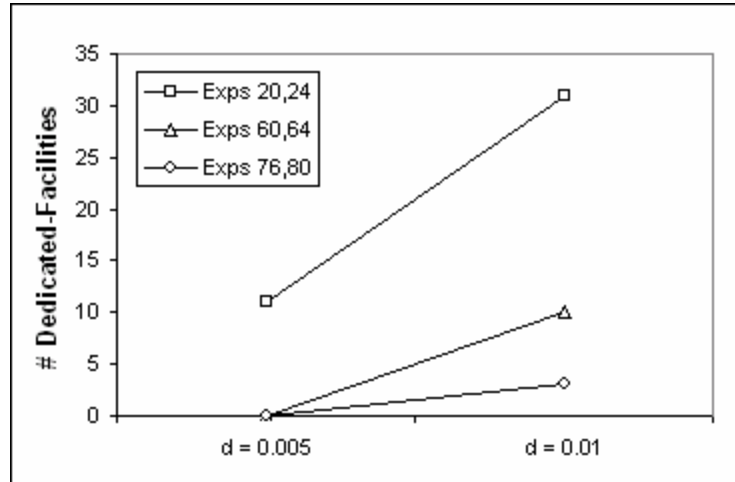


Figure 3. Effect of demand on the number of dedicated facilities opened

### *Effect of network density*

Another important observation is that the benefit of the inclusion of dedicated facilities depends on the density of the network. Suppose we define the density of the network ( $\rho$ ) as the average number of customers within the time window of any given customer.

$$\rho = \frac{\sum_{j \in J} v_j}{n} \quad (2.10)$$

where  $v_j$  is the number of other customers within the time window of customer  $j$ . Figure 4 and Figure 5 show networks with low and high densities respectively, and green circles are drawn around those dedicated facilities that are opened in the optimal solution. These results correspond to experiment 56 in the DOE table.

The network in Figure 4 has a density of 18.72 customers. In this network, the optimal solution chooses 10 dedicated facilities. On the other hand, the network in Figure 5 has a density as high as 26.04 customers, and the optimal solution chooses only 4 dedicated facilities. This leads us to believe that dedicated facilities are more helpful in low density networks.

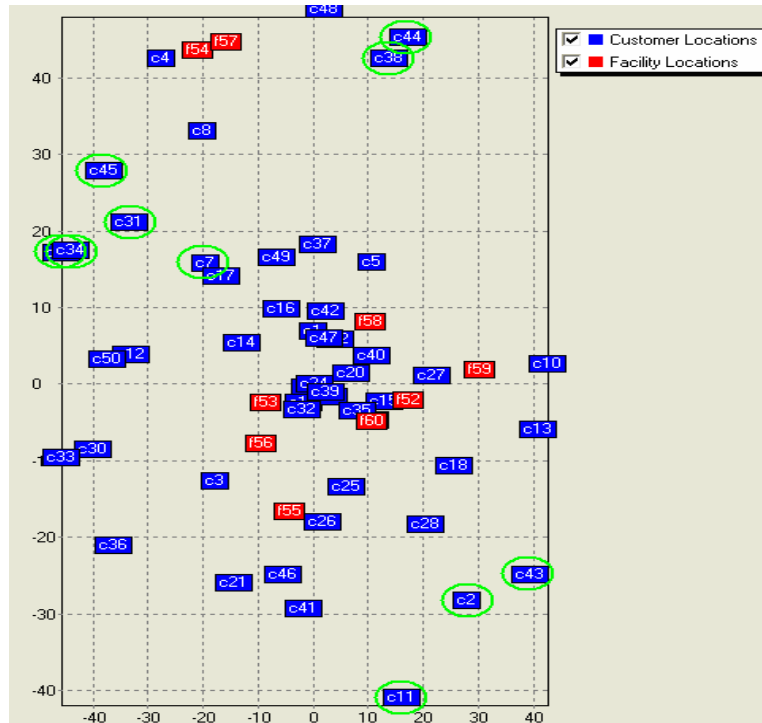


Figure 4. Low density network



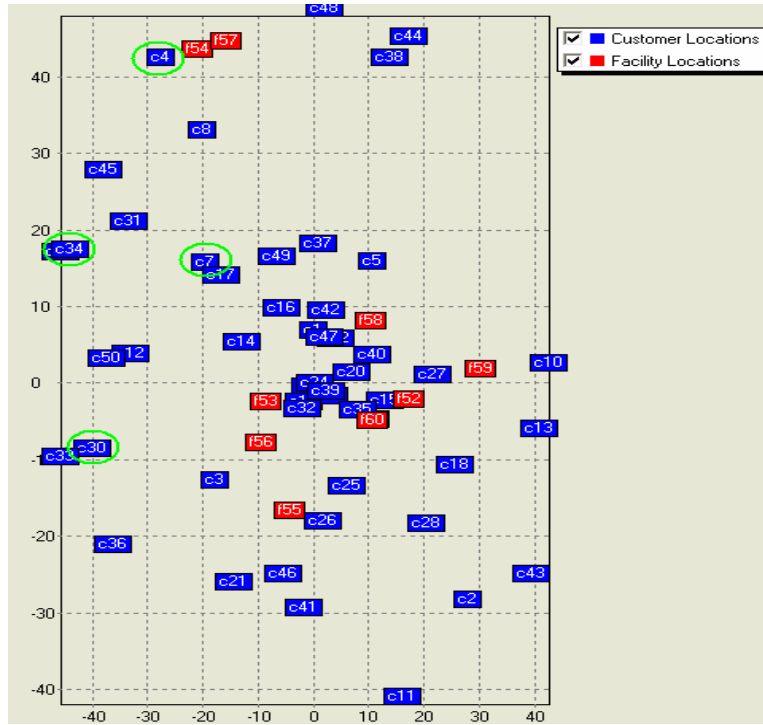


Figure 5. High density network

In order to test this hypothesis, we ran the DOE for the high density network. Appendix C shows the complete table of results. The optimal solution for the low density network had more dedicated facilities than that of the high density network in 20 out of 144 parameter combinations. We did not observe any cases where the optimal solution for the high density network chose to open more dedicated facilities than the corresponding low density network.

Therefore, in addition to low holding cost parameters and high demand values, low network density is another system parameter that encourages the opening of dedicated facilities.

### ***Improvement in solution time***

The inclusion of dedicated facilities in the decision making process can sometimes help reduce solution time as well. Figure 6 shows some cases in which this phenomena is observed.

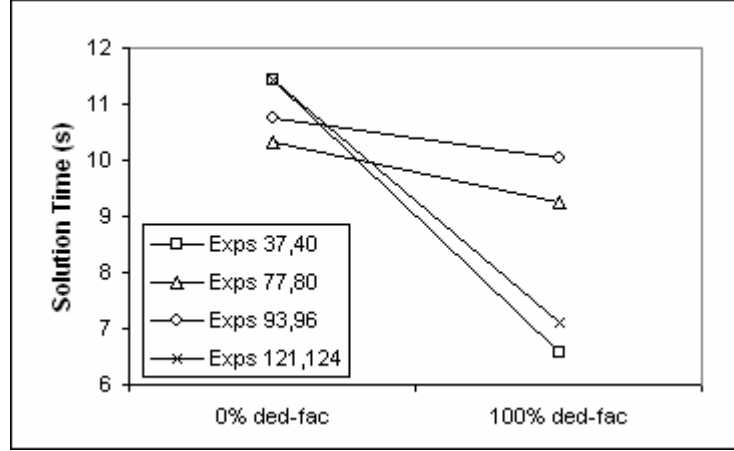


Figure 6. Effect of number of potential dedicated facility locations on solution time

This is primarily due to the result observed in Theorem 2.1. In a pre-processing step, the solver identifies those dedicated facilities that will have to remain open in any optimal solution, thus handling the part of the service level constraint in the preprocessing stage. As a result, the remaining problem is simplified and can be solved in less time.

### ***System-wide Vs Customer-centric service levels***

In order to gain more insight into problem, we ran two more scenarios of the problem while varying the number of customer-accounts. Experimental results with  $|R|=1$  and  $R=J$  are given in Appendix D and Appendix E respectively.

As we vary customer-accounts, we notice that the customer centric model ( $R=J$ ) always opens at least as many dedicated facilities as in the system-wide case ( $|R|=1$ ). The fact that dedicated facilities provide a 100% fill rate intuitively supports this result.

Another interesting result is that sometimes a dedicated facility is opened at a customer site although there exists an open and stocked shared facility within the time window. Figure 7 shows that a dedicated facility is opened on-site of customer ‘7’ although customer ‘7’ is only 22.04 time units away from opened and stocked shared facility ‘53’.

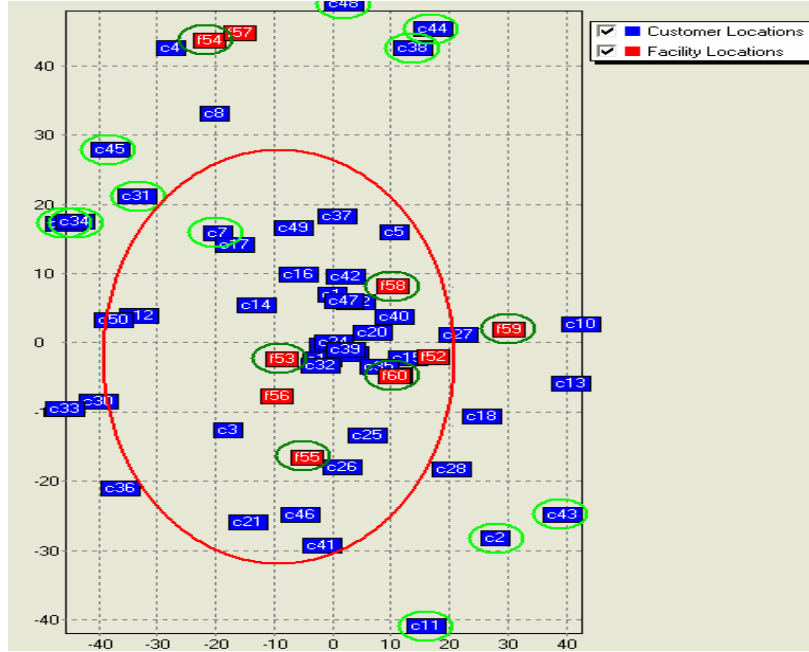


Figure 7. Dedicated facility opened within time window of an open shared facility

This could happen when the solver tries to avoid overshooting the service level constraint. In other words, if some other customer (not within the time window of an open and stocked shared facility) were to be assigned a dedicated facility, then this customer would have a 100% service, and customer ‘7’ will still have positive service, thus overshooting the target service level.

As a final step in this section, we ran a DOE to validate the first and second special cases in Table 1. The DOE results can be seen in Table 4 and Table 5.

Table 4. DOE results for first special case in Table 1

INPUT				OUTPUT			
$f_i$	$h_i$	$\alpha$	$d_j$	# ded	Obj Val	Sol Time	Status
0	0	0.6	0.005	50	0	1.592	Opt
0	0	0.6	0.01	50	0	0.06	Opt
0	0	0.8	0.005	50	0	0.06	Opt
0	0	0.8	0.01	50	0	0.07	Opt
0	0.1	0.6	0.005	30	3	0.11	Opt
0	0.1	0.6	0.01	30	3	0.08	Opt
0	0.1	0.8	0.005	40	4	0.081	Opt
0	0.1	0.8	0.01	40	4	0.08	Opt
0	0.2	0.6	0.005	30	6	0.08	Opt
0	0.2	0.6	0.01	30	6	0.08	Opt
0	0.2	0.8	0.005	40	8	0.08	Opt
0	0.2	0.8	0.01	40	8	0.08	Opt
0.2	0	0.6	0.005	30	6	0.08	Opt
0.2	0	0.6	0.01	30	6	0.07	Opt
0.2	0	0.8	0.005	40	8	0.07	Opt
0.2	0	0.8	0.01	40	8	0.061	Opt
0.2	0.1	0.6	0.005	30	9	0.07	Opt
0.2	0.1	0.6	0.01	30	9	0.07	Opt
0.2	0.1	0.8	0.005	40	12	0.08	Opt
0.2	0.1	0.8	0.01	40	12	0.07	Opt
0.2	0.2	0.6	0.005	30	12	0.07	Opt
0.2	0.2	0.6	0.01	30	12	0.07	Opt
0.2	0.2	0.8	0.005	40	16	0.07	Opt
0.2	0.2	0.8	0.01	40	16	0.07	Opt
0.4	0	0.6	0.005	30	12	0.07	Opt
0.4	0	0.6	0.01	30	12	0.071	Opt
0.4	0	0.8	0.005	40	16	0.07	Opt
0.4	0	0.8	0.01	40	16	0.07	Opt
0.4	0.1	0.6	0.005	30	15	0.06	Opt
0.4	0.1	0.6	0.01	30	15	0.07	Opt
0.4	0.1	0.8	0.005	40	20	0.07	Opt
0.4	0.1	0.8	0.01	40	20	0.07	Opt
0.4	0.2	0.6	0.005	30	18	0.07	Opt
0.4	0.2	0.6	0.01	30	18	0.07	Opt
0.4	0.2	0.8	0.005	40	24	0.071	Opt
0.4	0.2	0.8	0.01	40	24	0.07	Opt

Table 5. DOE results for second special case in Table 1

INPUT				OUTPUT									
$h_i$	$c_{i,j}$	$\alpha$	$d_j$	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status
0	0	0.6	0.005	50	0	50	0	0	0	0	0	0.08	Opt
0	0	0.6	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0	0	0.8	0.005	50	0	50	0	0	0	0	0	0.06	Opt
0	0	0.8	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0	1	0.6	0.005	50	0	50	0	0	0	0	0	0.06	Opt
0	1	0.6	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0	1	0.8	0.005	50	0	50	0	0	0	0	0	0.06	Opt
0	1	0.8	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0	2	0.6	0.005	50	0	50	0	0	0	0	0	0.06	Opt
0	2	0.6	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0	2	0.8	0.005	50	0	50	0	0	0	0	0	0.061	Opt
0	2	0.8	0.01	50	0	50	0	0	0	0	0	0.06	Opt
0.1	0	0.6	0.005	0	1	0	1	0	0	0.1	0.1	0.07	Opt
0.1	0	0.6	0.01	0	1	0	1	0	0	0.1	0.1	0.07	Opt
0.1	0	0.8	0.005	0	1	0	1	0	0	0.1	0.1	0.06	Opt
0.1	0	0.8	0.01	0	1	0	2	0	0	0.2	0.2	0.25	Opt
0.1	1	0.6	0.005	0	1	0	1	0	0.25	0.1	0.35	0.08	Opt
0.1	1	0.6	0.01	0	1	0	1	0	0.5	0.1	0.6	0.081	Opt
0.1	1	0.8	0.005	0	1	0	1	0	0.25	0.1	0.35	0.07	Opt
0.1	1	0.8	0.01	0	1	0	2	0	0.5	0.2	0.7	0.16	Opt
0.1	2	0.6	0.005	0	1	0	1	0	0.5	0.1	0.6	0.08	Opt
0.1	2	0.6	0.01	0	1	0	1	0	1	0.1	1.1	0.11	Opt
0.1	2	0.8	0.005	0	1	0	1	0	0.5	0.1	0.6	0.09	Opt
0.1	2	0.8	0.01	0	1	0	2	0	1	0.2	1.2	0.171	Opt
0.2	0	0.6	0.005	0	1	0	1	0	0	0.2	0.2	0.08	Opt
0.2	0	0.6	0.01	0	1	0	1	0	0	0.2	0.2	0.08	Opt
0.2	0	0.8	0.005	0	1	0	1	0	0	0.2	0.2	0.07	Opt
0.2	0	0.8	0.01	0	1	0	2	0	0	0.4	0.4	0.15	Opt
0.2	1	0.6	0.005	0	1	0	1	0	0.25	0.2	0.45	0.08	Opt
0.2	1	0.6	0.01	0	1	0	1	0	0.5	0.2	0.7	0.08	Opt
0.2	1	0.8	0.005	0	1	0	1	0	0.25	0.2	0.45	0.07	Opt
0.2	1	0.8	0.01	0	1	0	2	0	0.5	0.4	0.9	0.151	Opt
0.2	2	0.6	0.005	0	1	0	1	0	0.5	0.2	0.7	0.08	Opt
0.2	2	0.6	0.01	0	1	0	1	0	1	0.2	1.2	0.08	Opt
0.2	2	0.8	0.005	0	1	0	1	0	0.5	0.2	0.7	0.08	Opt
0.2	2	0.8	0.01	0	1	0	2	0	1	0.4	1.4	0.16	Opt

From Table 4 and Table 5, we see that these problems are solved instantaneously. This supports the theoretical result in Table 1 that these special cases are significantly easier to solve than the general case. We mentioned earlier that the second special case is easy to solve. In the next section, we will explain this in detail.

## **5 Extension – benefit of risk pooling**

The second special case in Table 1 can be used to assess the benefits of risk pooling in SPL. In this section, we formulate this special case and define conditions for which complete centralization and complete decentralization are optimal. Computational results show that the range of cost parameter values within which partial decentralization is optimal is very small. As a result, in most cases the optimal solution is either close to complete decentralization or close to complete centralization. Finally, we develop an algorithm that evaluates a small set of solutions that form an efficient frontier over the rest of the feasible solutions.

The general benefit of risk pooling has been extensively studied in the literature. Schwarz (1989) analyzes the benefit of risk pooling in terms of the lead time values for complete centralization versus complete decentralization. His main conclusion was that the degree of benefit of risk pooling is highly dependent on the pipeline inventory holding cost when inventory is completely centralized. As the pipeline inventory holding cost decreases, the benefit of risk pooling increases.

Xu and Evers (2003) prove that partial centralization can never be better than complete centralization based on demand correlation alone. However, transportation cost and lead times may favor partial centralization. Das and Tyagi (1997) develop an optimization model to analyze the optimal degree of centralization while balancing transportation and inventory costs.

In production-inventory systems, Kim and Benjaafar (2002) show that the benefit of pooling is sensitive to the utilization of the production system and the variability in demand and production times. Counter to intuition, the benefit of pooling is minimal when utilization of the production system is high and/or the variability in demand and production times is high.

Wong et al. (2005a) use Markov chains to obtain computational results on the benefits of pooling repairable service parts. Stocking decisions are then made by minimizing the inventory holding cost, downtime cost, and transshipment costs (Wong et al. (2005b)). In this section, we provide results similar to those of Das and Tyagi (1997), but in the context of service parts, in which demand is very low, inventory is replenished through a base stock policy, and a time-based service level must be satisfied.

### 5.1 Notation/Assumptions

As mentioned in Table 1, in this special case we assume that there exists one shared facility ( $|I''|=1$ ), and every customer is a potential dedicated facility ( $I'=J$ ) and is within the time window of the shared facility ( $\delta_{i'j}=1 \ \forall j$ ). Each customer has a demand of  $d$  units and is subject to a transportation cost of  $c$  per unit demand (if assigned to the shared facility). The holding cost is  $h$  at the shared and dedicated facilities. In order to isolate the effects of inventory cost and transportation cost on risk pooling, we assume that shared and dedicated facilities can be opened at no cost ( $f_{i'}=0 \ \forall i', f_{i''}=0 \ \forall i''$ ). Furthermore, we allow all customers to be assigned to the central warehouse.

Let  $N = \sum_{i' \in I'} Y_{i'}$  be the number of dedicated facilities to be opened, let  $S = \sum_{i'' \in I''} S_{i''}$  be the (base) stock level at the shared facility (note that the set of shared facilities  $I''$  has only one element), and let  $n$  be the total number of customers. Since all customers are within the time window, we can write the service level constraint as

$$Nd + \beta(S, (n-N)d)(n-N)d \geq \alpha nd \quad (2.6h''')$$

where  $\lambda = (n-N)d$  is the mean demand during lead time at the shared facility when  $N$  of the customers are served by dedicated facilities.

## 5.2 Reduced formulation

Assuming that capacity  $s_{\max}$  is large enough to handle all the demand at the shared facility, we now formulate the optimization model as follows:

**P<sub>2'''</sub>**: Minimize

$$z(N, S) = (n - N)cd + (N + S)h = (h - cd)N + hS + ncd \quad (2.6a''')$$

subject to

$$N + \beta(S, (n - N)d)(n - N) \geq \alpha n \quad (2.6h''')$$

$$N \in \{0, 1, \dots, n\} \quad (2.6k''')$$

$$S \in \{0, 1, \dots, s_{\max}\}. \quad (2.6m')$$

Dividing  $z(N, S)$  by the constant  $cd$ , the proportional objective function is  $\left(\frac{h}{cd} - 1\right)N + \frac{h}{cd}S + nh$ . Therefore, the value of ratio  $h/cd$  plays a significant role in controlling the decision of centralization versus decentralization. Lower  $h/cd$  values favor decentralization, whereas centralization becomes increasingly favorable as this ratio increases.

## 5.3 Theoretical results

An important observation is that the service level function for a fixed stock level is non-decreasing with respect to the number of dedicated facilities. In order to prove this, let us define  $f(S, N) = N + \beta(S, (n - N)d)(n - N)$  as the left hand side of the constraint for given stock level  $S$  at the shared facility and number of dedicated facilities,  $N$ .

**Theorem 2.2.** *For a given value of  $S$ ,  $f$  is a monotonically non-decreasing function in  $N$ , i.e.  $f(S, N+1) - f(S, N) \geq 0$ .*

**Proof:**

We have  $f(S, N) = N + \beta(S, (n - N)d)(n - N)$  and



$$f(S, N+1) = (N+1) + \beta(S, (n-(N+1))d)(n-(N+1)).$$

Therefore,

$$\begin{aligned} f(S, N+1) - f(S, N) &= 1 + \beta(S, (n-N-1)d)(n-N-1) - \beta(S, (n-N)d)(n-N) \\ &= 1 + (n-N)(\beta(S, (n-N-1)d) - \beta(S, (n-N)d)) - \beta(S, (n-N-1)d) \end{aligned}$$

But for a given stock level  $S$ , fill rate increases as mean demand decreases. Hence,

$$(\beta(S, (n-N-1)d) - \beta(S, (n-N)d)) \geq 0.$$

Since  $N \leq n$ ,

$$(n-N)(\beta(S, (n-N-1)d) - \beta(S, (n-N)d)) \geq 0.$$

Adding '1' to both sides,

$$1 + (n-N)(\beta(S, (n-N-1)d) - \beta(S, (n-N)d)) \geq 1.$$

Since the fill rate function is a proportion (between 0 and 1),

$$1 + (n-N)(\beta(S, (n-N-1)d) - \beta(S, (n-N)d)) - \beta(S, (n-N-1)d) \geq 0.$$

Hence,  $f(S, N+1) - f(S, N) \geq 0$ . ■

The implication of Theorem 2.2 is that for each stock level at the shared facility, we can now calculate the number of dedicated facilities required to satisfy the target service level (Corollary 2.1). Let  $\bar{S}$  be the stock level required at the shared facility to satisfy the demand of all the customers while maintaining the target service level;  $\bar{S} = \min_{S \in \{0,1,\dots\}} \{S : \beta(S, nd) \geq \alpha\}$ . The associated solution represents stocking  $\bar{S}$  at the shared facility without any dedicated facilities, hence “complete centralization” with total cost of  $h\bar{S} + ncd$ . In comparison, suppose  $S$  ( $< \bar{S}$ ) units are stocked at the shared facility, let  $\hat{N}_S$  be the smallest number of dedicated facilities that need to be opened in order to maintain the target service level, and let  $\hat{\lambda}_S$  be the corresponding mean demand at the shared facility.

**Corollary 2.2.1.** For a given value of  $S$ ,  $\hat{N}_S = n - \lfloor \hat{\lambda}_S / d \rfloor$  where

$$\hat{\lambda}_S = \max_{\lambda \leq nd} \{ \lambda : \lambda(1 - \beta(S, \lambda)) \leq nd(1 - \alpha) \}.$$

**Proof:**

By definition,  $\lambda = (n - N)d$ . Therefore, for a given value of  $S$ ,  $\hat{\lambda}_S = (n - \hat{N}_S)d$ .

Rearranging the terms, the value of  $\hat{N}_S$  is

$$\hat{N}_S = n - \left\lfloor \frac{\hat{\lambda}_S}{d} \right\rfloor$$

since  $\hat{N}_S$  is defined as the smallest number of dedicated facilities that need to be opened.

Now, in order for equation (13) to be satisfied, we require

$$\hat{N}_S + \beta(S, (n - \hat{N}_S)d)(n - \hat{N}_S) \geq \alpha n.$$

Multiplying across by  $-d$  and adding  $nd$  to both sides,

$$nd - \hat{N}_S d - \beta(S, (n - \hat{N}_S)d)(n - \hat{N}_S)d \leq nd - \alpha nd.$$

Substituting  $\hat{\lambda}_S = (n - \hat{N}_S)d$ ,

$$\hat{\lambda}_S (1 - \beta(S, \hat{\lambda}_S)) \leq nd(1 - \alpha).$$

Again, since  $\hat{N}_S$  is defined as the smallest number of dedicated facilities that need to be

opened,  $\hat{\lambda}_S$  should be as large as possible. However,  $\lambda \leq nd$  is an upper bound on

$\hat{\lambda}_S \forall S \in \{0, 1, \dots, \bar{S}\}$ . Therefore,

$$\hat{\lambda}_S = \max_{\lambda \leq nd} \{ \lambda : \lambda(1 - \beta(S, \lambda)) \leq nd(1 - \alpha) \}. \blacksquare$$

For given system parameters  $(\alpha, n, d)$ , and cost parameters  $(h, c)$ , we now find conditions favoring centralization and decentralization.

**Theorem 2.3.** *Sufficient optimality conditions.*

- (a) Complete decentralization  $(S^* = 0, N^* = n)$  is optimal if  $\frac{h}{cd} \leq 1$ .
- (b)  $(S^* = 0, N^* = \lceil \alpha n \rceil)$  is optimal if  $1 < \frac{h}{cd} \leq \min_{k \in \{1, 2, \dots, \bar{S}\}} \left\{ \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k} \right\}$ .
- (c) Complete centralization  $(S^* = \bar{S}, N^* = 0)$  is optimal if  $\frac{h}{cd} \geq \max_{k \in \{0, 1, \dots, \bar{S}-1\}} \left\{ \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\}$ .

**Proof:**

- (a) Complete decentralization:

The coefficient of  $N$  in the objective function  $z(N, S)$  is negative since  $h - cd \leq 0$ . Therefore, the optimal solution is to set  $S = 0$  and  $N = n$ .

- (b) If  $1 < \frac{h}{cd} \leq \min_{k \in \{1, 2, \dots, \bar{S}\}} \left\{ \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k} \right\}$ , then for every  $k \in \{1, \dots, \bar{S}\}$  we have

$$\frac{h}{cd} \leq \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k}.$$

Multiplying both sides by  $cd(\lceil \alpha n \rceil - \hat{N}_k - k)$ ,

$$h(\lceil \alpha n \rceil - \hat{N}_k - k) \leq cd(\lceil \alpha n \rceil - \hat{N}_k).$$

Rearranging the terms,

$$(h - cd)\lceil \alpha n \rceil \leq (h - cd)\hat{N}_k + hk.$$

This can be rewritten as,

$$(h - cd)\lceil \alpha n \rceil + h(0) \leq (h - cd)\hat{N}_k + hk.$$

The left hand side of the last inequality is  $z(\lceil \alpha n \rceil, 0)$ . Since this holds for all  $k$  under the condition, the optimal solution is to set  $S = 0$  and  $N = \lceil \alpha n \rceil$ .

(c) *Complete centralization:*

If  $\frac{h}{cd} \geq \max_{k \in \{0, 1, \dots, \bar{S}-1\}} \left\{ \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\}$ , then for every  $k \in \{0, \dots, \bar{S}-1\}$  we have

$$\frac{h}{cd} \geq \frac{\hat{N}_k}{\hat{N}_k - \bar{S} + k}.$$

Multiplying both sides by  $cd(\hat{N}_k - \bar{S} + k)$ ,

$$h(\hat{N}_k - \bar{S} + k) \geq cd\hat{N}_k.$$

Rearranging the terms,

$$(h - cd)\hat{N}_k + hk \geq h\bar{S}.$$

This can be rewritten as,

$$(h - cd)\hat{N}_k + hk \geq (h - cd)(0) + h\bar{S}.$$

The right hand side of the last inequality is  $z(0, \bar{S})$ . Since this holds for all  $k$ , the optimal solution is to set  $S = \bar{S}$  and  $N = 0$ . ■

We can now extend the results from Theorems 2.2 and 2.3 to derive an algorithm for solving the risk pooling problem. The algorithm takes advantage of the fact there are only  $\bar{S} + 1$  feasible solutions worth comparing because they form an efficient frontier over the rest of the feasible solutions (from Theorem 2.2).

***Algorithm for the risk pooling problem***

**Step 1.** If  $\frac{h}{cd} \leq 1$ , then set  $S^* = 0, N^* = n$ . Otherwise, go to step 2.

**Step 2.** Calculate  $\bar{S} = \min_{S \in \{0,1,\dots\}} \{S : \beta(S, nd) \geq \alpha\}$ , and  $\hat{N}_k = n - \lfloor \hat{\lambda}_k / d \rfloor$  for each

$k \in \{0, \dots, \bar{S}\}$ , where  $\hat{\lambda}_S = \max_{\lambda \leq nd} \{\lambda : \lambda(1 - \beta(S, \lambda)) \leq nd(1 - \alpha)\}$ . If

$\frac{h}{cd} \leq \min_{k \in \{1, 2, \dots, \bar{S}\}} \left\{ \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k} \right\}$ , then set  $S^* = 0, N^* = \lceil \alpha n \rceil$ . Otherwise, go to step 3.

**Step 3.** If  $\frac{h}{cd} \geq \max_{k \in \{0, 1, \dots, \bar{S}-1\}} \left\{ \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\}$ , then set  $S^* = \bar{S}, N^* = 0$ . Otherwise go to step 4.

**Step 4:** Among all  $k \in \{0, \dots, \bar{S}\}$ , if  $(k^*, \hat{N}_{k^*})$  is the pair that yields the smallest objective function value, then set  $S^* = k^*, N^* = \hat{N}_{k^*}$ .

#### 5.4 Numerical example

Consider a network of  $n=100$  customers each with demand  $d=0.01$ . For a service level of  $\alpha=95\%$ ,  $\bar{S}=4$  units need to be stocked at the shared facility under the complete centralization policy. Suppose the holding cost is  $h=0.105$  per unit time and transportation cost is  $c=10$  per unit demand, then the ratio  $\frac{h}{cd}=1.05$ . Table 6 shows the calculations required for the solution algorithm.

Table 6: Calculations for algorithm

$S$	$\hat{\lambda}_S$	$\hat{N}_S$	$\frac{\lceil \alpha n \rceil - \hat{N}_S}{\lceil \alpha n \rceil - \hat{N}_S - S}$	$\frac{\hat{N}_S}{\hat{N}_S - (\bar{S} - S)}$	$z(\hat{N}_S, S)$
0	0.05	95	N/A	1.0439	10.475
1	0.25	75	1.0526	1.0416	10.480
2	0.55	45	1.0416	1.0465	10.435
3	0.93	7	1.0352	1.1666	10.350
4	1.00	0	1.0439	N/A	10.420

Given that  $\frac{h}{cd}=1.05$  is greater than 1, complete decentralization is not optimal. Since

$\frac{h}{cd}=1.05$  is also greater than 1.0352 (minimum of fourth column in Table 6), we move

on to step 3 of the algorithm. The maximum value of the fifth column in Table 6 (1.1666) is greater than  $\frac{h}{cd} = 1.05$ . Therefore, in step 4 of the algorithm we identify that  $z(3,7)=10.350$  is the smallest value in column six of Table 6 and hence the optimal solution. Figure 8 is a graphical representation of the solution.

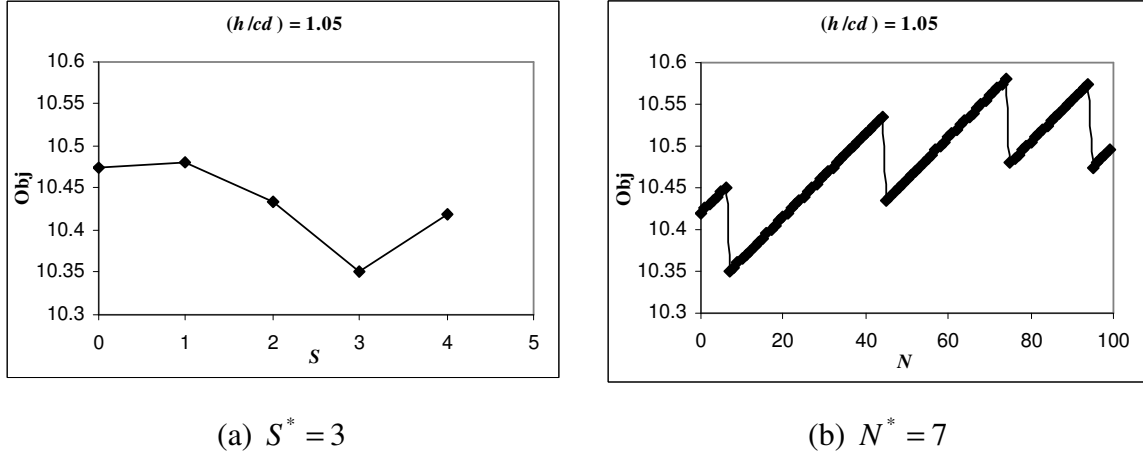


Figure 8. Plots of  $z(\hat{N}_S, S)$  with respect to  $S$  and  $N$

The fact that  $\bar{S} + 1 = 5$  solutions form an efficient frontier over all other feasible solutions can also be seen in Figure 8(b). We can also use this example to illustrate Theorems 2.2 and 2.3. Figure 9 shows the non-decreasing nature of the service level for given  $S$  with respect to  $N$ . In Figure 10, we can see that the objective function curve changes based on the transportation cost and inventory cost parameters.

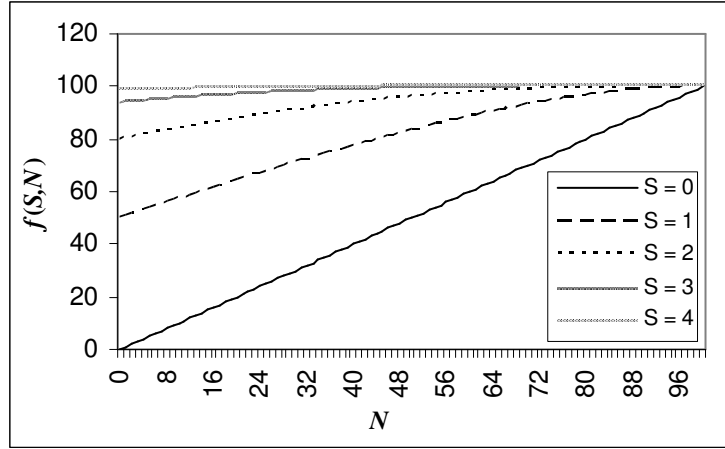


Figure 9. Illustration of Theorem 2.2

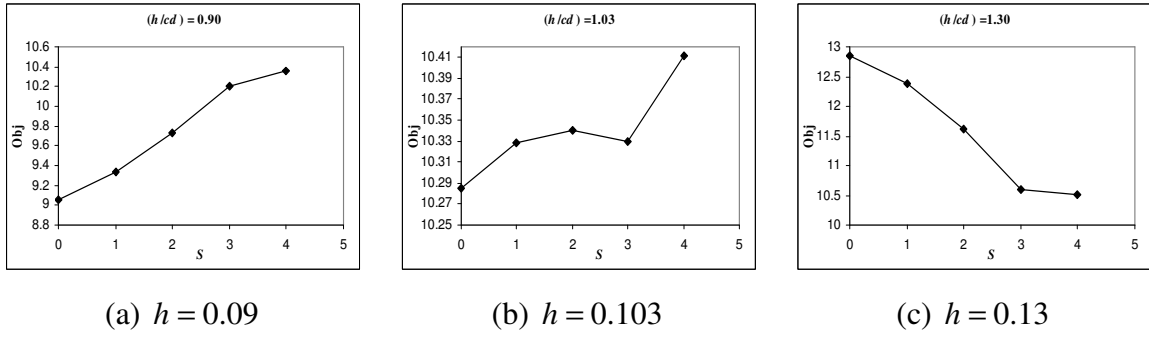


Figure 10. Illustration of Theorem 2.3

Figure 10(a), Figure 10(b), and Figure 10(c) correspond to (a), (b), and (c) in Theorem 2.3. Note that as the  $h/cd$  ratio increases, the optimal solution turns from complete decentralization (Figure 10(a)) to partial decentralization (Figure 10(b) and Figure 8(a)) to complete centralization (Figure 10(c)).

We now test the likelihood that a problem would yield a partially decentralized optimal solution. We know that this occurs only when the  $h/cd$  ratio falls in the interval

$$\left( \min_{k \in \{1, 2, \dots, \bar{S}\}} \left\{ \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k} \right\}, \max_{k \in \{0, 1, \dots, \bar{S}-1\}} \left\{ \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\} \right).$$

Define  $LB = \min_{k \in \{1, 2, \dots, \bar{S}\}} \left\{ \frac{\lceil \alpha n \rceil - \hat{N}_k}{\lceil \alpha n \rceil - \hat{N}_k - k} \right\}$  and  $UB = \max_{k \in \{0, 1, \dots, \bar{S}-1\}} \left\{ \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\}$ , then the size of the  $UB-LB$  gap would give us an idea of the likelihood of partially decentralized optimal solutions.

Consider the experimental design presented in Table 7, with 10 different values of  $n$ ,  $\alpha$ , and  $d$ , each represented as a factor in the design. For each of the 1000 combinations, we calculate the  $LB$  and  $UB$  values (Appendix F). The average gap is 0.033 and the maximum gap is 0.994. Therefore, we can conclude that in most cases, the optimal solution will either be complete centralization or decentralization (with  $N \geq \alpha n$  dedicated facilities).

Table 7. Input system parameters for risk pooling DOE

$n$	$\alpha$	$d$
100	0.75	0.001
200	0.8	0.002
300	0.85	0.003
400	0.9	0.004
500	0.94	0.005
600	0.95	0.006
700	0.96	0.007
800	0.97	0.008
900	0.98	0.009
1000	0.99	0.01

Furthermore, each combination in Table 7 yielded an optimal solution with  $S^* = 0$ ,  $S^* = \bar{S} - 1$ , or  $S^* = \bar{S}$ , regardless of the cost parameters  $h$  and  $c$ . In other words, suppose  $S^* = k$  where  $k \in \{1, 2, \dots, \bar{S} - 2\}$ . This could potentially occur only when  $k$  satisfies  $z(\hat{N}_k, k) < z(\alpha n, 0)$ ,  $z(\hat{N}_k, k) < z(0, \bar{S})$ , and  $z(\hat{N}_k, k) < z(\hat{N}_{\bar{S}-1}, \bar{S} - 1)$ . This can be

rewritten as  $\frac{\alpha n - \hat{N}_k}{\alpha n - \hat{N}_k - k} < \frac{h}{cd} < \min \left\{ \frac{\hat{N}_k - \hat{N}_{\bar{S}-1}}{\hat{N}_k - \hat{N}_{\bar{S}-1} - (\bar{S} - k - 1)}, \frac{\hat{N}_k}{\hat{N}_k - (\bar{S} - k)} \right\}$ . This



interval does not exist for any of the combinations in Table 7, thus resulting in either  $S^* = 0$ ,  $S^* = \bar{S} - 1$ , or  $S^* = \bar{S}$ .

So far in this section, we assume that all the customers are within the time window, and they all have the same demand. This leads us to the result in Theorem 2.2. If we drop these assumptions, then Theorem 2.2 does not necessarily hold.

## 6 Conclusions

In this chapter we allow so-called “dedicated facilities” to be installed at high priority customer locations in an effort to generalize the problem. This enabled us to identify certain special cases of NDIP problem that could be solved as a simple binary knapsack problem, or sometimes even by inspection. Some of this information could be used for pre-processing by variable fixing.

Computational results show us that dedicated facilities become preferable in service parts networks with low holding cost, high demand, and low density of customers. We have also defined specific conditions under which a specific dedicated facility will be opened in any optimal solution. In such cases, the problem with dedicated facilities would solve more quickly than the problem with only shared facilities.

In terms of risk pooling, we obtain boundary conditions on cost parameters beyond which the solution is either complete centralization or complete decentralization. Computational results show that in most cases the gap between the boundary conditions is very small. Moreover, we notice that for such low demand items, the optimal solution turns out to be  $S^* = 0$ ,  $S^* = \bar{S} - 1$ , or  $S^* = \bar{S}$  regardless of the cost parameters.

In the next chapter, we research the idea of inventory sharing so that we can incorporate it into the optimization model.

## **Chapter 3: Inventory Sharing**

An important characteristic of SPL is that parts have high cost but low demand. For that reason, inventory optimization is a thriving research topic in SPL. In this chapter we incorporate the concept of inventory sharing between facilities within the inventory optimization framework with time based service level constraints. This is achieved by first estimating fill rates analytically, followed by a new network design formulation with the inventory sharing fill rates. As an extension, we also identify cases where inventory sharing could be worse than not sharing inventory.

### **1 Literature review**

A recent paper by Burton et al. (2005) showed the superiority of inventory sharing over any other non-sharing policy using a cost parametric analysis. They also showed that ad hoc emergency transshipments are more effective than systematic transshipments based on stock equalization. Moreover, Pyke (1990) also concluded that lateral transshipments have the most impact in the limit when transshipment times go to zero. However, Grahovac et al. (2001) suggested that although inventory sharing may be beneficial from a cost point of view, it may not be favorable for everyone in the supply chain. For example, inventory sharing may reduce holding and shipping costs, but the individual facilities may not be very supportive of fulfilling the demand of other customers which may not count towards their service.

Zhao et al. (2005) further explored this idea from a game theoretic point of view. They allowed each facility to have its own rationing level, which defines the portion of inventory that each facility is willing to share. A Nash equilibrium is guaranteed to exist if each facility attempts to maximize its own service. Rudi et al. (2001) formulated a model that solves for the optimum transshipment prices that induce facilities to make inventory decisions consistent with joint cost minimization.

Modeling inventory of service parts was first explored by Sherbrooke (1968) when he developed the Multi-Echelon Technique for Recoverable Item Control (METRIC) model which could be used to find optimum stock levels to minimize expected backorders subject to the budget. In 1980, Muckstadt et al. extended METRIC to include direct deliveries from the central warehouse by taking advantage of the system structure. Graves (1985) further improved METRIC with his VARI-METRIC model. However, none of these models allowed inventory sharing.

Lee (1987) was the first paper that modeled inventory sharing through lateral transshipments. After dividing facilities among a few pooling groups, he assumed that all the facilities are identical in each pooling group. He also developed an algorithm to solve for optimal stock levels while minimizing holding costs subject to service level constraints. Dropping the assumption of identical facilities in each pooling group, Axsäter (1990) developed a methodology for better results than Lee (1987) assuming exponentially distributed replenishment times. Moynadeh et al. (1991) also modeled a policy for inventory management with lateral transshipments assuming deterministic lead times.

While Lee (1987) and Axsäter (1990) assumed that facilities with no on-hand inventory cannot act as sources for lateral transshipments, Sherbrooke (1992) allowed these facilities to have backordered lateral transshipments. Whenever replenishment from the central warehouse comes in, these facilities laterally transship the orders to the respective facilities that placed the order. Due to the complexity of this model, Sherbrooke (1992) used simulation as a modeling technique, whereas Wong et al. (2005a) developed an analytic model for the same problem.

Dada (1992) further extended the inventory sharing model to allow items in transit to be used for filling orders as well. This was the first model of its kind. Finally Alfredsson and Verrijdt (1999) combined the works of Dada (1992) and Axsäter (1990) to develop

an analytic model that calculates the fraction of demand of a customer satisfied by different sources such as the regular order fills from the assigned facility, lateral transshipments from other facilities, direct shipments from the central warehouse etc. Alfredsson and Verrijdt (1999) concluded that the distribution of shipment times has a negligible effect on the overall model.

A number of papers have been written on variations of these inventory models. Herer et al. (1999) included replenishment costs into the model, and Wong et al. (2005b) included downtime cost but ignore service level constraints in the model. Axsäter (2003) formulated a model to minimize the expected cost assuming that no more lateral transshipments will take place in the future, whereas Aggrawal et al. (1994) completely ignored lateral transshipments and their strategy is production to order. In other words, it is a pull strategy through the supply chain that results in no stock at any of the facilities. While all the above mentioned models are continuous review models, Tagaras (1989) and Archibald et al. (1995) developed periodic review models for the same problem.

In this chapter, we extend the works of Lee (1987) and Alfredsson and Verrijdt (1999). Let us define a “pool” to be a set of stocking facilities that are allowed to share inventory. Then demand occurring at a facility is satisfied in the following order:

- If the facility has stock on-hand, then this on-hand stock is used to satisfy the demand.
- If the facility is out of stock and another facility in the pool has stock on-hand, then demand is satisfied by the other facility.
- If all the facilities in the pool are out of stock, then demand is satisfied by a direct shipment from the central warehouse which has infinite supply. However, this will be counted as a lost sale for the assigned facility.

Note that all the facilities in this chapter are shared facilities, and all of them are replenished from the central warehouse according to the base stock policy.

Lee (1987) analyzed a multiple pool system assuming that all the facilities in a given pool are identical whereas Axsäter (1990) allowed non-identical facilities in the same pool. Later on, Alfredsson and Verrijdt (1999) extended Axsäter's (1990) model by allowing the central warehouse to run out of stock, in which case it will be replenished by the plant, which has infinite supply. They also allowed each facility to share inventory with every other facility (i.e. all facilities belong to the same big pool). A comparison of the three papers is shown in Table 8.

Table 8. Comparison of the relevant papers in inventory sharing

<b>Alfredsson and Verrijdt (1999)</b>	<b>Lee (1987)</b>	<b>This chapter</b>
Supply chain network has four echelons (includes plant)	Supply chain network has three echelons	Supply chain network has three echelons
New parts are produced in the plant	No new parts are produced (parts are recycled)	New parts are distributed from the central warehouse
Base stock replenishment policy	Base stock replenishment policy	Base stock replenishment policy
Unsatisfied demand is lost	Unsatisfied demand is backordered	Unsatisfied demand is lost
Only one pool exists, but facilities within it need not be identical	Many pools exist, but all facilities within a pool are identical	Many pools exist, and all facilities within a pool need not be identical, but only two facilities are allowed in each pool

When we consider inventory sharing between facilities, estimating fill rates becomes a challenge. Alfredsson and Verrijdt (1999) estimated these probabilities iteratively using Markov chains. In this chapter however, we use the low demand nature of spare parts to simplify the Markov chain based iterative formula into a set of simultaneous equations. Furthermore, we incorporate the inventory sharing formulae within the inventory optimization problem with time based service level constraints.

### ***Inventory Optimization Problem***

Consider a network of inventory stocking facilities across the nation. Each existing customer is assigned to a specific stocking facility for spare parts, but the facility should be stocked well enough to satisfy a target service level. The two decision variables here are (1) allocation of customer demand to facilities and (2) stock levels at each facility.

The main trade-off is between the inventory holding cost and the transportation cost. Decreasing the stock level at a facility would reduce the inventory cost, but the fill rate is also reduced. Therefore a customer in close proximity to the facility may have to be reassigned to another facility (at a larger distance) in order to maintain the target service level, which in turn increases the transportation cost. Note that the holding cost is accompanied by the fixed cost of opening and operating the facility.

This problem of minimizing the total inventory cost, fixed cost, and transportation cost subject to a service level constraint is what we call the “inventory optimization problem”. In this problem, the service level constraint ensures that the target service level percentage of total demand is satisfied within a predefined time window.

As mentioned earlier, inventory holding cost per unit is high for spare parts. Therefore, we would like to consider sharing of inventory between facilities such that inventory cost is reduced without much reduction in fill rates.

## **2 Single pool inventory problem with inventory sharing**

In this section we formulate the inventory optimization problem for a single pool of two facilities with inventory sharing between the facilities. In this regard, first we modify the iterative methodology of Alfredsson and Verrijdt (1999) in estimating the local and lateral fill rates for a single pool with two facilities. We then formulate equations to estimate the fill rates (as opposed to using the iterative methodology of Alfredsson and Verrijdt (1999)).

## 2.1 Estimating fill rates

Consider a system of two facilities belonging to the same pool (Figure 11). Suppose  $I = \{1,2\}$  is the set of facilities. At each facility  $i \in I$ , let  $S_i$  denote the stock level and let us redefine  $\lambda_i$  to be the demand “rate” (as opposed to mean demand during lead time in Chapter 2). The fill rates are as follows:

$\beta_i$  -fraction of demand satisfied by on-hand stock at the facility  $i$ ,

$\gamma_i$  -fraction of demand of facility  $i$  satisfied by lateral transshipment from another facility in the pool, and

$\theta$  -fraction of demand satisfied by a direct shipment from the central warehouse (CW).

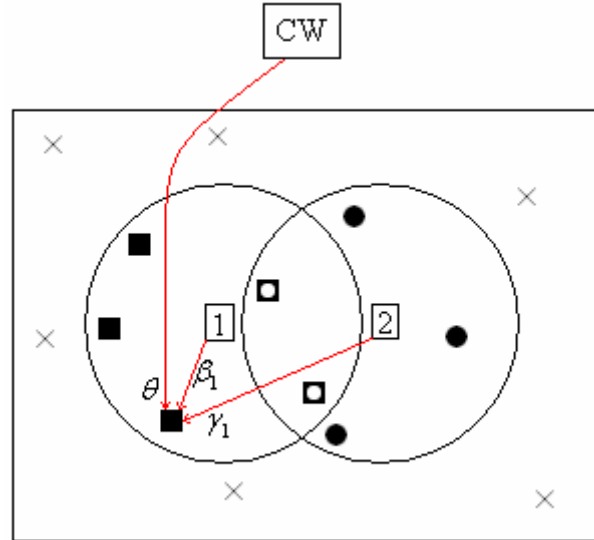


Figure 11. Two facility pool

Note that the customers that are only within the time window of facility 1 are symbolized by “■” in Figure 11, those that are only within the time window of facility 2 are shown as “●”, and the “□” symbols are those customers within the time window of both facilities.

On the other hand, let “x” be those customers that do not fall within the time window of either facility.

Given that a shipment from the central warehouse is required only when the entire pool runs out of inventory, we estimate  $\theta$  using a Markov chain with demand and stock aggregated over the entire pool. Next, the local fill-rate ( $\beta_i$ ) at each facility is estimated using a Markov chain (for each facility) where lateral demand is added to the local demand.

### *Iterative method of estimating fill rates*

Step 1: Estimating  $\theta$ ;

Combine all the facilities within the pool into an aggregate facility with stock level  $\bar{S} = S_1 + S_2$ , replenishment rate  $\mu$  and demand rate  $\bar{\lambda} = \lambda_1 + \lambda_2$ . Suppose  $k$  denotes the on-hand inventory level at the aggregate facility, then let each  $k = 0, 1, \dots, \bar{S}$  be a single state in a continuous time Markov chain as seen in Figure 12.

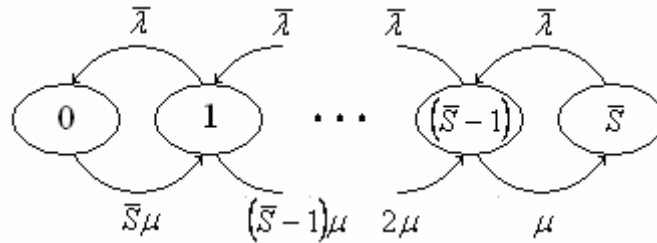


Figure 12. State transition diagram for the pool

We can now obtain the steady state probability that the pool has an aggregate inventory of  $k$  units ( $\pi^k$ ) by solving the following equations:

$$\pi^k = \frac{\bar{S}!}{(\bar{S}-k)!} \left( \frac{\mu}{\bar{\lambda}} \right)^k \pi^0 \quad \forall k = 0, 1, \dots, \bar{S}, \quad (3.1)$$



$$\sum_{k=0}^{\bar{S}} \pi^k = \sum_{k=0}^{\bar{S}} \frac{\bar{S}!}{(\bar{S}-k)!} \left( \frac{\mu}{\bar{\lambda}} \right)^k \pi^0 = 1, \quad (3.2)$$

where equation (3.1) is the rate equation and equation (3.2) is the normalizing equation.

The probability that demand is satisfied by a direct shipment from the central warehouse ( $\theta$ ) is the probability that the entire pool has zero units on-hand in the long run, i.e.,

$$\theta = \pi^0. \quad (3.3)$$

Note that all the facilities in the same pool will have the same value for  $\theta$ .

Step 2: Estimating  $\beta$  and  $\gamma$ ;

Suppose  $e_i$  is the rate of lateral transshipments from the other facility in the pool.

Alfredsson and Verrijdt (1999) approximated  $e_1 = \frac{\gamma_2 \lambda_2}{\beta_1}$  and  $e_2 = \frac{\gamma_1 \lambda_1}{\beta_2}$ , which is

the fraction of demand rate from the other facility conditioned on the probability that the facility has stock on-hand. For any value of  $e_i$ , the long run total demand rate at facility  $i$  is  $\lambda_i + e_i$ . In the long run, the demand process at a facility with lateral transshipments can be approximated as a Poisson process (verified using simulation).

We can now setup another continuous time Markov chain where each state  $l$  corresponds to the on-hand inventory level at facility  $i$  (Figure 13).

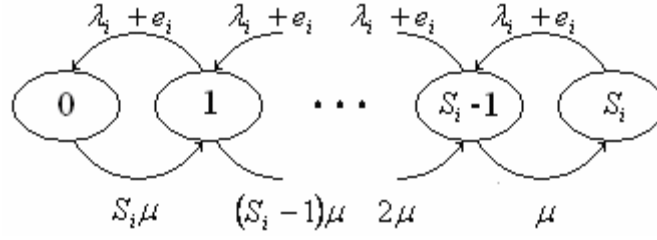


Figure 13. State transition diagram for each facility  $i$

Let  $\phi_i^l$  be the steady state probability that facility  $i$  has  $l$  units of inventory on-hand. The steady state probabilities can be obtained by solving the following equations:

$$\phi_i^l = \frac{S_i!}{(S_i - l)!} \left( \frac{\mu}{\lambda_i + e_i} \right)^l \phi_i^0 \quad \forall l = 0, 1, \dots, S_i, \quad (3.4)$$

$$\sum_{l=0}^{S_i} \phi_i^l = \sum_{l=0}^{S_i} \frac{S_i!}{(S_i - l)!} \left( \frac{\mu}{\lambda_i + e_i} \right)^l \phi_i^0 = 1, \quad (3.5)$$

where equation (3.4) is the rate equation and equation (3.5) is the normalizing equation.

The probability that demand at facility  $i$  is satisfied by on-hand inventory is the probability that the on-hand inventory is greater than 0 in the long run, i.e.,

$$\beta_i = 1 - \phi_i^0. \quad (3.6)$$

We also know that

$$\beta_i + \gamma_i + \theta = 1. \quad (3.7)$$

The above formulae show us that  $e_i$ ,  $\beta_i$ , and  $\gamma_i$  are dependent on each other. Therefore, using  $e_i = 0$  as a starting point, we can now iteratively update the values of  $\beta_i$  and  $\gamma_i$  until they converge.

For example, consider the following two-facility pool (Table 9).

Table 9. Input parameters for iterative estimation of fill rates

	$i = 1$	$i = 2$
$\lambda_i$	0.15	0.2
$S_i$	1	1

Using the input values shown in Table 9 and a replenishment rate of  $\mu = 1$ , we first calculate the probability that the entire pool stocks out, i.e.  $\theta = 0.0434$  (step 1). Based on this, Table 10 shows multiple iterations of step 2.

Table 10. Results by iteration of fill rate estimation

Iteration	$e_i$		$\gamma_i$		$\beta_i$		Gap
	$i = 1$	$i = 2$	$i = 1$	$i = 2$	$i = 1$	$i = 2$	
0	0	0	0.087	0.1233	0.8696	0.8333	0.215075894
1	0.0284	0.0157	0.108	0.134	0.8486	0.8226	0.0263908
2	0.0316	0.0197	0.1103	0.1367	0.8463	0.8199	0.005469977
3	0.0323	0.0202	0.1108	0.137	0.8458	0.8196	0.000775356
4	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	0.000145339
5	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	<b>2.217E-05</b>
6	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	3.93213E-06
7	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	6.24038E-07
8	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	1.07454E-07
9	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	1.7424E-08
10	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	2.95275E-09
11	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	4.8441E-10
12	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	8.13862E-11
13	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	1.3436E-11
14	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	2.24785E-12
15	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	3.72472E-13
16	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	6.20787E-14
17	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	1.1014E-14
18	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	2.00254E-15
19	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	1.00127E-15
20	0.0324	0.0203	0.1109	0.1371	0.8457	0.8195	0

We see that 5 iterations are enough to estimate the values of  $\beta_i$  and  $\gamma_i$  within 0.002 % of the actual values. Therefore, we observe that the iterative procedure of estimating fill

rates converges quickly. However, from an optimization point of view we would like to have analytic equations to estimate  $\beta_i$  and  $\gamma_i$  values.

### *Analytic method of estimating fill rates*

Using equations (3.1), (3.2), and (3.3), we know that

$$\theta = \pi^0 = \frac{1}{\sum_{k=0}^{\bar{S}} \frac{\bar{S}!}{(\bar{S}-k)!} \left(\frac{\mu}{\bar{\lambda}}\right)^k}. \quad (3.8)$$

Combining equations (3.4), (3.5), and (3.6),

$$\begin{aligned} \beta_i &= 1 - \phi_i^0 \\ &= 1 - \frac{1}{\sum_{l=0}^{S_i} \frac{S_i!}{(S_i-l)!} \left(\frac{\mu}{\lambda_i + e_i}\right)^l}. \end{aligned}$$

For a single pool with two facilities,  $e_1 = \frac{\gamma_2 \lambda_2}{\beta_1}$  and  $e_2 = \frac{\gamma_1 \lambda_1}{\beta_2}$  (Alfredsson and Verrijdt (1999)). We now replace the value of  $e_1$  in the formula of  $\beta_1$ , i.e.,

$$\begin{aligned} \beta_1 &= 1 - \frac{1}{\sum_{l=0}^{S_1} \frac{S_1!}{(S_1-l)!} \left(\frac{\mu}{\lambda_1 + e_1}\right)^l} \\ &= 1 - \frac{1}{\sum_{l=0}^{S_1} \frac{S_1!}{(S_1-l)!} \left(\frac{\mu}{\lambda_1 + \frac{\gamma_2 \lambda_2}{\beta_1}}\right)^l}, \end{aligned}$$

and a similar equation can be written for  $\beta_2$ . But we also know that  $\gamma_i = 1 - \beta_i - \theta$  from equation (3.7). Therefore, the values of  $\beta_1$  and  $\beta_2$  can be obtained by simultaneously solving the following equations:

$$\beta_1 + \frac{1}{\sum_{l=0}^{S_1} \frac{S_1!}{(S_1-l)!} \left( \frac{\mu}{\lambda_1 + \frac{(1-\theta-\beta_2)\lambda_2}{\beta_1}} \right)^l} = 1, \quad (3.9)$$

$$\beta_2 + \frac{1}{\sum_{l=0}^{S_2} \frac{S_2!}{(S_2-l)!} \left( \frac{\mu}{\lambda_2 + \frac{(1-\theta-\beta_1)\lambda_1}{\beta_2}} \right)^l} = 1. \quad (3.10)$$

As a verification step, we implemented equations (3.8), (3.9), and (3.10) on the input data from Table 9 in Excel and ensured that we obtained the same values for the fill rates as we did in the iterative procedure. Moreover, we also checked these values with an Arena based simulation model. Note that all the following work in this dissertation is based on the validity of the fill rate approximation. The long run fill rates in the simulation model were the same as those from equations (3.8), (3.9), and (3.10) up to the fifth decimal place.

### ***Special case in SPL***

Due to the low demand nature of spare parts in SPL, let us assume that  $S_i = 1$  is sufficient to satisfy all the demand assigned to facility  $i$ . That is, it is sufficient to consider the stock level at a facility to be 0 or 1. Suppose the lead time is 1 week, then this corresponds to a maximum demand rate of 0.01 per facility per week for 100% service. We continue to hold this assumption for the remainder of this chapter. Based on this assumption, equations (3.9) and (3.10) can be further simplified through a series of algebraic manipulations as shown below. If  $S_1 = 1$ , then

$$\beta_1 = 1 - \frac{1}{\sum_{l=0}^1 \frac{1!}{(1-l)!} \left( \frac{\mu}{\lambda_1 + \frac{\gamma_2 \lambda_2}{\beta_1}} \right)^l}.$$

Expanding the sum and simplifying the fraction we obtain,

$$\beta_1 = \frac{\mu - \gamma_2 \lambda_2}{\mu + \lambda_1} = \frac{\mu - (1 - \beta_2 - \theta) \lambda_2}{\mu + \lambda_1},$$

and similarly if  $S_2 = 1$ , then,

$$\beta_2 = \frac{\mu - \gamma_1 \lambda_1}{\mu + \lambda_2} = \frac{\mu - (1 - \beta_1 - \theta) \lambda_1}{\mu + \lambda_2}.$$

Therefore, if  $S_1 = 1$  and  $S_2 = 1$ , the above equations can be solved simultaneously to obtain the following equations for the fill rates. From equation (3.8),

$$\theta = \frac{\bar{\lambda}^2}{(\bar{\lambda} + \mu)^2 + \mu^2}. \quad (3.8')$$

Inserting  $\theta$  into the simplified versions of equations (3.9) and (3.10),

$$\beta_1 = \frac{\mu(\bar{\lambda}^2 + 2\mu^2 + 2\mu(\lambda_2 + \bar{\lambda}))}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}, \text{ and} \quad (3.9')$$

$$\beta_2 = \frac{\mu(\bar{\lambda}^2 + 2\mu^2 + 2\mu(\lambda_1 + \bar{\lambda}))}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}. \quad (3.10')$$

Replacing  $\theta$  and  $\beta$  in equation (3.7),

$$\gamma_1 = \frac{\mu(\bar{\lambda}^2 + 2\mu\lambda_1)}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}, \text{ and} \quad (3.11)$$

$$\gamma_2 = \frac{\mu(\bar{\lambda}^2 + 2\mu\lambda_2)}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}. \quad (3.12)$$

As a result, under the low demand assumption of SPL, we are able to accurately estimate the fill rates for given demand rates and stock levels in a two-facility pool without iterations.

The fill rate estimation equations assume that we know the demand allocation and the stock levels at each facility. Suppose we do not have this information, and we would like to find the optimal demand allocation and stock levels such that a time based service constraint is satisfied. In order to do this, let us first define some new notation.

## 2.2 Notation/Assumptions

In this chapter, we allow customers to be assigned to facilities with no stock (which was not allowed in Chapter 2). This is because inventory is now shared between facilities. Furthermore, in this chapter we continue to assume that customers cannot be directly assigned to the central warehouse (as in Chapter 2), but there exists a transportation cost component for demand satisfied from the central warehouse when all the facilities in the pool are out of stock.

Suppose  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$  are demand parameters such that  $d_1$  is the total demand rate from customers only within the time window of facility 1,  $d_2$  is the total demand rate from customers only within the time window of facility 2,  $d_0$  is the total demand rate from customers that are within the time window of both facility 1 and facility 2, and  $d_{-1}$  is the total demand rate from customers that are not within the time window of any facility. Referring back to Figure 11,  $d_1$  corresponds to the set of “■” customers,  $d_2$  corresponds to the set of “●” customers,  $d_0$  corresponds to the set of “■” customers, and  $d_{-1}$  corresponds to the set of “×” customers.

Let  $X_{01}$ ,  $X_{11}$ ,  $X_{21}$ ,  $X_{-11}$ ,  $X_{02}$ ,  $X_{22}$ ,  $X_{12}$ ,  $X_{-12}$  be demand allocation variables where

$X_{01}$  – demand within the time window of both facilities assigned to facility 1

- $X_{11}$  – demand within the time window of facility 1 assigned to facility 1
- $X_{21}$  – demand within the time window of facility 2 assigned to facility 1
- $X_{-11}$  – demand outside the time window of both facilities assigned to facility 1
- $X_{02}$  – demand within the time window of both facilities assigned to facility 2
- $X_{22}$  – demand within the time window of facility 2 assigned to facility 2
- $X_{12}$  – demand within the time window of facility 1 assigned to facility 2
- $X_{-12}$  – demand outside the time window of both facilities assigned to facility 2

In other words,  $d_1 = X_{11} + X_{12}$ ,  $d_2 = X_{21} + X_{22}$ ,  $d_0 = X_{01} + X_{02}$ , and  $d_{-1} = X_{-11} + X_{-12}$ .

An illustration of the notation can be seen in Figure 14.

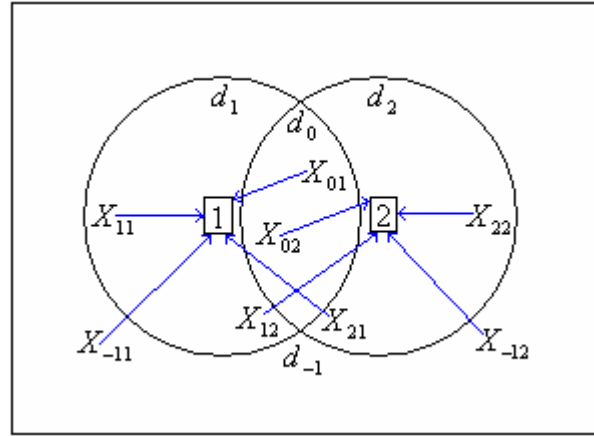


Figure 14. Demand allocation variables in the two facility pool

With a fixed cost of  $f$  to open and operate a facility per unit time (say 1 week), and a unit holding cost of  $h$  per unit time, suppose we have the following additional cost parameters:  $c^{in}$  is the unit transportation cost of demand satisfied within the time window of a facility,  $c^{out}$  is the unit transportation cost of demand satisfied outside the time window of the facility, and  $c^e$  is the transportation cost of demand satisfied as an



emergency shipment from the central warehouse. Note that we inherently assume that  $c^{in} \leq c^{out}$ .

### 2.3 Formulation of a single two-facility pool problem

A breakdown of the total cost is given as follows:

$$\text{Fixed cost and Inventory cost} = (f + h)(S_1 + S_2)$$

$$\begin{aligned} \text{Local transportation cost} &= c^{in} \beta_1(X_{01} + X_{11}) + c^{out} \beta_1(X_{21} + X_{-11}) \\ &\quad + c^{in} \beta_2(X_{02} + X_{22}) + c^{out} \beta_2(X_{12} + X_{-12}) \end{aligned}$$

$$\begin{aligned} \text{Lateral transportation cost} &= c^{in} \gamma_1(X_{01} + X_{21}) + c^{out} \gamma_1(X_{11} + X_{-11}) \\ &\quad + c^{in} \gamma_2(X_{02} + X_{12}) + c^{out} \gamma_2(X_{22} + X_{-12}) \end{aligned}$$

$$\begin{aligned} \text{Emergency transportation cost} &= c^e \theta (X_{01} + X_{11} + X_{21} + X_{-11} + X_{02} + X_{22} + X_{12} + X_{-12}) \\ &= c^e \theta \bar{\lambda} \end{aligned}$$

Note that the total cost function is different from that of Chapter 2. Now that we allow inventory sharing, we need to know where the part actually comes from (as opposed to just knowing which facility the customer is assigned to).

The proportion of satisfied demand that falls within the time window is

$$\beta_1(X_{01} + X_{11}) + \gamma_1(X_{01} + X_{21}) + \beta_2(X_{02} + X_{22}) + \gamma_2(X_{02} + X_{12}).$$

Suppose we require  $\alpha$  of the total pool demand to be satisfied within the time window. We can now formulate an optimization problem that minimizes the total cost subject to a time based service level constraint.

**P<sub>3</sub>:** Minimize

$$\begin{aligned} z(S_1, S_2) &= (f + h)(S_1 + S_2) \\ &\quad + c^{in} \beta_1(X_{01} + X_{11}) + c^{out} \beta_1(X_{21} + X_{-11}) + c^{in} \beta_2(X_{02} + X_{22}) + c^{out} \beta_2(X_{12} + X_{-12}) \\ &\quad + c^{in} \gamma_1(X_{01} + X_{21}) + c^{out} \gamma_1(X_{11} + X_{-11}) + c^{in} \gamma_2(X_{02} + X_{12}) + c^{out} \gamma_2(X_{22} + X_{-12}) \end{aligned}$$

$$+c^e\theta\bar{\lambda} \quad (3.13a)$$

subject to

$$\begin{aligned} u(S_1, S_2) &= \beta_1(X_{01} + X_{11}) + \gamma_1(X_{01} + X_{21}) \\ &+ \beta_2(X_{02} + X_{22}) + \gamma_2(X_{02} + X_{12}) \geq \alpha\bar{\lambda} \end{aligned} \quad (3.13b)$$

$$d_1 = X_{11} + X_{12} \quad (3.13c)$$

$$d_2 = X_{21} + X_{22} \quad (3.13d)$$

$$d_0 = X_{01} + X_{02} \quad (3.13e)$$

$$d_{-1} = X_{-11} + X_{-12} \quad (3.13f)$$

$$X_{01}, X_{11}, X_{21}, X_{-11}, X_{02}, X_{22}, X_{12}, X_{-12} \geq 0 \quad (3.13g)$$

$$S_1, S_2 \in \{0, 1, 2, \dots\}. \quad (3.13h)$$

where the fill rates  $\theta, \beta_1, \beta_2, \gamma_1$ , and  $\gamma_2$  are estimated based on equations (3.7), (3.8), (3.9), and (3.10).

## 2.4 Theoretical results

Problem **P<sub>3</sub>** is a non-linear integer optimization problem, however the low demand nature of SPL enables us to simplify the problem. In fact, if we limit  $S_1, S_2 \in \{0, 1\}$  then the entire problem has a trivial solution (can be solved by inspection). The following theorems build up a case to prove this claim.

**Theorem 3.1:** *If  $S_1, S_2 \in \{0, 1\}$  and  $d_1 \geq d_2$ , then the solution to problem **P<sub>3</sub>** is either  $(S_1, S_2) = (1, 0)$  or  $(S_1, S_2) = (1, 1)$ .*

**Proof:** The possible solutions to  $(S_1, S_2)$  are  $(0, 0)$ ,  $(0, 1)$ ,  $(1, 0)$ , and  $(1, 1)$ . Assuming that  $\alpha > 0$ , we can eliminate  $(0, 0)$  as a solution.

In order to compare  $(S_1, S_2) = (0, 1)$  and  $(S_1, S_2) = (1, 0)$ , consider the case where

$(S_1, S_2) = (1, 0)$ . Since  $S_2 = 0$ ,  $\beta_2 = \gamma_1 = 0$ . Also,  $\theta = \frac{\bar{\lambda}}{\bar{\lambda} + \mu}$  since  $\bar{S} = S_1 + S_2 = 1$ .

Therefore,  $\beta_1 = \gamma_2 = \frac{\mu}{\bar{\lambda} + \mu}$  by solving equations (3.9) and (3.10). After calculating the fill rates in a similar way for  $(S_1, S_2) = (0, 1)$ , we can incorporate them in  $z(S_1, S_2)$  and  $u(S_1, S_2)$  as follows.

$$u(1, 0) = \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_1)$$

$$u(0, 1) = \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_2)$$

$$z(1, 0) = (f + h) + \frac{\bar{\lambda}^2}{\bar{\lambda} + \mu} c^e + \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_1) c^{in} + \frac{\mu}{\bar{\lambda} + \mu} (d_2 + d_{-1}) c^{out}$$

$$z(0, 1) = (f + h) + \frac{\bar{\lambda}^2}{\bar{\lambda} + \mu} c^e + \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_2) c^{in} + \frac{\mu}{\bar{\lambda} + \mu} (d_1 + d_{-1}) c^{out}$$

We observe that  $u(1, 0) \geq u(0, 1)$  and  $z(1, 0) \leq z(0, 1)$  if  $d_1 \geq d_2$ . However, without loss of generality we can “rename” the larger demand region as  $d_1$ . As a result,  $(S_1, S_2) = (1, 0)$  dominates  $(S_1, S_2) = (0, 1)$  as a solution. Strictly speaking,  $(S_1, S_2) = (1, 0)$  and  $(S_1, S_2) = (1, 1)$  are undominated solutions to problem **P**<sub>3</sub>. ■

**Corollary 3.1.1:** *For stock level  $(S_1, S_2) = (1, 0)$  and  $d_1 \geq d_2$ , any feasible demand allocation solution is optimal.*

**Proof:** From Theorem 3.1, if  $(S_1, S_2) = (1, 0)$ , then

$$u(1, 0) = \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_1), \text{ and}$$

$$z(1, 0) = (f + h) + \frac{\bar{\lambda}^2}{\bar{\lambda} + \mu} c^e + \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_1) c^{in} + \frac{\mu}{\bar{\lambda} + \mu} (d_2 + d_{-1}) c^{out}.$$

The demand allocation variables do not appear in the constraint or in the objective function. Therefore, any feasible set of  $X_{01}, X_{11}, X_{21}, X_{-11}, X_{02}, X_{22}, X_{12}, X_{-12}$  values is optimal. ■

Therefore, if  $(S_1, S_2) = (1, 0)$ , we could potentially assign all the demand to facility 1. For  $(S_1, S_2) = (1, 1)$ , if we can prove a result similar to Corollary 3.1.1, then we can conclude that problem  $\mathbf{P}_3$  is trivial.

**Theorem 3.2:** For stock levels of  $(S_1, S_2) = (1, 1)$  and  $d_1 \geq d_2$ , the optimal demand allocation is  $X_{01} = 0, X_{02} = d_0, X_{11} = d_1, X_{12} = 0, X_{21} = 0, X_{22} = d_2, X_{-11} = 0$ , and  $X_{-12} = d_{-1}$ .

**Proof:** In the case where  $(S_1, S_2) = (1, 1)$ , the fill rates are given in equations (3.8'), (3.9'), (3.10'), (3.11), and (3.12). Inserting these fill rates into  $z(S_1, S_2)$  and  $u(S_1, S_2)$ , we obtain the following equations.

$$z(1,1) = 2(f + h) + \frac{\bar{\lambda}^3}{(\bar{\lambda} + \mu)^2 + \mu^2} c^e$$

$$+ \frac{\mu}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)} \left\{ \begin{aligned} & \left( (\bar{\lambda}^2 + 2(X_{01} + X_{11} + X_{21} + X_{-11})\mu) \right) ((d_0 + d_2)c^{in} + (d_1 + d_{-1})c^{out}) \\ & + \left( (\bar{\lambda}^2 + 2(X_{02} + X_{22} + X_{12} + X_{-12})\mu) \right) ((d_0 + d_1)c^{in} + (d_2 + d_{-1})c^{out}) \\ & + 2\mu(\bar{\lambda} + \mu)(d_0c^{in} + d_{-1}c^{out} + (X_{11} + X_{22})c^{in} + (X_{21} + X_{12})c^{out}) \end{aligned} \right\}$$

$$u(1,1) = \left( 1 - \frac{\bar{\lambda}^2}{(\bar{\lambda} + \mu)^2 + \mu^2} \right) d_0$$

$$+ \frac{\mu}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)} \left\{ \begin{aligned} & \bar{\lambda}^2(d_1 + d_2) + 2\mu(\bar{\lambda} + \mu + d_2)X_{11} \\ & + 2\mu(\bar{\lambda} + \mu + d_1)X_{22} \\ & + 2\mu d_2(X_{01} + X_{21}) + 2\mu d_1(X_{02} + X_{12}) \end{aligned} \right\}$$

Let us now compare the coefficients of  $X_{01}$  and  $X_{02}$  in  $z(1,1)$  and  $u(1,1)$ .

$$z(1,1) \text{ coefficient of } X_{01}: \frac{2\mu^2((d_0 + d_2)c^{in} + (d_1 + d_{-1})c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$z(1,1) \text{ coefficient of } X_{02}: \frac{2\mu^2((d_0 + d_1)c^{in} + (d_2 + d_{-1})c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$u(1,1) \text{ coefficient of } X_{01}: \frac{2\mu^2 d_2}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$u(1,1) \text{ coefficient of } X_{02}: \frac{2\mu^2 d_1}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

We observe that when  $d_1 \geq d_2$  (without loss of generality), the objective function coefficient of  $X_{02}$  is less than that of  $X_{01}$  and the constraint coefficient of  $X_{02}$  is greater than that of  $X_{01}$  (i.e.,  $X_{02}$  dominates  $X_{01}$ ). As mentioned earlier in Theorem 3.1, we can assume  $d_1 \geq d_2$  without loss of generality. In effect,  $X_{01} = 0$  and  $X_{02} = d_0$  if  $(S_1, S_2) = (1, 1)$ .

Similarly we can compare the coefficients of  $X_{11}$ ,  $X_{12}$ ,  $X_{21}$ ,  $X_{22}$ ,  $X_{-11}$ , and  $X_{-12}$  in  $z(1,1)$  and  $u(1,1)$ .

$$X_{11} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_2)c^{in} + (d_1 + d_{-1})c^{out} + (\bar{\lambda} + \mu)c^{in})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{12} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_1)c^{in} + (d_2 + d_{-1})c^{out} + (\bar{\lambda} + \mu)c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{21} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_2)c^{in} + (d_1 + d_{-1})c^{out} + (\bar{\lambda} + \mu)c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{22} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_1)c^{in} + (d_2 + d_{-1})c^{out} + (\bar{\lambda} + \mu)c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{-11} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_2)c^{in} + (d_1 + d_{-1})c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{-12} \text{ in } z(1,1): \frac{2\mu^2((d_0 + d_1)c^{in} + (d_2 + d_{-1})c^{out})}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{11} \text{ in } u(1,1): \frac{2\mu^2(\bar{\lambda} + \mu + d_2)}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{12} \text{ in } u(1,1): \frac{2\mu^2 d_1}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{21} \text{ in } u(1,1): \frac{2\mu^2 d_2}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{22} \text{ in } u(1,1): \frac{2\mu^2(\bar{\lambda} + \mu + d_1)}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)}$$

$$X_{-11} \text{ in } u(1,1): 0$$

$$X_{-12} \text{ in } u(1,1): 0$$

We again observe the dominance of  $X_{11}$  over  $X_{12}$ ,  $X_{22}$  over  $X_{21}$ , and  $X_{-12}$  over  $X_{-11}$  when  $d_1 \geq d_2$ . Therefore, in the case where  $(S_1, S_2) = (1, 1)$ ,  $X_{11} = d_1$ ,  $X_{12} = 0$ ,  $X_{22} = d_2$ ,  $X_{21} = 0$ ,  $X_{-12} = d_{-1}$ , and  $X_{-11} = 0$ . The demand allocation can be obtained by inspection when  $(S_1, S_2) = (1, 1)$ . ■

In other words, if we decide to open and stock a single unit at each facility, then the demand that is only within the time window of facility 1 should be assigned to facility 1. All the rest of the demand should be assigned to facility 2. Intuitively, this makes sense because  $d_1 \geq d_2$ . So, the facility with less demand within its time window is assigned to more customers.

Moreover, for every stock level combination, we can now calculate the objective function and constraint values. We know that

$$z(0,0) = c^e \bar{\lambda}, \quad (3.14)$$

and

$$u(0,0) = 0. \quad (3.15)$$

From Theorem 3.1,

$$z(1,0) = (f + h) + \frac{\bar{\lambda}^2}{\bar{\lambda} + \mu} c^e + \frac{\mu}{\bar{\lambda} + \mu} ((d_0 + d_1) c^{in} + (d_2 + d_{-1}) c^{out}), \quad (3.16)$$

$$u(1,0) = \frac{\mu}{\bar{\lambda} + \mu} (d_0 + d_1), \quad (3.17)$$

and from Theorem 3.2,

$$\begin{aligned} z(1,1) = & 2(f + h) + \frac{\bar{\lambda}^3}{(\bar{\lambda} + \mu)^2 + \mu^2} c^e \\ & + \frac{\mu}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)} \left\{ \begin{aligned} & c^{in} \left( \begin{aligned} & (\bar{\lambda}^2 + 2\mu d_1)(d_0 + d_2) \\ & + (\bar{\lambda}^2 + 2\mu(d_0 + d_2 + d_{-1}))(d_0 + d_1) \\ & + 2\mu(\bar{\lambda} + \mu)(d_0 + d_1 + d_2) \end{aligned} \right) \\ & + c^{out} \left( \begin{aligned} & (\bar{\lambda}^2 + 2\mu d_1)(d_1 + d_{-1}) \\ & + (\bar{\lambda}^2 + 2\mu(d_0 + d_2 + d_{-1}))(d_2 + d_{-1}) \\ & + 2\mu d_{-1}(\bar{\lambda} + \mu) \end{aligned} \right) \end{aligned} \right\}, \quad (3.18) \\ u(1,1) = & \left( 1 - \frac{\bar{\lambda}^2}{(\bar{\lambda} + \mu)^2 + \mu^2} \right) d_0 \\ & + \frac{\mu}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)} \left\{ \begin{aligned} & \bar{\lambda}^2(d_1 + d_2) + 2\mu d_1(\bar{\lambda} + \mu + d_2) \\ & + 2\mu d_2(\bar{\lambda} + \mu + d_1) + 2\mu d_1 d_0 \end{aligned} \right\}. \quad (3.19) \end{aligned}$$

Consequently from Theorems 3.1 and 3.2, the solution to  $\mathbf{P}_3$  can be obtained by simply evaluating undominated solutions  $(S_1, S_2) = (1,0)$  and  $(S_1, S_2) = (1,1)$ . Note that we cannot always assume  $z(1,1) \geq z(1,0)$  because when  $c^e$  is high, choosing  $(S_1, S_2) = (1,0)$  may result in very high emergency transportation cost. A formal procedure to solve the two facility single pool problem  $\mathbf{P}_3$  is outlined in the following algorithm. Figure 15 is a visual representation of this algorithm.

### Algorithm for the single pool problem

**Step 1.** Assign the larger demand region facility as facility '1'.

**Step 2.** If  $z(1,1) < z(1,0)$ , then  $(S_1^*, S_2^*) = (1,1)$  and  $(X_{01}^*, X_{11}^*, X_{21}^*, X_{-11}^*, X_{02}^*, X_{22}^*, X_{12}^*, X_{-12}^*) = (0, d_1, 0, 0, d_0, d_2, 0, d_{-1})$ . Otherwise, go to step 3.

**Step 3.** If  $u(1,0) < \alpha \bar{\lambda}$ , then  $(S_1^*, S_2^*) = (1,1)$  and  $(X_{01}^*, X_{11}^*, X_{21}^*, X_{-11}^*, X_{02}^*, X_{22}^*, X_{12}^*, X_{-12}^*) = (0, d_1, 0, 0, d_0, d_2, 0, d_{-1})$ . Otherwise,  $(S_1^*, S_2^*) = (1,0)$  and set  $(X_{01}^*, X_{11}^*, X_{21}^*, X_{-11}^*, X_{02}^*, X_{22}^*, X_{12}^*, X_{-12}^*)$  arbitrarily such that  $X_{11} + X_{12} = d_1$ ,  $X_{21} + X_{22} = d_2$ ,  $X_{01} + X_{02} = d_0$ , and  $X_{-11} + X_{-12} = d_{-1}$ .

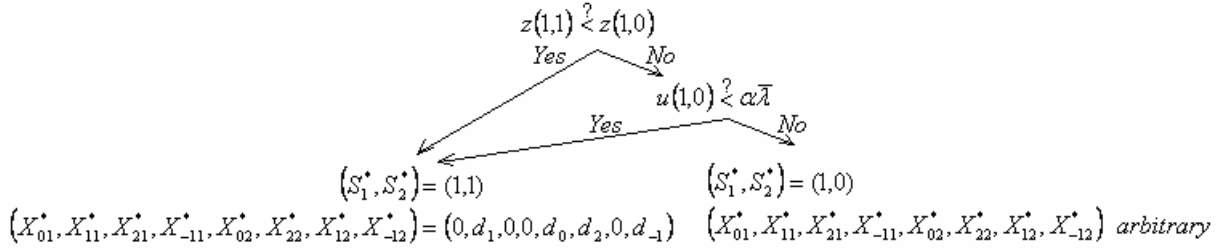


Figure 15. Graphical representation of single pool algorithm

### 2.5 Numerical example

As an example, consider the three scenarios in Table 11 where the system-wide service level is  $\alpha = 40\%$  in each scenario. Each scenario follows a different path in the algorithm. In the first scenario, the transportation cost from the central warehouse ( $c^e$ ) is set high such that  $z(1,1) < z(1,0)$ . In scenarios 2 and 3,  $z(1,1) \geq z(1,0)$ , but we vary demand in the overlapping region ( $d_0$ ). In scenario 2,  $d_0$  is so low that  $S = (1,0)$  does not satisfy the service level constraint, whereas  $d_0$  is high enough in scenario 3 that  $S = (1,0)$  is sufficient to satisfy the target service level. Figure 16 illustrates the algorithm for these three scenarios, and in order to focus on the inventory portion of the problem, we set  $f = 0$  for the rest of this chapter.



Table 11. Examples of two-facility pools

	Scenario 1	Scenario 2	Scenario 3
<b>System Parameters</b>			
$\bar{\lambda}$	1.3	1.3	1.3
$\mu$	1	1	1
$d_0$	0.25	0.25	0.6
$d_1$	0.6	0.6	0.6
$d_2$	0.4	0.4	0.05
$d_{-1}$	0.05	0.05	0.05
<b>Cost Parameters</b>			
$h$	3	3	3
$c^e$	9	1.5	1.5
$c^{in}$	0.5	0.5	0.5
$c^{out}$	0.75	0.75	0.75

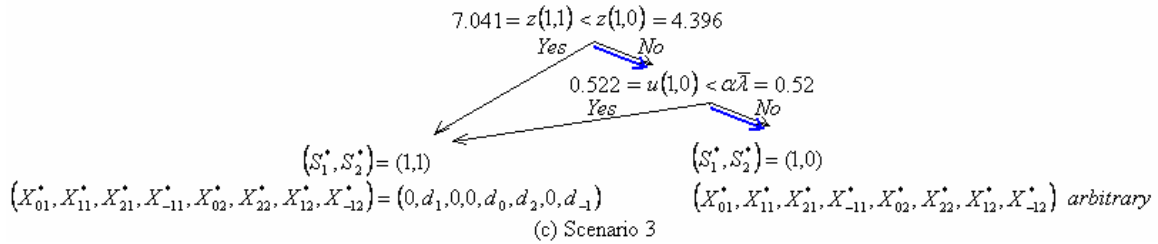
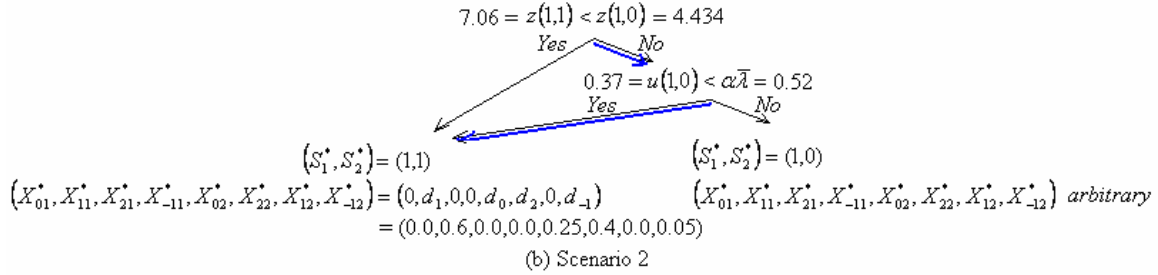
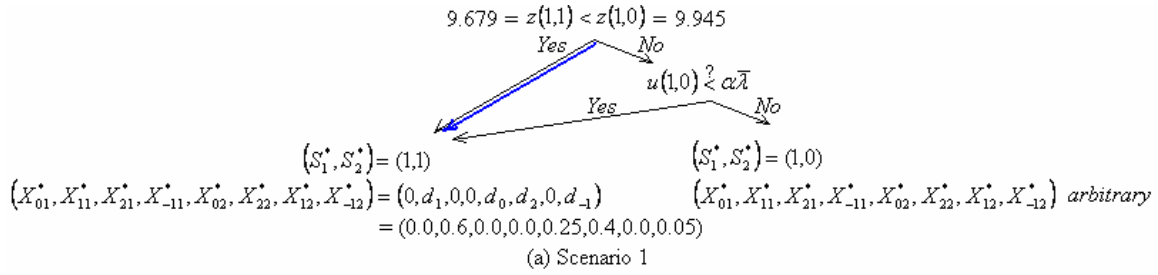


Figure 16. Solution procedure for each scenario in Table 11

An important observation in the single pool problem is that  $S = (1,0)$  becomes sufficient to satisfy the target service level when  $d_0$  is high. If we measure the degree of inventory sharing based on the idea that  $S = (1,0)$  corresponds to more sharing as compared to  $S = (1,1)$ , then the pool reflects a higher degree of sharing when the demand in the overlapping region (of facilities 1 and 2) is high. Even in the case where  $S = (1,1)$ , the service level increases with increase in  $d_0$  (Figure 17). The plot in Figure 17 corresponds to scenario 2 in Table 11.

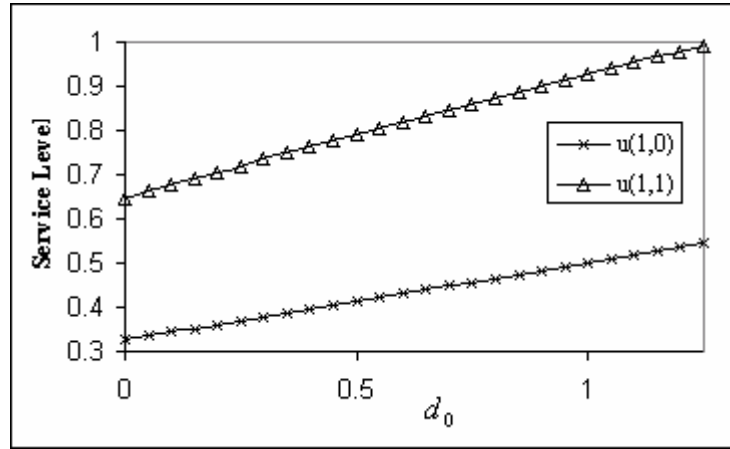


Figure 17. Service level as a function of overlapping demand

### 3 Multiple pool inventory problem with inventory sharing

Consider a network of multiple two facility pools as seen in Figure 18. In addition to the assumptions we make in the single pool problem, let us also assume that each customer belongs to only one pool, i.e., there is no overlap of demand between pools. Also, we assume that a customer cannot be assigned to a facility outside of its pool. Now that we have a system-wide service level constraint over all the pools, we can allow pools to have zero inventory. All the customers in such pools would end up being satisfied by the central warehouse, but this may still prove beneficial from a global point of view.

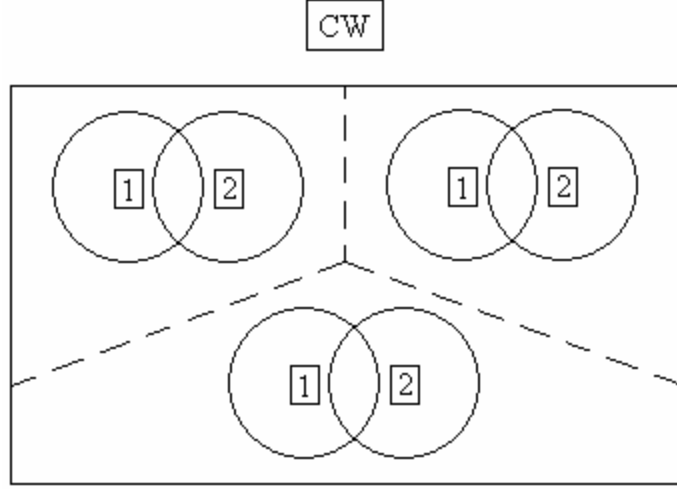


Figure 18. Example of three pools with two facilities in each pool

Suppose the set of pools  $P$  is indexed by  $p$ . We include the index “ $p$ ” to all the parameters and variables (except  $\alpha$ ) to denote the pool they belong to. As a result, the cost of pool  $p$  is given by

$$\begin{aligned}
 z(S_{1p}, S_{2p}) = & (f + h)(S_{1p} + S_{2p}) \\
 & + c^{in} \beta_{1p} (X_{01p} + X_{11p}) + c^{out} \beta_{1p} (X_{21p} + X_{-11p}) \\
 & + c^{in} \beta_{2p} (X_{02p} + X_{22p}) + c^{out} \beta_{2p} (X_{12p} + X_{-12p}) \\
 & + c^{in} \gamma_{1p} (X_{01p} + X_{21p}) + c^{out} \gamma_{1p} (X_{11p} + X_{-11p}) \\
 & + c^{in} \gamma_{2p} (X_{02p} + X_{12p}) + c^{out} \gamma_{2p} (X_{22p} + X_{-12p}) \\
 & + c^e \theta_p \bar{\lambda}_p,
 \end{aligned}$$

and the contribution of pool  $p$  towards service is

$$\begin{aligned}
 u_p(S_{1p}, S_{2p}) = & \beta_{1p} (X_{01p} + X_{11p}) + \gamma_{1p} (X_{01p} + X_{21p}) \\
 & + \beta_{2p} (X_{02p} + X_{22p}) + \gamma_{2p} (X_{02p} + X_{12p}).
 \end{aligned}$$

### 3.1 Formulation of multiple pool problem

The problem of minimizing the total cost of all the pools subject to a service level constraint simply involves combining the single pool problem for each pool subject to a system-wide service level requirement  $\alpha$ .

**P<sub>4</sub>:** Minimize

$$\sum_{p \in P} z_p(s_{1p}, s_{2p}) \quad (3.20a)$$

subject to

$$\sum_{p \in P} u_p(s_{1p}, s_{2p}) \geq \alpha \sum_{p \in P} \bar{\lambda}_p \quad (3.20b)$$

$$d_{1p} = X_{11p} + X_{12p} \quad p \in P \quad (3.20c)$$

$$d_{2p} = X_{21p} + X_{22p} \quad p \in P \quad (3.20d)$$

$$d_{0p} = X_{01p} + X_{02p} \quad p \in P \quad (3.20e)$$

$$d_{-1p} = X_{-11p} + X_{-12p} \quad p \in P \quad (3.20f)$$

$$X_{01p}, X_{11p}, X_{21p}, X_{-11p}, X_{02p}, X_{22p}, X_{12p}, X_{-12p} \geq 0 \quad p \in P \quad (3.20g)$$

$$s_{1p}, s_{2p} \in \{0, 1, 2, \dots\} \quad p \in P. \quad (3.20h)$$

Note that if each pool  $p$  has to satisfy a target service level of  $\alpha_p$ , then the problem can be separated by pool.

Applying the low demand assumption of SPL, a single unit of stock should suffice at each facility. Moreover, Theorems 3.1 and 3.2 show that we do not need to consider  $(s_1, s_2) = (0, 1)$  in any given pool since it will always be dominated by  $(s_1, s_2) = (1, 0)$  as long as  $d_1 \geq d_2$  for the pool. For each pool, we end up with three feasible solutions;  $(s_1, s_2) = (0, 0)$ ,  $(s_1, s_2) = (1, 0)$ , and  $(s_1, s_2) = (1, 1)$ . Therefore, Problem **P<sub>4</sub>** has at most  $3^{|P|}$  feasible solutions since we also show that the allocation decisions are trivial for a given  $(s_1, s_2)$  combination (equations (3.16-3.19)).

As the number of pools  $|P|$  increases, the solutions space increases exponentially. However, suppose we introduce two binary variables;  $V_p$  set to 1 if pool  $p$  is upgraded from  $(S_1, S_2) = (0,0)$  to  $(S_1, S_2) = (1,0)$ , and  $W_p$  set to 1 if pool  $p$  is upgraded from  $(S_1, S_2) = (1,0)$  to  $(S_1, S_2) = (1,1)$ . This leads to an alternative binary knapsack formulation of problem  $\mathbf{P}_4$  where we identify the subset of pools that are “upgraded” to either  $(S_1, S_2) = (1,0)$  or  $(S_1, S_2) = (1,1)$ . The binary knapsack formulation can be formulated as follows:

#### ***Alternative formulation***

$\mathbf{P}_4$ : Minimize

$$\sum_{p \in P} z_p(0,0) + \sum_{p \in P} (z_p(1,0) - z_p(0,0))V_p + \sum_{p \in P} (z_p(1,1) - z_p(1,0))W_p \quad (3.20a')$$

subject to

$$\sum_{p \in P} u_p(0,0) + \sum_{p \in P} (u_p(1,0) - u_p(0,0))V_p + \sum_{p \in P} (u_p(1,1) - u_p(1,0))W_p \geq \alpha \sum_{p \in P} \bar{\lambda}_p \quad (3.20b')$$

$$W_p \leq V_p \quad p \in P \quad (3.21)$$

$$V_p, W_p \in \{0,1\} \quad p \in P, \quad (3.22)$$

where  $z_p(0,0), z_p(1,0), z_p(1,1), u_p(0,0), u_p(1,0)$ , and  $u_p(1,1)$  are all parameters (from equations 3.14-3.19). Note that  $u_p(1,1) - u_p(1,0)$  can be algebraically simplified and rewritten as

$$u_p(1,1) - u_p(1,0) = \frac{\mu((\bar{\lambda}^2 + 2\mu(d_1 + \bar{\lambda}))(d_0 + d_2) + 2\mu(d_1 + \mu)d_2)}{(\bar{\lambda} + \mu)((\bar{\lambda} + \mu)^2 + \mu^2)},$$

which is greater than or equal to zero since each term in the above expression is non-negative. As a result, if  $z_p(1,1) < z_p(1,0)$  for some pool  $p$ , then  $W_p = 1$  in any optimal solution because  $u_p(1,1) \geq u_p(1,0)$ .

In an effort to obtain a high quality upper bound on the optimal solution we propose the use of the following greedy heuristic. We sort each pool based on the ratio of the marginal increase in cost divided by the marginal increase in service, and pick the pools with the smallest ratios to be upgraded.

***Greedy heuristic for the multiple pool problem***

**Step 1.** Initialize  $V_p = 0$ , and  $W_p = 0$  for every pool  $p \in P$ .

**Step 2.** Sort all the pools in non-decreasing order of  $\frac{z_p(1,0) - z_p(0,0)}{u_p(1,0) - u_p(0,0)}$ , and set  $V_p = 1$  in

this order until either  $\sum_{p \in P} (u_p(1,0) - u_p(0,0))V_p + \sum_{p \in P} (u_p(1,1) - u_p(1,0))W_p \geq \alpha \sum_{p \in P} \bar{\lambda}_p$  or

$V_p = 1, \forall p \in P$ .

**Step 3.** Sort all the pools in non-decreasing order of  $\frac{z_p(1,1) - z_p(1,0)}{u_p(1,1) - u_p(1,0)}$ , and set  $W_p = 1$  in

this order until  $\sum_{p \in P} (u_p(1,0) - u_p(0,0))V_p + \sum_{p \in P} (u_p(1,1) - u_p(1,0))W_p \geq \alpha \sum_{p \in P} \bar{\lambda}_p$ .

The reason we first upgrade pools from  $(S_1, S_2) = (0,0)$  to  $(S_1, S_2) = (1,0)$ , and then we consider upgrading them from  $(S_1, S_2) = (1,0)$  to  $(S_1, S_2) = (1,1)$  as opposed to upgrading them directly from  $(S_1, S_2) = (0,0)$  to  $(S_1, S_2) = (1,1)$  is because  $z_p(1,1) \geq z_p(1,0)$  in most cases.

The worst case bound of the heuristic can be obtained by taking a difference of the LP lower bound and the heuristic upper bound. There are two cases here depending on where the heuristic terminates.

*Case 1:* If the heuristic terminates in step 2, then let  $\bar{P}$  denote the subset of  $P$  for which  $V_p = 1$ , and let  $\bar{p}$  be the index of the last pool added to  $\bar{P}$ . In this case, the worst case gap between the LP lower bound and the heuristic upper bound is

$$\frac{z_{\bar{p}}(1,0) - z_{\bar{p}}(0,0)}{u_{\bar{p}}(1,0) - u_{\bar{p}}(0,0)} \left( \sum_{p \in \bar{P}} (u_p(1,0) - u_p(0,0)) - \alpha \sum_{p \in \bar{P}} \bar{\lambda}_p \right), \quad (3.23)$$

which is the ratio of the objective function coefficient and constraint coefficient of pool  $\bar{p}$  multiplied by the amount by which pool  $\bar{p}$  exceeded the right hand side of the constraint.

*Case 2:* If the heuristic passes through step 2 and terminates in step 3, then let  $\bar{P}$  denote the subset of  $P$  for which  $W_p = 1$ , and let  $\bar{p}$  be the index of the last pool added to  $\bar{P}$ .

The worst case gap in this case is

$$\frac{z_{\bar{p}}(1,1) - z_{\bar{p}}(1,0)}{u_{\bar{p}}(1,1) - u_{\bar{p}}(1,0)} \left( \sum_{p \in \bar{P}} (u_p(1,0) - u_p(0,0)) + \sum_{p \in \bar{P}} (u_p(1,1) - u_p(1,0)) - \alpha \sum_{p \in \bar{P}} \bar{\lambda}_p \right). \quad (3.24)$$

In set  $\bar{P}$ , the ratio of the marginal increase in cost divided by the marginal increase in service increases. Therefore, we expect larger gaps as  $|\bar{P}|$  increases.

### 3.2 Numerical examples

Another upper bound on the optimal solution of problem  $\mathbf{P}_4$  can be obtained by solving each pool separately by setting  $\alpha = \alpha_p$  in the single pool algorithm. We observe that a pool could have a solution of  $(S_1^*, S_2^*) = (1,1)$  when solved separately and switch to  $(S_1^*, S_2^*) = (1,0)$  in the combined problem. Conversely, it is possible for a pool to switch from  $(S_1^*, S_2^*) = (1,0)$  in the individual pool problem to  $(S_1^*, S_2^*) = (1,1)$  in the combined problem. This can be seen in the following two pool example (Table 12) with a system-wide target service level of  $\alpha = 40\%$ .

Table 12. Two pool example

	$p = 1$	$p = 2$
<b>System Parameters</b>		
$\bar{\lambda}$	0.75	2.5
$\mu$	1	1
$d_0$	0.75	1
$d_1$	0	1.5
$d_2$	0	0
$d_{-1}$	0	0
<b>Cost Parameters</b>		
$h$	2	2
$c^e$	1.5	1.5
$c^{in}$	0.5	0.5
$c^{out}$	7.5	7.5

The optimal solution of each pool solved individually is  $(S_{11}^*, S_{21}^*) = (1, 0)$  and  $(S_{12}^*, S_{22}^*) = (1, 1)$  costing a total of 11.22 units for 53.3% service. However, when we solve them in the 2-pool combined problem, the optimal solution turns out to be  $(S_{11}^*, S_{21}^*) = (1, 1)$  and  $(S_{12}^*, S_{22}^*) = (1, 0)$  which costs only 9.51 units and provides 40.8% service. The upper bound from solving each pool individually typically gets worse for larger problem instances.

Let us now consider a three pool problem (Table 13) and evaluate the greedy heuristic for a system-wide target service level of  $\alpha = 40\%$ .



Table 13. Three pool example

	$p = 1$	$p = 2$	$p = 3$
<b>System Parameters</b>			
$\bar{\lambda}$	3	1	1.45
$\mu$	1	1	1
$d_0$	2	1	1.45
$d_1$	1	0	0
$d_2$	0	0	0
$d_{-1}$	0	0	0
<b>Cost Parameters</b>			
$h$	1	1	1
$c^e$	1	1	1
$c^{in}$	1	1	1
$c^{out}$	2	2	2

Using the greedy heuristic, the  $\frac{z_p(1,0) - z_p(0,0)}{u_p(1,0) - u_p(0,0)}$  ratio for pools 1, 2, and 3 are calculated to be 1.333, 2.000, and 1.689, respectively. Therefore, in step 2 we first upgrade pool 1 to  $(S_1, S_2) = (1,0)$ , followed by pools 3 and 2. The service level achieved is 33.8% which is below the required service level. Calculating the  $\frac{z_p(1,1) - z_p(1,0)}{u_p(1,1) - u_p(1,0)}$  ratio in step 3, we obtain a value of 2.323 for pool 1, 3.333 for pool 2, and 2.365 for pool 3. The heuristic recommends that we now upgrade pool 1 from  $(S_1, S_2) = (1,0)$  to  $(S_1, S_2) = (1,1)$  which achieves a service level of 42.9% at a cost of 9.61 units. However, the optimal solution to the three pool problem is  $(S_{11}^*, S_{21}^*) = (1,0)$ ,  $(S_{12}^*, S_{22}^*) = (1,0)$ , and  $(S_{13}^*, S_{23}^*) = (1,1)$  where the total cost is 9.45 units and the service level is 41.5%. Therefore, the greedy heuristic solution remains sub-optimal.

Since the greedy heuristic terminated in step 3, the worst case gap is calculated (from equation 3.24) to be 0.376 units, whereas the actual gap turned out to be  $9.61 - 9.45 = 0.16$  units. Incidentally, solving each pool in Table 13 separately gives the same solution as

the greedy heuristic. Note that these examples are solved by complete enumeration, but in Section 5 we solve the binary knapsack problem using optimization software and evaluate the performance of the greedy heuristic in an experimental setting.

## 4 Sharing vs No-Sharing

In general, one would expect that sharing is more beneficial than not sharing inventory. However, sharing could sometimes hurt with respect to cost and/or service due to the assumption that every facility has to share its entire inventory. In order to compare sharing versus no-sharing, let us first formulate the no-sharing equivalent formulation of **P<sub>3</sub>**. Since we do not allow inventory sharing between facilities, this formulation is obtained by simply setting  $\gamma_1 = 0$  and  $\gamma_2 = 0$  in formulation **P<sub>3</sub>**.

**P<sub>3</sub>**: Minimize

$$\begin{aligned} z(S_1, S_2) = & (f + h)(S_1 + S_2) \\ & + c^{in} \beta_1(X_{01} + X_{11}) + c^{out} \beta_1(X_{21} + X_{-11}) + c^{in} \beta_2(X_{02} + X_{22}) + c^{out} \beta_2(X_{12} + X_{-12}) \\ & + c^e \theta \bar{\lambda} \end{aligned} \quad (3.13a')$$

Subject to

$$u(S_1, S_2) = \beta_1(X_{01} + X_{11}) + \beta_2(X_{02} + X_{22}) \geq \alpha \bar{\lambda} \quad (3.13b')$$

$$d_1 = X_{11} + X_{12} \quad (3.13c')$$

$$d_2 = X_{21} + X_{22} \quad (3.13d')$$

$$d_0 = X_{01} + X_{02} \quad (3.13e')$$

$$d_{-1} = X_{-11} + X_{-12} \quad (3.13f')$$

$$X_{01}, X_{11}, X_{21}, X_{-11}, X_{02}, X_{22}, X_{12}, X_{-12} \geq 0 \quad (3.13g')$$

$$S_1, S_2 \in \{0, 1\}. \quad (3.13h')$$

Let  $z(S_1^*, S_2^*)_{\text{sharing}}$  and  $u(S_1^*, S_2^*)_{\text{sharing}}$  be the optimal objective value and service level of  $\mathbf{P}_3'$  respectively, and let  $z(S_1^*, S_2^*)_{\text{no-sharing}}$  and  $u(S_1^*, S_2^*)_{\text{no-sharing}}$  be the corresponding values in the no-sharing formulation  $\mathbf{P}_3$ . In the case where sharing was allowed ( $\mathbf{P}_3$ ), we observed that demand allocation was trivial for any given stock level. This is partially true in the case of no-sharing. If  $(S_1^*, S_2^*) = (0,0)$  or  $(S_1^*, S_2^*) = (1,0)$ , then  $z(S_1^*, S_2^*)_{\text{sharing}}$  and  $u(S_1^*, S_2^*)_{\text{sharing}}$  are independent of the demand allocation variables (just like in the sharing case). Therefore,

$$\begin{aligned} z(0,0)_{\text{sharing}} &= z(0,0)_{\text{no-sharing}} , \\ u(0,0)_{\text{sharing}} &= u(0,0)_{\text{no-sharing}} , \\ z(1,0)_{\text{sharing}} &= z(1,0)_{\text{no-sharing}} , \text{ and} \\ u(1,0)_{\text{sharing}} &= u(1,0)_{\text{no-sharing}} . \end{aligned}$$

In other words, sharing does not benefit or harm when  $(S_1^*, S_2^*) = (0,0)$  or  $(S_1^*, S_2^*) = (1,0)$ .

However, in the event that  $(S_1^*, S_2^*) = (1,1)$ ,  $z(1,1)_{\text{sharing}}$  and  $u(1,1)_{\text{sharing}}$  are not independent of the demand allocation variables. Moreover, unlike the no-sharing case, there does not exist dominance of certain demand allocation variables in  $z(1,1)_{\text{sharing}}$  and  $u(1,1)_{\text{sharing}}$ . Therefore, the demand allocation for  $(S_1, S_2) = (1,1)$  can only be obtained by solving the non-linear optimization problem in  $\mathbf{P}_3'$ . Nevertheless, we can still find conditions in which sharing is more beneficial than no-sharing for  $(S_1, S_2) = (1,1)$  stock levels. We know that sharing is beneficial with respect to service only if  $u(1,1)_{\text{sharing}} \geq u(1,1)_{\text{no-sharing}}$  and with respect to cost only if  $z(1,1)_{\text{sharing}} \leq z(1,1)_{\text{no-sharing}}$ . The formulae for these conditions are given in Appendix G.

Figure 19 and Figure 20 illustrate that sharing is only beneficial under certain conditions. In Figure 19, we plot the service level as a function of demand in the overlapping region

of both facilities ( $d_0$ ). The rest of the parameters for this plot are  $d_1 = 0.6$ ,  $d_2 = 0.1$ ,  $d_{-1} = 0.1$ , and  $\mu = 12$ .

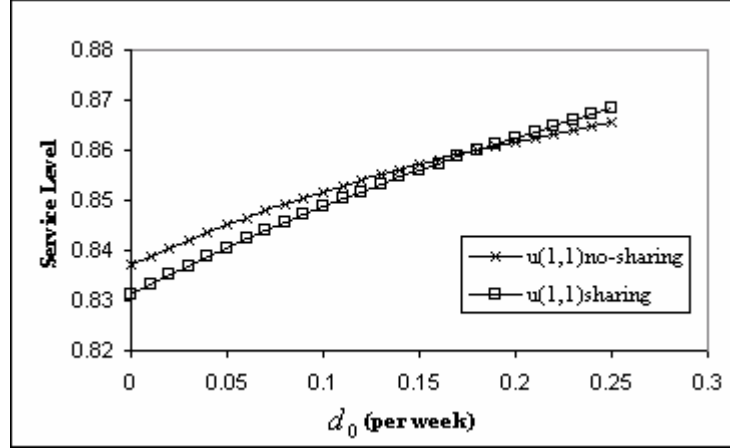


Figure 19. Sharing hurts with respect to service level in some cases

Similarly, in Figure 20 we plot the total cost as a function of the replenishment rate ( $\mu$ ). For this plot, we set  $d_1 = 0.6$ ,  $d_2 = 0.1$ ,  $d_0 = 4.0$ , and  $d_{-1} = 0.1$ .

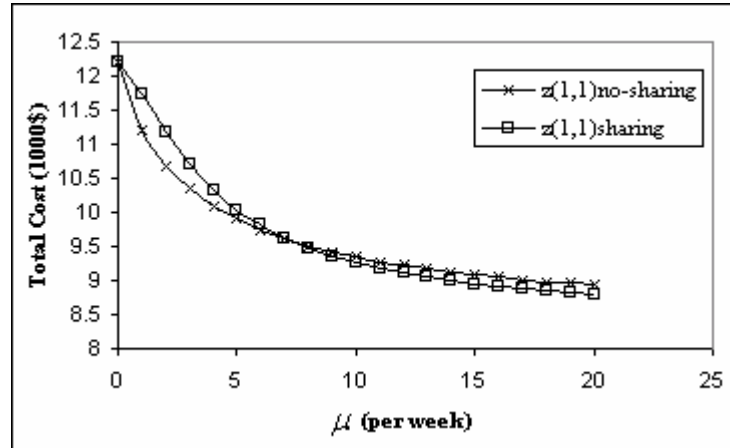


Figure 20. Sharing hurts with respect to total cost in some cases

In summary, inventory sharing is beneficial when a large number of customers exist in the overlapping region of the time windows of both facilities and when each facility has a high replenishment rate of inventory. This is because, when most of the demand exists

outside the overlapping region of both facilities, facilities end up having to share inventory with customers that do not contribute to their service level. Similarly, low replenishment rates cause facilities to remain out of stock for longer periods of time because the facilities are forced to share inventory with all the customers in the pool.

We mentioned earlier that demand allocation is not trivial for all given stock levels. Therefore, the no-sharing problem remains non-linear in the no-sharing case.

## 5 Computational results

In this section, we run some experiments on the formulation and heuristic from Section 4. The  $\mathbf{P}_4$  formulation is modeled in MOSEL and solved using branch and bound with Xpress MP as the solver. The multiple pool problem can be solved in a significantly short amount of time. Using a Pentium M 1.4 GHz processor with 512 MB of RAM, we can solve the optimization problem with up to 5000 pools in less than a minute.

Consider a network of 50 pools, with each pool having two facilities. In order to identify system parameters that induce a greater degree of inventory sharing, we conduct a controlled set of experiments (see Appendix H for details) with the following factors with their corresponding levels.

- $h = \{0, 5, 10\}$
- $c^{in} = \{0, 0.5, 1.0\}$
- $c^{out} = \{0, 1, 2\}$
- $c^e = \{0, 1.5, 3.0\}$
- $\alpha = \{0.75, 0.85\}$
- $d_1 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_2 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_0 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_{-1} = \{[0, 0.01], [0.01, 0.02]\}$

Note that we only run those combinations where  $c^{in} \leq c^{out}$  and we set  $f = 0$  to highlight the effects of inventory sharing. All costs are in 1000s of \$, and demand parameters are in mean rates per week while the replenishment rate at each facility is set to  $\mu = 1$  unit per week. Before running the experiment over different parameter values, we generate a random set of demand values for  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$ . We then maintain this demand set throughout the experiment so that we can compare the results of the experiments.

The input parameters are organized as follows.

- Holding cost of inventory at each facility – denoted by “ $h$ ”
- Transportation cost of demand satisfied within the time window of a facility – denoted by “ $c^{in}$ ”
- Transportation cost of demand satisfied outside the time window of a facility – denoted by “ $c^{out}$ ”
- Transportation cost of demand satisfied as an emergency shipment from the central warehouse – denoted by “ $c^e$ ”
- Target system wide service level – denoted by “ $\alpha$ ”
- Total demand rate from customers only within the time window of facility 1 – denoted by “ $d_1$ ”
- Total demand rate from customers only within the time window of facility 2 – denoted by “ $d_2$ ”
- Total demand rate from customers that are within the time window of both facility 1 and facility 2 – denoted by “ $d_0$ ”
- Total demand rate from customers that are not within the time window of any facility – denoted by “ $d_{-1}$ ”

The output is organized as follows.

- Number of pools with  $(S_{1p}, S_{2p}) = (0,0)$  – denoted by “(0,0)”

- Number of pools with  $(S_{1p}, S_{2p}) = (1,0)$  – denoted by “(1,0)”
- Number of pools with  $(S_{1p}, S_{2p}) = (1,1)$  – denoted by “(1,1)”
- Optimal objective value – denoted by “Opt obj”
- Status of optimal solution at termination – denoted by “Status”
- Time to obtain optimal solution – denoted by “Opt sol time”
- Heuristic objective value – denoted by “H obj”
- Time to obtain heuristic solution – denoted by “H sol time”
- Gap between heuristic solution and optimal solution as a fraction of the optimal solution – denoted by “H-Opt gap”

***Performance of greedy heuristic for the multiple pool problem***

Analysis of the results reveals that the heuristic performs well in instances where the holding cost is positive. See Table 14 for a subset of some experiments with zero holding cost and another subset with positive holding cost (where  $c^{in} = 1$ ,  $c^{out} = 2$ , and  $c^e = 3$ ). Among the 672 instances where holding cost is positive, the heuristic is on average within 0.12% of the optimal solution, and the maximum gap is 1.8%.

Table 14. Snapshot of experiments varying  $h$

Input Parameters						Output							
$h$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Opt sol time	H obj	H sol time	H-Opt gap
0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	10.31	0.04	12.01	0	0.1646
0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	0	50	11.39	0.031	12.58	0.01	0.1052
0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	0	50	12.89	0.03	15.24	0	0.1826
0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	13.98	0.03	15.68	0	0.122
0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.569	0.04	4.862	0	0.0643
0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	0	0	0	0
0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	0	50	6.926	0.03	7.662	0	0.1063
0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	0	50	7.97	0.04	8.062	0	0.0115
5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	402.1	0.06	402.1	0	0
5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	437.6	0.06	437.6	0	1E-05
5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	395.3	0.06	395.3	0	0
5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	425.8	0.06	425.8	0	0
5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	380	0.06	380	0	0
5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	0.01	0	0	0
5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	357.8	0.05	357.8	0	0
5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	473.1	0.05	473.1	0	1E-05

This is because when the holding cost is zero, a large number of pools end up with two units of stock and the greedy heuristic terminates in step 2. As a result, many pools have  $W_p = 1$ , and the set  $\bar{P}$  is quite large which in turn causes a larger worst case gap (Section 3.2).

We observe (in Table 15) that the number of pools with two units of stock increases with increase in  $\alpha$ ,  $d_1$ ,  $d_2$ , and  $d_{-1}$ . This serves as a validity check for the model, because we expect that more inventory would be required to satisfy more demand and/or higher target service levels. Another important observation from Table 15 is that the number of pools with two units of stock decreases with increase in  $d_0$ . Therefore, as the demand in the overlapping region of the time window of both facilities increases, the pool can afford to reduce inventory because of a greater degree of inventory sharing. This reinforces the observation in Figure 17.

Table 15. Snapshot of experiments varying  $\alpha$ ,  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$

Input Parameters						Output							
$h$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Opt sol time	H obj	H sol time	H-Opt gap
5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	295.5	0.061	300.5	0	0.0167
5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	381	0.06	381	0	0
5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	273.7	0.05	273.7	0.01	0
5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	324.3	0.05	324.3	0.01	0
5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	402.1	0.06	402.1	0	0
5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	437.6	0.06	437.6	0	1E-05
5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	395.3	0.06	395.3	0	0
5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	425.8	0.06	425.8	0	0
5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	380	0.06	380	0	0
5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	0.01	0	0	0
5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	357.8	0.05	357.8	0	0
5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	473.1	0.05	473.1	0	1E-05
5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	475.8	0.061	475.8	0	2E-05
5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	0.01	0	0	0
5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	473.6	0.06	473.6	0	0
5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	514	0.04	514	0.01	0



All the cost parameters ( $h$ ,  $c^{in}$ ,  $c^{out}$ , and  $c^e$ ) have varying effects on the number of pools with two units of stock. In general we would expect that as cost increases, fewer pools would have two units of stock. However, varying these parameters sometime causes  $z(1,1) < z(1,0)$ , i.e, it becomes cheaper to stock two units in the pool than just one unit because of relatively high transportation cost to the central warehouse ( $c^e$ ).

## 6 Conclusions

In the literature, fill rates have been estimated through an iterative process. However, when we know that service parts in SPL have low demand we are able to simplify the steps of estimation. Furthermore, by limiting the number of facilities in a pool to two, we are able to estimate fill rates by simultaneously solving two linear equations. These equations are solved with demand allocation as a parameter.

Using the fill rate estimation equations we have been able to formulate the inventory optimization problem for a single pool with inventory sharing between the two facilities in the pool. In this case, demand allocation is a variable as well. Under the low demand assumption, we notice that there exist only two feasible inventory stocking solutions, and the demand allocation is trivial for each of them. Therefore, the single pool problem can be solved by simply comparing the two solutions.

The multiple pool problem is simply a combination of each of the individual pool problems with a system-wide service level constraint that ties all the pools together. Although the solution space increases exponentially with the number of pools, we have formulated an equivalent binary knapsack problem to solve the multiple pool problem. Finally, we have outlined a greedy heuristic to obtain an upper bound on the problem.

Computational results show that the greedy heuristic performs well in cases where the holding cost is not free. On average, the heuristic solution is within 0.12% of the optimal solution. Furthermore, we observe that a greater degree of sharing occurs when a large

number of customers are located in the area overlapping the time window of both facilities and when the replenishment rate is high at each facility. Due to this greater degree of sharing, lower stock levels are sufficient to achieve the same target service levels.

While measuring the benefit of inventory sharing, we observe that when the demand in the overlapping region of both facilities is low and/or the replenishment rate is low, then inventory sharing hurts the system. This is due to the assumption that all facilities are forced to share their inventory with the other facilities in the pool.

## Chapter 4: Dedicated Facilities and Inventory Sharing

In Chapter 2, we studied the impact of allowing some customers to have facilities dedicated to themselves, and in Chapter 3 we researched the idea of inventory sharing between shared facilities. However, most companies in the spare parts industry have a combination of both. In other words, they would have some customers with demand and service requirements high enough to justify opening a dedicated facility, and on the other hand they would have other customers with demand and service requirements low enough to justify inventory sharing between the facilities that they are assigned to. Therefore, in this chapter, we formulate the inventory sharing problem while allowing some customers to have dedicated facilities on-site. In the case of multiple pools, we also identify a greedy heuristic that provides a good upper bound. Finally, we compare the performance of the model in the literature with the models in this dissertation.

### 1 Single pool inventory sharing problem with dedicated facilities

Consider a single pool of two facilities. These facilities will be addressed as “shared facilities” from now on, in order to distinguish them from the customers with “dedicated facilities”. Demand of each customer is assumed to be low enough that a single unit of base stock level at the shared facility is sufficient to satisfy demand during lead time. In this way, each shared facility can be opened or closed and stocked with at most 1 unit each. We also continue to assume that a single unit of base stock level at a dedicated facility is sufficient to render 100% service to the demand of the customer on-site.

#### 1.1 Notation

In addition to the notation from Chapter 3, let  $J$  be the set of customers with potential dedicated facilities (red flagged customers in Figure 21). Furthermore, we define the following notation:

$J_1$  subset of  $J$  that are only within the time window of shared facility 1

$J_2$  subset of  $J$  that are only within the time window of shared facility 2

$J_0$  subset of  $J$  that are within the time window of both shared facilities 1 and 2

$J_{-1}$  subset of  $J$  that are not within the time window of shared facility 1 or 2

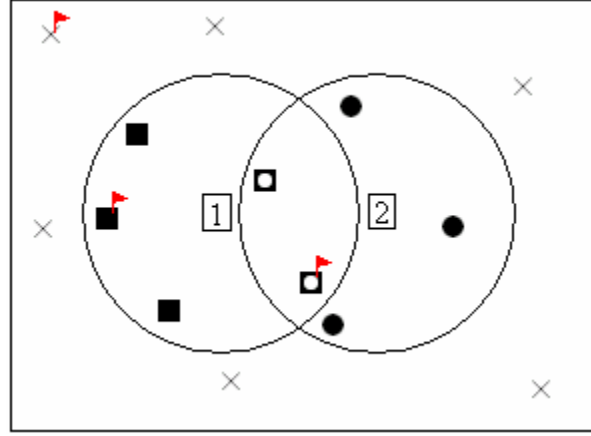


Figure 21. Single pool with dedicated facilities

Suppose  $\hat{d}_j$  is the mean demand rate per unit time of customer  $j$  and  $\hat{f}$  is the fixed cost of opening and operating a dedicated facility per unit time, and we introduce a new decision variable  $\hat{Y}_j$  which is set to 1 if a dedicated facility is opened at the location of customer  $j$ . So the red flagged customers could either be assigned to themselves by opening a dedicated facility on-site, or their demand could be assigned to either shared facility 1 or shared facility 2.

The rest of the customers (that are not potential dedicated facilities), however, can only be assigned to one of the two shared facilities. Therefore, we do not need to know the exact location of these customers. All we need to know is whether they are only within the time window of shared facility 1, or only within the time window of shared facility 2, or within the time window of both shared facilities, or outside the time window of both shared facilities. Based on this, the demand of these customers (that are not potential dedicated facilities) can be aggregated to obtain  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$ .

## 1.2 Formulation of a single pool problem with dedicated facilities

This formulation is simply an extension of the single pool inventory sharing formulation in Chapter 3. Our approach to solve the single pool problem with dedicated facilities is that we first aggregate the demand of all the customers that are not potential dedicated facilities to obtain  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$  and formulate the single pool inventory sharing problem. In addition to the fixed costs, holding costs, and transportation costs of each of the shared facilities, the objective function now includes a fixed and holding cost per unit for each dedicated facility. Moreover, the additional demand of each customer with a potential dedicated facility needs to be satisfied as well. The formulation is given as follows:

**P<sub>5</sub>:** Minimize

$$\begin{aligned}
 z(S_1, S_2) = & (f + h)(S_1 + S_2) + (\hat{f} + h) \sum_{j \in J} \hat{Y}_j \\
 & + c^{in} \beta_1(X_{01} + X_{11}) + c^{out} \beta_1(X_{21} + X_{-11}) + c^{in} \beta_2(X_{02} + X_{22}) + c^{out} \beta_2(X_{12} + X_{-12}) \\
 & + c^{in} \gamma_1(X_{01} + X_{21}) + c^{out} \gamma_1(X_{11} + X_{-11}) + c^{in} \gamma_2(X_{02} + X_{12}) + c^{out} \gamma_2(X_{22} + X_{-12}) \\
 & + c^e \theta \left( \bar{\lambda} + \sum_{j \in J} (1 - \hat{Y}_j) \hat{d}_j \right) \tag{4.1a}
 \end{aligned}$$

subject to

$$\begin{aligned}
 u(S_1, S_2) = & \beta_1(X_{01} + X_{11}) + \gamma_1(X_{01} + X_{21}) \\
 & + \beta_2(X_{02} + X_{22}) + \gamma_2(X_{02} + X_{12}) + \sum_{j \in J} \hat{d}_j \hat{Y}_j \geq \alpha \left( \bar{\lambda} + \sum_{j \in J} \hat{d}_j \right) \tag{4.1b}
 \end{aligned}$$

$$d_1 + \sum_{j \in J_1} \hat{d}_j (1 - \hat{Y}_j) = X_{11} + X_{12} \tag{4.1c}$$

$$d_2 + \sum_{j \in J_2} \hat{d}_j (1 - \hat{Y}_j) = X_{21} + X_{22} \tag{4.1d}$$

$$d_0 + \sum_{j \in J_0} \hat{d}_j (1 - \hat{Y}_j) = X_{01} + X_{02} \tag{4.1e}$$

$$d_{-1} + \sum_{j \in J_{-1}} \hat{d}_j (1 - \hat{Y}_j) = X_{-11} + X_{-12} \quad (4.1f)$$

$$X_{01}, X_{11}, X_{21}, X_{-11}, X_{02}, X_{22}, X_{12}, X_{-12} \geq 0 \quad (4.1g)$$

$$\hat{Y}_j \in \{0,1\} \quad \forall j \in J \quad (4.1h)$$

$$S_1, S_2 \in \{0,1\}, \quad (4.1i)$$

where  $d_1$ ,  $d_2$ ,  $d_0$ ,  $d_{-1}$ , and  $\bar{\lambda}$  are aggregated based on demand of customers that are not potential dedicated facility locations. The fill rates  $\theta, \beta_1, \beta_2, \gamma_1$ , and  $\gamma_2$  are now functions of  $\bar{\lambda} + \sum_{j \in J} \hat{d}_j (1 - \hat{Y}_j)$ .

The service level constraint (4.1b) reflects that each dedicated facility contributes 100% towards the target service level. This is due to the low demand nature of parts in SPL. Constraints (4.1c), (4.1d), (4.1e), and (4.1f) now include the demand of customers with potential dedicated facilities. In other words, either a dedicated facility should be opened at the customer location, or the demand of that particular customer should be assigned to one of the shared facilities.

In Chapter 3, we defined  $d_1$  as the total demand only within the time window of shared facility 1, and  $d_2$  as the total demand only within the time window of shared facility 2. We also prove that for given stock levels, the demand allocation is trivial as long as we maintain  $d_1 \geq d_2$ . However, now that the new value for total demand only within the time window of shared facility 1 is  $d'_1 = d_1 + \sum_{j \in J_1} \hat{d}_j (1 - \hat{Y}_j)$ , and the total demand only within the time window of shared facility 2 is  $d'_2 = d_2 + \sum_{j \in J_2} \hat{d}_j (1 - \hat{Y}_j)$ , we cannot guarantee  $d'_1 \geq d'_2$  since they are now dependent on variables  $\hat{Y}_j$ . Nevertheless, for a given  $\hat{Y}_j$  solution the result still holds because we can calculate the values of  $d'_1$  and  $d'_2$ , and switch the indices ('1' and '2') in case  $d'_1 < d'_2$ . Therefore, we can still enumerate all

the 0-1 combinations of each  $\hat{Y}_j$  variable and preserve the fact that demand allocation is trivial for given stock levels.

Let  $R$  be the set of 0-1 combinations of closing or opening each potential dedicated facility. The problem size  $|R| = 2^{|J|}$  grows exponentially with respect to  $|J|$ . This issue is addressed in Section 2 of this chapter.

The question now arises whether we can eliminate any combinations based on dominance, and the answer is no. This is because opening a dedicated facility always provides a higher service level than assigning the demand of that customer to a shared facility, but from a cost point of view opening or closing a dedicated facility could benefit or harm depending on the size of the customer's demand. In Section 1.4 of this chapter, we provide certain conditions on customer demand under which assigning this additional demand to the existing stock at the shared facilities might prove beneficial from a cost perspective.

For each combination ( $r \in R$ ), we can calculate  $z_r(S_1, S_2)$  as the total cost of stocking  $(S_1, S_2)$  at the shared facilities and opening dedicated facilities corresponding to combination  $r$ , and  $u_r(S_1, S_2)$  as the service level when stocking  $(S_1, S_2)$  at the shared facilities and opening dedicated facilities corresponding to combination  $r$ .

For example, suppose there are three potential dedicated facilities  $J = \{1, 2, 3\}$  where  $J_1 = \{1, 2\}$ ,  $J_2 = \{ \}$ ,  $J_0 = \{ \}$ , and  $J_{-1} = \{3\}$ . If we open dedicated facilities 1 and 3, i.e.,  $r = (1, 0, 1)$ , then  $z_r(S_1, S_2)$  and  $u_r(S_1, S_2)$  are calculated as follows. Since dedicated facility 2 is closed, its demand is added to demand region 1 (since  $J_1 = \{1, 2\}$ ). Therefore, we first calculate the new value for total demand of customers only within the time

window of facility 1 as  $d_1' = d_1 + \hat{d}_2$  and the new total demand to be satisfied by the pool as  $\bar{\lambda}' = \bar{\lambda} + \hat{d}_2$ . Then,

$$\begin{aligned} z_r(0,0) &= z(0,0) + 2(\hat{f} + h), \\ u_r(0,0) &= u(0,0) + (\hat{d}_1 + \hat{d}_3), \\ z_r(1,0) &= z(1,0) + 2(\hat{f} + h), \\ u_r(1,0) &= u(1,0) + (\hat{d}_1 + \hat{d}_3), \\ z_r(1,1) &= z(1,1) + 2(\hat{f} + h), \\ u_r(1,1) &= u(1,1) + (\hat{d}_1 + \hat{d}_3). \end{aligned}$$

where  $z(0,0)$ ,  $u(0,0)$ ,  $z(1,0)$ ,  $u(1,0)$ ,  $z(1,1)$ , and  $u(1,1)$  are calculated by replacing  $d_1$  with  $d_1'$ , and  $\bar{\lambda}$  with  $\bar{\lambda}'$  in equations (3.14-3.19) of Chapter 3.

We now define a new binary variable  $Y_r(S_1, S_2)$  which is set to 1 if  $(S_1, S_2)$  are stocked at the shared facility and dedicated facilities are opened according to combination  $r$ . An alternative formulation to solve the single pool inventory sharing problem with dedicated facilities is given below.

### ***Alternative formulation***

**P<sub>5</sub>**:Minimize

$$\sum_{r \in R} z_r(0,0)Y_r(0,0) + z_r(1,0)Y_r(1,0) + z_r(1,1)Y_r(1,1) \quad (4.1a')$$

subject to

$$\sum_{r \in R} u_r(0,0)Y_r(0,0) + u_r(1,0)Y_r(1,0) + u_r(1,1)Y_r(1,1) \geq \alpha \left( \bar{\lambda} + \sum_{j \in J} \hat{d}_j \right) \quad (4.1b')$$

$$\sum_{r \in R} Y_r(0,0) + Y_r(1,0) + Y_r(1,1) = 1 \quad (4.1j)$$

$$Y_r(0,0), Y_r(1,0), Y_r(1,1) \in \{0,1\} \quad \forall r \in R. \quad (4.1k)$$



Among all the  $Y_r(0,0)$ ,  $Y_r(1,0)$ , and  $Y_r(1,1)$  variables, constraint (4.1j) sets all but one to zero. This ensures that only one stock level combination and one dedicated facility vector combination is chosen. The total cost (4.1a') and the service level (4.1b') are then evaluated accordingly. As we mentioned earlier, the fact that the problem size grows exponentially as  $|J|$  increases will be addressed when formulating and solving the multiple pool case of this problem (Section 2).

By the way, since we calculate the  $z_r(S_1, S_2)$  and  $u_r(S_1, S_2)$  values for each  $r \in R$  ahead of time, we can still continue to ignore the  $(S_1, S_2) = (0,1)$  setting because we know which demand region is larger, and can rename it as the region belonging to shared facility 1.

### 1.3 Special case: Single dedicated facility

In an effort to gain insight into the problem, we analyze the case with  $|J|=1$ . In other words, there exists only one customer with a potential dedicated facility. Demand from the remaining customers are aggregated into demand regions  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$  based on their locations, and let us define  $\mathbf{d} = [d_1 \ d_2 \ d_0 \ d_{-1}]$  as the vector of demand regions. Suppose the demand of the customer with the potential dedicated facility is  $\hat{d}$ , then let  $\mathbf{d}'$  be the demand vector with  $\hat{d}$  added to the appropriate demand region. Based on this notation,  $z(S_1, S_2)_{\mathbf{d}}$  and  $u(S_1, S_2)_{\mathbf{d}}$  denote the objective function and constraint values calculated using demand vector  $\mathbf{d}$ , and  $z(S_1, S_2)_{\mathbf{d}'}$  and  $u(S_1, S_2)_{\mathbf{d}'}$  are calculated using demand vector  $\mathbf{d}'$ . Furthermore, let us also define  $\tilde{z}_{\mathbf{d}}$  and  $\tilde{u}_{\mathbf{d}}$  as the optimal objective value and constraint value (respectively) when the dedicated facility is opened, and let  $\tilde{z}_{\mathbf{d}'}$  and  $\tilde{u}_{\mathbf{d}'}$  be the corresponding values when the dedicated facility is closed.

If  $\hat{Y}$  is the decision variable whether or not to open the dedicated facility, then the optimal solution can be obtained by comparing two alternatives; open the dedicated facility, or close the dedicated facility and assign the demand of the customer on-site to

one of the shared facilities. This can be done because for a given demand vector, we know the optimal stock level and demand allocation (from the single pool algorithm of Section 2.4 in Chapter 3). This procedure can be written as the following algorithm.

***Algorithm for the single pool, single dedicated facility problem***

**Step 1.** Add  $\hat{d}$  to the appropriate demand region to obtain  $\mathbf{d}'$ , and swap indices '1' and '2' if  $d_1 < d_2$  in  $\mathbf{d}'$ .

**Step 2.** Evaluate the option of opening the dedicated facility (step 2.1) and the option of closing it (step 2.2).

**Step 2.1** If  $z(1,1)_{\mathbf{d}} < z(1,0)_{\mathbf{d}}$ , then go to step 2.1.1. Otherwise, if  $u(1,0)_{\mathbf{d}} + \hat{d} < \alpha(\bar{\lambda} + \hat{d})$ , then go to step 2.1.1. Otherwise, go to step 2.1.2.

**Step 2.1.1** Set  $\tilde{z}_{\mathbf{d}} = z(1,1)_{\mathbf{d}} + \hat{f} + h$  and  $\tilde{u}_{\mathbf{d}} = u(1,1)_{\mathbf{d}} + \hat{d}$ .

**Step 2.1.2** Set  $\tilde{z}_{\mathbf{d}} = z(1,0)_{\mathbf{d}} + \hat{f} + h$  and  $\tilde{u}_{\mathbf{d}} = u(1,0)_{\mathbf{d}} + \hat{d}$ .

**Step 2.2** If  $z(1,1)_{\mathbf{d}'} < z(1,0)_{\mathbf{d}'}$ , then go to step 2.2.1. Otherwise, if  $u(1,0)_{\mathbf{d}'} < \alpha(\bar{\lambda} + \hat{d})$ , then go to step 2.2.1. Otherwise, go to step 2.2.2.

**Step 2.2.1** Set  $\tilde{z}_{\mathbf{d}'} = z(1,1)_{\mathbf{d}'}$  and  $\tilde{u}_{\mathbf{d}'} = u(1,1)_{\mathbf{d}'}$ .

**Step 2.2.2** Set  $\tilde{z}_{\mathbf{d}'} = z(1,0)_{\mathbf{d}'}$  and  $\tilde{u}_{\mathbf{d}'} = u(1,0)_{\mathbf{d}'}$ .

**Step 3.** Compare alternatives as follows. If  $\tilde{z}_{\mathbf{d}'} < \tilde{z}_{\mathbf{d}}$  and  $\tilde{u}_{\mathbf{d}'} \geq \alpha(\bar{\lambda} + \hat{d})$  then set  $\hat{Y} = 0$ .

Otherwise, set  $\hat{Y} = 1$ .

Using the algorithm with cost parameters (shown in Table 16), we solve the single pool problem for a system-wide target service level of  $\alpha = 80\%$  while varying the demand of the single dedicated facility. The three scenarios are  $\hat{d} = 0$ ,  $\hat{d} = 0.1$ , and  $\hat{d} = 0.5$  (Table 17).

Table 16. Input cost parameters for special case

Cost Parameters	
$f$	2
$\hat{f}$	1
$h$	0.5
$c^e$	1.5
$c^{in}$	0.5
$c^{out}$	0.75

Table 17. Additional demand scenarios

System Parameters	Scenario 1	Scenario 2	Scenario 3
$\bar{\lambda}$	1	1	1
$\mu$	12	12	12
$d_0$	0.25	0.25	0.25
$d_1$	0.6	0.6	0.6
$d_2$	0.1	0.1	0.1
$d_{-1}$	0.05	0.05	0.05
$\hat{d}$	0	0.1	0.5

Solution	Stock (1,1)	Stock (1,0) Open dedicated facility	Stock (1,0) Close dedicated facility
Total Cost (1000\$)	5.52	4.611	3.45
Service Level	0.914	0.804	0.8

In general, we expect the service level to decrease and total cost to increase as  $\hat{d}$  increases because of a higher service level requirement, and potentially higher stock levels to fulfill the additional demand. However, if we compare scenarios 1, 2 and 3 in Table 17, we can see that the additional demand decreases the total cost. In order to ensure that this behavior is not simply an outcome of the heuristic, we now explore the conditions under which such non-intuitive results occur.

In the case where (1,0) units are stocked at the shared facilities, the total cost decreases with increase in additional demand  $\hat{d}$  if  $z(1,0)_a \leq z(1,0)_d$ . This can be rewritten as

$$0 \leq \hat{d} \leq \frac{1}{c^e(\bar{\lambda} + \mu)} (\mu(c^{out} - c^{in})(d_2 - d_{-1}) - \bar{\lambda}c^e(\bar{\lambda} + 2\mu) - \mu^2c^{in}).$$

This range exists only when the right hand side of the inequality

$$\frac{1}{c^e(\bar{\lambda} + \mu)} (\mu(c^{out} - c^{in})(d_2 - d_{-1}) - \bar{\lambda}c^e(\bar{\lambda} + 2\mu) - \mu^2c^{in}) \geq 0.$$

Solving the above inequality with respect to  $c^{out}$  by replacing all the other parameters with those in Table 16 and Table 17, we observe that this range exists for  $c^{out} > 62.4$ . Figure 22 shows this decrease in cost with respect to additional demand ( $c^{out} = 80$  in Figure 22).

Similarly, in the case where (1,0) units are stocked at the shared facilities, service increases with increase in additional demand  $\hat{d}$  if  $u(1,0)_a \geq u(1,0)_d$ , which in terms of  $\hat{d}$  is given by

$$0 \leq \hat{d} \leq \frac{(\bar{\lambda} + \mu)(d_2 + d_{-1})}{(d_0 + d_1)} - \bar{\lambda}.$$

In order for this range to exist, we require the right hand side of the inequality

$$\frac{(\bar{\lambda} + \mu)(d_2 + d_{-1})}{(d_0 + d_1)} - \bar{\lambda} \geq 0.$$

For the system parameters in Table 17, this range exists when  $\mu > 5.2$ . Figure 23 shows increase in service within this range (where  $\mu = 12$ ).

Although these are theoretical possibilities, it is highly unlikely that  $c^{out} = 62.5$  would be so much larger than  $c^{in} = 0.5$ . Moreover, a replenishment rate of  $\mu = 5.2$  per week is also not very likely. Therefore, such cases may not occur in practice, but we cannot ignore these possibilities while building algorithms and heuristics to solve this problem.

Such non-intuitive results were not observed in the case where (1,1) units are stocked at the shared facilities.

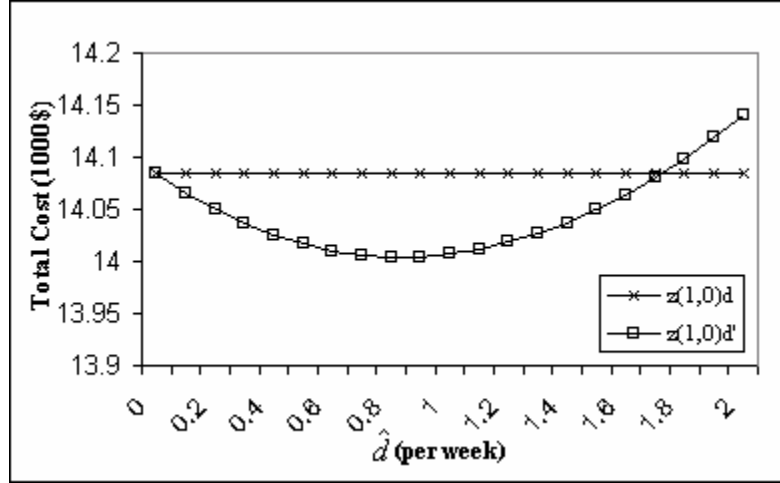


Figure 22. Reduction in cost with additional demand

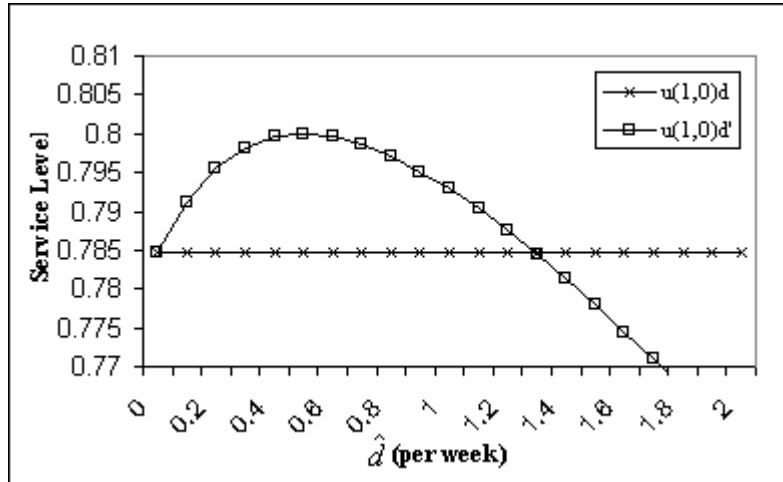


Figure 23. Increase in service with additional demand

#### 1.4 Numerical example

Consider a single pool of two shared facilities. Suppose there exist a number of customers, 10 of which are potential dedicated facilities, and the rest are pooled together to form the demand vector  $\mathbf{d} = [d_1 \ d_2 \ d_0 \ d_{-1}]$  based on their locations. The system

demand parameters and cost parameters are given in Table 18, and the demand for those customers with potential dedicated facilities can be seen in Table 19.

Suppose the customers with potential dedicated facilities are situated such that  $J_1 = \{1,3,4,6,8,9,10\}$  are only within the time window of shared facility 1,  $J_2 = \{2,7\}$  are only within the time window of shared facility 2,  $J_0 = \{5\}$  is within the time window of both shared facilities, and  $J_{-1} = \{ \}$  are outside the time window of both shared facilities. For a system-wide target service level of  $\alpha = 93\%$ , the formulation in  $\mathbf{P}_5'$  is solved using MOSEL as the modeling language and XpressMP as the solver. The optimal solution is to open and stock 1 unit in each shared facility, and open dedicated facilities at customer locations 6, 3, 9, and 4. This corresponds to a total cost of 11.61 units and a service level of 93.4%, and the problem is solved instantly (less than 1 second).

Among the customers with potential dedicated facilities, notice that the optimal solution chose to open dedicated facilities at those customer locations with high demand. In Section 2 of this chapter, we capitalize on this observation by incorporating it within a heuristic. However, when  $\alpha = 92\%$ , dedicated facilities 6, 3, and 1 are opened (i.e. locations 9 and 4 were skipped even though they had higher demand than location 1). Therefore, picking high demand customers as dedicated facilities remains sub-optimal.

Table 18. Input parameters for general case

System Parameters	
$\bar{\lambda}$	1
$\mu$	12
$d_0$	0.25
$d_1$	0.6
$d_2$	0.1
$d_{-1}$	0.05
Cost Parameters	
$f$	2
$\hat{f}$	1
$h$	0.5
$c^e$	1.5
$c^{in}$	0.5
$c^{out}$	0.75

Table 19. List of customers with potential dedicated facilities

Potential Dedicated Facilities	
$j$	$\hat{d}_j$
1	0.0656401
2	0.011916
3	0.0745505
4	0.0727971
5	0.0411361
6	0.0800164
7	0.0321793
8	0.0162623
9	0.073702
10	0.004096

## 2 Multiple pool inventory sharing problem with dedicated facilities

Let  $J^p$  be the set of customers with potential dedicated facilities in pool  $p$ . An index  $p$  is attached to all the variables and parameters indicating the pool they belong to. Recall the assumption that there is no region of overlap between pools, and customers cannot be

assigned to facilities outside of their own pool. The multiple pool formulation is simply an extension of the single pool formulation ( $\mathbf{P}_5''$ ) as shown below.

$\mathbf{P}_5''$ :Minimize

$$\sum_{p \in P} \sum_{r \in R} z_{rp} (0,0)Y_{rp} (0,0) + z_{rp} (1,0)Y_{rp} (1,0) + z_{rp} (1,1)Y_{rp} (1,1) \quad (4.1a'')$$

subject to

$$\sum_{p \in P} u_{rp} (0,0)Y_{rp} (0,0) + u_{rp} (1,0)Y_{rp} (1,0) + u_{rp} (1,1)Y_{rp} (1,1) \geq \alpha \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \right) \quad (4.1b'')$$

$$\sum_{r \in R} Y_{rp} (0,0) + Y_{rp} (1,0) + Y_{rp} (1,1) = 1 \quad \forall p \in P \quad (4.1j')$$

$$Y_{rp} (0,0), Y_{rp} (1,0), Y_{rp} (1,1) \in \{0,1\} \quad \forall r \in R, p \in P. \quad (4.1k')$$

The main difference between  $\mathbf{P}_5''$  and  $\mathbf{P}_5'$  is that now constraint (4.1b'') is the system-wide service level constraint which ties all the pools together. If each pool had its own target service level ( $\alpha_p$  for example), then  $\mathbf{P}_5''$  separates by pool and can be solved by solving  $\mathbf{P}_5'$  for each pool.

Consider a network with parameter values as seen in Table 20. As we mentioned earlier, the above formulation ( $\mathbf{P}_5''$ ) has a large number of variables because  $|R| = 2^{|J^p|}$  for every pool  $p$ . Suppose all the pools have the same number of potential dedicated facilities  $|J^p| = |J| \quad \forall p \in P$ . For a system-wide target service level of  $\alpha = 75\%$ , it is evident from Table 21 that the solution time increases exponentially with increase in  $|J|$ . To run the experiments in Table 21, we used a Pentium M 1.4GHz processor with 512 MB RAM.



Table 20. Parameters for solution time experiment

System Parameters	
$\mu$	4
$d_0$	[0.05,0.1]
$d_1$	[0.05,0.1]
$d_2$	[0.05,0.1]
$d_{-1}$	[0.01,0.02]
$\hat{d}_j$	[0.005,0.01]
Cost Parameters	
$f$	10
$\hat{f}$	1
$h$	0.5
$c^e$	1
$c^{in}$	0.05
$c^{out}$	0.075

Table 21. Solution time of multiple pool problem

$ P $	$ J $	Opt sol time/s
10	5	0.45
25	5	2.233
50	5	32.437
2	5	0.07
2	10	1.382
2	11	4.136
2	12	14.221
2	13	51.645

Due to this large number of combinations for open/close dedicated facility decisions, we derive a heuristic to obtain near-optimal solutions to the multiple pool problem. The heuristic is based on the special case algorithm in Section 1.3 and the observation in Section 1.4 that customers with high demand are likely to have dedicated facilities in the optimal solution.

The idea behind the heuristic is to first solve the multiple pool inventory sharing problem while ignoring all the potential dedicated facilities and their demand. This can be done using the greedy heuristic in Section 4 of Chapter 3. Next, we pick the potential dedicated facility with the highest demand and use the algorithm in Section 1.3 of this chapter to decide whether to open a dedicated facility at its location or not. Once all potential dedicated facilities in all the pools have been considered, if the solution is infeasible, then we simply upgrade pools and open dedicated facilities based on a cost/service ratio until the solution is feasible. Thus, we have an upper bound on the solution to problem  $\mathbf{P}_5''$ . In terms of lower bounds, computational results (in Section 3) show that the LP relaxation bound performs well for problem  $\mathbf{P}_5''$ .

We now define some new notation to help us with the heuristic. Let  $z_p^*$  be the best objective value contribution of pool  $p$  at any given point in the heuristic and let  $u_p^*$  be the corresponding contribution of pool  $p$  to the service level constraint. Suppose  $k, l, m_p$ , and  $n_j$  are arbitrary parameters for bookkeeping purposes. Then, computational results (in Section 3) show that the following heuristic provides a good upper bound for problem  $\mathbf{P}_5''$ .

***Heuristic for the multiple pool, multiple dedicated facility problem***

**Step 1.** Solve the multiple pool inventory sharing problem ignoring the demand of customers with potential dedicated facilities as follows.

**Step 1.1.** Initialize  $V_p = 0$ , and  $W_p = 0$  for every pool  $p \in P$ .

**Step 1.2.** Sort all the pools in non-decreasing order of  $\frac{z_p(1,0)_d - z_p(0,0)_d}{u_p(1,0)_d - u_p(0,0)_d}$ , and set

$$V_p = 1 \text{ in this order until either } \sum_{p \in P} (u_p(1,0)_d - u_p(0,0)_d) \mathcal{N}_p + \sum_{p \in P} (u_p(1,1)_d - u_p(1,0)_d) W_p \geq$$

$$\alpha \sum_{p \in P} \bar{\lambda}_p \text{ or } V_p = 1, \forall p \in P.$$

**Step 1.3.** Sort all the pools in non-decreasing order of  $\frac{z_p(1,1)_d - z_p(1,0)_d}{u_p(1,1)_d - u_p(1,0)_d}$ , and set

$$W_p = 1 \text{ in this order until either } \sum_{p \in P} (u_p(1,0)_d - u_p(0,0)_d) V_p + \sum_{p \in P} (u_p(1,1)_d - u_p(1,0)_d) W_p \geq \alpha \sum_{p \in P} \bar{\lambda}_p \text{ or } W_p = 1, \forall p \in P.$$

**Step 1.4.** For every pool  $p \in P$ , if  $V_p = 1$ , then set  $z_p^* = z_p(1,0)_d$  and  $u_p^* = u_p(1,0)_d$ .

Otherwise, set  $z_p^* = z_p(0,0)_d$  and  $u_p^* = u_p(0,0)_d$ . For every pool  $p \in P$ , if  $W_p = 1$ , then set  $z_p^* = z_p(1,1)_d$  and  $u_p^* = u_p(1,1)_d$ .

**Step 2.** Consider each potential dedicated facility one at a time based on highest demand as shown below.

**Step 2.1.** Initialize  $\hat{Y}_j = 0 \forall j \in J^p, p \in P$ .

**Step 2.2.** Sort all the potential dedicated facilities in non-increasing order of  $\hat{d}_j$ .

Among all pools  $p \in P$ , pick the potential dedicated facility  $\bar{j}$  with the largest  $\hat{d}_{\bar{j}}$  and identify the pool  $\bar{p}$  it belongs to. Add  $\hat{d}_{\bar{j}}$  to the appropriate demand region to obtain  $\mathbf{d}'$ , and swap indices '1' and '2' if  $d_1 < d_2$  in  $\mathbf{d}'$ .

**Step 2.3.** Evaluate the option of opening the dedicated facility (step 2.3.1) and the option of closing it (step 2.3.2).

**Step 2.3.1.** If  $z_{\bar{p}}(1,1)_d < z_{\bar{p}}(1,0)_d$ , then go to step 2.3.1.1. Otherwise, if

$$u(1,0)_{\bar{p}d} + \hat{d}_{\bar{j}} + \sum_{p \in P \setminus \bar{p}} u_p^* < \alpha \left( \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \hat{Y}_j \right) + \hat{d}_{\bar{j}} \right), \text{ then go to step 2.3.1.1.}$$

Otherwise, go to step 2.3.1.2.

**Step 2.3.1.1.** Set  $k = 2$ ,  $\tilde{z}_{\bar{p}d} = z_{\bar{p}}(1,1)_d + \hat{f} + h + \sum_{j \in J^{\bar{p}}} (\hat{f} + h) \hat{Y}_j$ , and

$$\tilde{u}_{\bar{p}d} = u(1,1)_{\bar{p}d} + \hat{d}_{\bar{j}} + \sum_{j \in J^{\bar{p}}} \hat{d}_j \hat{Y}_j.$$

**Step 2.3.1.2.** Set  $k = 1$ ,  $\tilde{z}_{\bar{p}\mathbf{d}} = z_{\bar{p}}(1,0)_{\mathbf{d}} + \hat{f} + h + \sum_{j \in J^{\bar{p}}} (\hat{f} + h) \hat{Y}_j$ , and

$$\tilde{u}_{\bar{p}\mathbf{d}} = u(1,0)_{\bar{p}\mathbf{d}} + \hat{d}_{\bar{j}} + \sum_{j \in J^{\bar{p}}} \hat{d}_j \hat{Y}_j.$$

**Step 2.3.2.** If  $z_{\bar{p}}(1,1)_{\mathbf{d}'} < z_{\bar{p}}(1,0)_{\mathbf{d}'}$ , then go to step 2.3.2.1. Otherwise, if

$$u(1,0)_{\bar{p}\mathbf{d}'} + \sum_{p \in P \setminus \bar{p}} u_p^* < \alpha \left( \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \hat{Y}_j \right) + \hat{d}_{\bar{j}} \right), \text{ then go to step 2.3.2.1. Otherwise,}$$

go to step 2.3.2.2.

**Step 2.3.2.1.** Set  $l = 2$ ,  $\tilde{z}_{\bar{p}\mathbf{d}'} = z_{\bar{p}}(1,1)_{\mathbf{d}'} + \sum_{j \in J^{\bar{p}}} (\hat{f} + h) \hat{Y}_j$ , and

$$\tilde{u}_{\bar{p}\mathbf{d}'} = u(1,1)_{\bar{p}\mathbf{d}'} + \sum_{j \in J^{\bar{p}}} \hat{d}_j \hat{Y}_j.$$

**Step 2.3.2.2.** Set  $l = 1$ ,  $\tilde{z}_{\bar{p}\mathbf{d}'} = z_{\bar{p}}(1,0)_{\mathbf{d}'} + \sum_{j \in J^{\bar{p}}} (\hat{f} + h) \hat{Y}_j$ , and

$$\tilde{u}_{\bar{p}\mathbf{d}'} = u(1,0)_{\bar{p}\mathbf{d}'} + \sum_{j \in J^{\bar{p}}} \hat{d}_j \hat{Y}_j.$$

**Step 2.4.** Compare alternatives as follows. If  $\tilde{z}_{\bar{p}\mathbf{d}'} < \tilde{z}_{\bar{p}\mathbf{d}}$  and  $\tilde{u}_{\bar{p}\mathbf{d}'} + \sum_{p \in P \setminus \bar{p}} u_p^* \geq$

$\alpha \left( \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \hat{Y}_j \right) + \hat{d}_{\bar{j}} \right)$  then go to step 2.4.1. Otherwise, go to step 2.4.2.

**Step 2.4.1.** Set  $\hat{Y}_{\bar{j}} = 0$ , and replace;  $z_{\bar{p}}^* \leftarrow \tilde{z}_{\bar{p}\mathbf{d}'}$ ,  $u_{\bar{p}}^* \leftarrow \tilde{u}_{\bar{p}\mathbf{d}'}$ ,  $\bar{\lambda}_p \leftarrow \bar{\lambda}_p + \hat{d}_{\bar{j}}$ , and

$\mathbf{d} \leftarrow \mathbf{d}'$ . If  $l = 2$ , then set  $W_{\bar{p}} = 1$  and  $V_{\bar{p}} = 1$ . Otherwise, set  $V_{\bar{p}} = 1$ .

**Step 2.4.2.** Set  $\hat{Y}_{\bar{j}} = 1$ , and replace;  $z_{\bar{p}}^* \leftarrow \tilde{z}_{\bar{p}\mathbf{d}}$ , and  $u_{\bar{p}}^* \leftarrow \tilde{u}_{\bar{p}\mathbf{d}}$ . If  $k = 2$ , then set

$W_{\bar{p}} = 1$  and  $V_{\bar{p}} = 1$ . Otherwise, set  $V_{\bar{p}} = 1$ .

**Step 3.** If all the customers in pool  $\bar{p}$  have been considered, then remove  $\bar{p}$  from  $P$ . If

$|P| > 0$ , then go to step 2.2. Otherwise, if  $\sum_{p \in P} u_p^* \geq \alpha \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \hat{Y}_j \right)$ , then report

$\hat{Y}_j \forall j \in J^p$ ,  $V_p$ , and  $W_p \forall p \in P$ . Otherwise, go to step 4.

**Step 4.** Restore feasibility by upgrading pools and/or opening dedicated facilities as follows.

**Step 4.1.** For every pool  $p \in P$ , if  $V_p = 0$ , then set  $m_p = \frac{z_p(1,0)_d - z_p(0,0)_d}{u_p(1,0)_d - u_p(0,0)_d}$ .

Otherwise, if  $V_p = 1$  and  $W_p = 0$ , then set  $m_p = \frac{z_p(1,1)_d - z_p(1,0)_d}{u_p(1,1)_d - u_p(1,0)_d}$ . Otherwise, set

$$m_p = \infty.$$

**Step 4.2.** For every dedicated facility  $j \in J^p$  in every pool  $p \in P$  such that  $\hat{Y}_j = 0$ , if

$V_p = 0$  then set  $n_j = \frac{z_p(0,0)_d + \hat{f} + h - z_p(0,0)_d}{u_p(0,0)_d + \hat{d}_j - u_p(0,0)_d}$ . Otherwise, if  $V_p = 1$  and  $W_p = 0$ ,

then set  $n_j = \frac{z_p(1,0)_d + \hat{f} + h - z_p(1,0)_d}{u_p(1,0)_d + \hat{d}_j - u_p(1,0)_d}$ . Otherwise, set

$$n_j = \frac{z_p(1,1)_d + \hat{f} + h - z_p(1,1)_d}{u_p(1,1)_d + \hat{d}_j - u_p(1,1)_d}.$$

**Step 4.3.** Sort all  $m_p$  and  $n_j$  in non-decreasing order and upgrade pool  $p$  or open

dedicated facility  $j$  in this order until  $\sum_{p \in P} (u_p(1,0)_d - u_p(0,0)_d) V_p + (u_p(1,1)_d - u_p(1,0)_d) W_p$

$$+ \sum_{p \in P} \sum_{j \in J^p} \hat{d}_j \hat{Y}_j \geq \alpha \sum_{p \in P} \left( \bar{\lambda}_p + \sum_{j \in J^p} \hat{d}_j \right). \text{ Report } \hat{Y}_j \ \forall j \in J^p, \ V_p, \text{ and } W_p \ \forall p \in P.$$

In the next section, we see that this heuristic provides good upper bounds to problem  $\mathbf{P}_5''$ . However, this remains a heuristic because we do not revise stock level decisions at each step based on dedicated facility locations. We hope to address this issue in the future.

### 3 Computational results

In order to test the effects of the parameters on stock levels and dedicated facilities, we conduct experiments with varying parameter values for a network of  $|P|=10$  pools and

each pool  $p \in P$  having  $|J^p| = 5$  dedicated facilities each. The formulation in  $\mathbf{P}_5$  is modeled in MOSEL using XpressMP as the solver. This is run on the same Pentium M 1.4 GHz processor with 512 MB RAM. We use the following combinations of parameter values.

- $f = \{10, 20\}$
- $\hat{f} = \{1, 2\}$
- $h = \{0.5, 1.0\}$
- $c^{in} = \{0.05, 0.1\}$
- $c^{out} = \{0.075, 0.15\}$
- $c^e = \{1, 2\}$
- $\alpha = \{0.70, 0.75\}$
- $d_1 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_2 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_0 = \{[0, 0.05], [0.05, 0.1]\}$
- $d_{-1} = \{[0, 0.01], [0.01, 0.02]\}$
- $\hat{d} = \{[0, 0.001], [0.001, 0.002]\}$

As we mentioned earlier, the demand regions  $d_1$ ,  $d_2$ ,  $d_0$ , and  $d_{-1}$  are random values in the given ranges, but we maintain the same set through all the experiments. The units of demand are in rates per week, and we set the replenishment rate as  $\mu = 4$  per week. All cost parameters are in 1000s of \$.

The results can be seen in Appendix I, and note that we only run those combinations where  $c^{in} \leq c^{out}$ . The input parameters are organized as follows.

- Fixed cost of opening shared facilities – denoted by “ $f$ ”
- Fixed cost of opening dedicated facilities – denoted by “ $\hat{f}$ ”
- Holding cost per unit of inventory at each facility – denoted by “ $h$ ”

- Transportation cost of demand satisfied within the time window of a shared facility – denoted by “ $c^{in}$ ”
- Transportation cost of demand satisfied outside the time window of a shared facility – denoted by “ $c^{out}$ ”
- Transportation cost of demand satisfied as an emergency shipment from the central warehouse – denoted by “ $c^e$ ”
- Target system wide service level – denoted by “ $\alpha$ ”
- Total demand rate from customers only within the time window of shared facility 1 – denoted by “ $d_1$ ”
- Total demand rate from customers only within the time window of shared facility 2 – denoted by “ $d_2$ ”
- Total demand rate from customers that are within the time window of both shared facility 1 and shared facility 2 – denoted by “ $d_0$ ”
- Total demand rate from customers that are not within the time window of any shared facility – denoted by “ $d_{-1}$ ”
- Demand rate of customers with potential dedicated facilities – denoted by “ $\hat{d}$ ”

The output is organized as follows.

- Optimization
  - Number of pools with  $(S_{1p}, S_{2p}) = (0,0)$  – denoted by “Opt (0,0)”
  - Number of pools with  $(S_{1p}, S_{2p}) = (1,0)$  – denoted by “Opt (1,0)”
  - Number of pools with  $(S_{1p}, S_{2p}) = (1,1)$  – denoted by “Opt (1,1)”
  - Number of dedicated facilities opened – denoted by “Opt # ded”
  - Objective value – denoted by “Opt cost”
  - Service level – denoted by “Opt service”
  - Status of optimal solution at termination – denoted by “Opt status”
  - Time to obtain optimal solution – denoted by “Opt solTime”

- Heuristic
  - Number of pools with  $(S_{1p}, S_{2p}) = (0,0)$  – denoted by “H (0,0)”
  - Number of pools with  $(S_{1p}, S_{2p}) = (1,0)$  – denoted by “H (1,0)”
  - Number of pools with  $(S_{1p}, S_{2p}) = (1,1)$  – denoted by “H (1,1)”
  - Number of dedicated facilities opened – denoted by “H # ded”
  - Objective value – denoted by “H cost”
  - Service level – denoted by “H service”
  - Time to obtain the heuristic’s final solution – denoted by “H solTime”
- Gap between heuristic solution and optimal solution as a fraction of the optimal solution – denoted by “H-Opt gap”

The results show that the number of pools with two units of stock decreases with increase in  $d_0$  (Table 22). This can be seen by comparing experiments 9-12 with experiments 13-16. Fewer units of inventory are sufficient because the degree of sharing is high. We observed similar results in Chapter 3 as well. In Table 22, the cost parameters are;  $f = 10$ ,  $\hat{f} = 1$ ,  $h = 0.5$ ,  $c^{in} = 0.05$ ,  $c^{out} = 0.075$ ,  $c^e = 1$ , and  $\alpha = 0.7$ .

Table 22. Degree of sharing with respect to overlapping demand

Exp #	Input Parameters				Output						
	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt solTime
9	[0.05,0.1]	[0.0.05]	[0.0.01]	[0.0.001]	0	7	3	0	136.6	0.7084	0.091
10	[0.05,0.1]	[0.0.05]	[0.0.01]	[0.001,0.002]	0	7	3	0	136.7	0.7088	0.1
11	[0.05,0.1]	[0.0.05]	[0.01,0.02]	[0.0.001]	0	6	4	0	147.2	0.7106	0.09
12	[0.05,0.1]	[0.0.05]	[0.01,0.02]	[0.001,0.002]	0	6	4	0	147.2	0.7105	0.11
13	[0.05,0.1]	[0.05,0.1]	[0.0.01]	[0.0.001]	0	8	2	0	126.2	0.7188	0.09
14	[0.05,0.1]	[0.05,0.1]	[0.0.01]	[0.001,0.002]	0	8	2	0	126.2	0.7182	0.1
15	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.0.001]	0	7	3	0	136.7	0.7222	0.1
16	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]	0	7	3	0	136.7	0.7218	0.141



Moreover, in Table 23 more dedicated facilities are opened when holding cost is low and demand is high. If we compare experiment 769 with 770, and experiment 771 with 772, we can see the effects of demand on the number of dedicated facilities. The effect of holding cost on the number of dedicated facilities can be seen by comparing experiment 770 with 962, and experiment 772 with 964. These results are consistent with our findings in Chapter 2. In Table 23, the cost parameters are;  $f = 10$ ,  $\hat{f} = 1$ ,  $c^{in} = 0.05$ ,  $c^{out} = 0.075$ , and  $c^e = 1$ . Demand rates  $d_1, d_2 = [0, 0.05]$ , and  $\alpha = 0.7$ .

Table 23. Number of dedicated facilities with respect to holding cost and demand

Exp #	Input Parameters				Output						
	$h$	$d_0$	$d_1$	$\hat{d}$	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt solTime
769	0.5	[0,0.05]	[0,0.01]	[0,0.001]	0	10	0	0	205.1	0.7148	0.22
770	0.5	[0,0.05]	[0,0.01]	[0.001,0.002]	1	9	0	12	202.6	0.7004	0.3
771	0.5	[0,0.05]	[0.01,0.02]	[0,0.001]	0	8	2	0	246.1	0.7048	0.201
772	0.5	[0,0.05]	[0.01,0.02]	[0.001,0.002]	0	9	1	13	245.1	0.7002	0.31
773	0.5	[0.05,0.1]	[0,0.01]	[0,0.001]	1	9	0	0	184.7	0.7276	0.2
774	0.5	[0.05,0.1]	[0,0.01]	[0.001,0.002]	1	9	0	0	184.7	0.7231	0.191
775	0.5	[0.05,0.1]	[0.01,0.02]	[0,0.001]	0	10	0	0	205.1	0.7378	0.21
776	0.5	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]	0	10	0	0	205.1	0.7358	0.2
961	1	[0,0.05]	[0,0.01]	[0,0.001]	0	10	0	0	210.1	0.7148	0.231
962	1	[0,0.05]	[0,0.01]	[0.001,0.002]	0	10	0	0	210.1	0.714	0.28
963	1	[0,0.05]	[0.01,0.02]	[0,0.001]	0	8	2	0	252.1	0.7048	0.231
964	1	[0,0.05]	[0.01,0.02]	[0.001,0.002]	0	8	2	0	252.1	0.7059	0.32
965	1	[0.05,0.1]	[0,0.01]	[0,0.001]	1	9	0	0	189.2	0.7276	0.23
966	1	[0.05,0.1]	[0,0.01]	[0.001,0.002]	1	9	0	0	189.2	0.7231	0.221
967	1	[0.05,0.1]	[0.01,0.02]	[0,0.001]	0	10	0	0	210.1	0.7378	0.22
968	1	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]	0	10	0	0	210.1	0.7358	0.23

### *Performance of heuristic for multiple pool problem with dedicated facilities*

For this small size problem ( $|P| = 10$  and  $|J_p| = 5 \forall p \in P$ ), we see that the average gap between the heuristic solution and the optimal solution is 1.7%. On average, the heuristic takes less than 0.01 seconds to get within this range of the optimal solution. However, the main benefit of the heuristic is in dealing with larger size problems. In order to test the performance of the heuristic, we run the examples in Table 20 using the heuristic, the results of which can be seen in Table 24.

Table 24. Performance of the heuristic for larger problems

$ P $	$ J $	Opt sol time/s	H sol time/s	LB sol time/s	H-LB gap	H-Opt gap
10	5	0.45	0.01	0.04	0.013091	6.59E-06
25	5	2.233	0.02	0.09	0.019752	0.016099
50	5	32.437	0.06	0.19	0.021562	0.019756
2	5	0.07	0.01	0.03	0.007392	0
2	10	1.382	0.01	0.3	0.020847	2.03E-05
2	11	4.136	0.01	0.581	0.020301	0
2	12	14.221	0.01	1.202	0.009848	0
2	13	51.645	0.01	2.544	0.023617	0

In the above table, “H” stands for heuristic, and “LB” is the lower bound obtained from solving the LP relaxation of the optimization model. Notice that the heuristic provides an upper bound within 1.97% of the optimal almost instantly, and the maximum gap between the heuristic upper bound and the LP lower bound is 2.36%. Moreover, the heuristic seems to take longer as  $|P|$  increases, but still shorter than the Xpress-MP solver used for optimization. A plot of the heuristic solution time versus optimization solution time with respect to  $|J|$  is given in Figure 24.

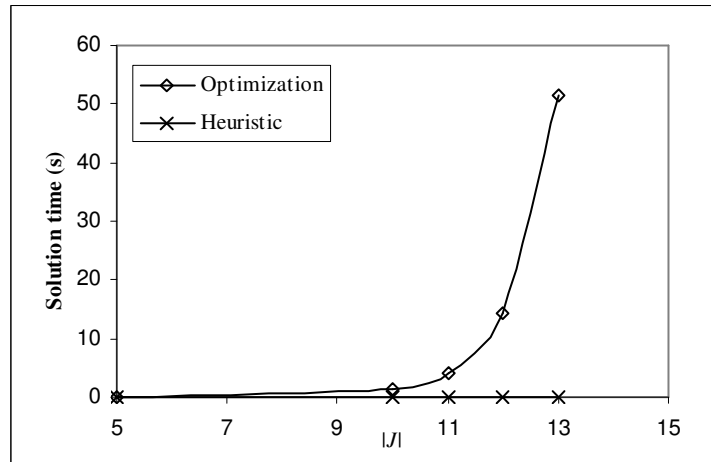


Figure 24. Solution time with respect to  $|J|$

### ***Benefit of inventory sharing and dedicated facilities in NDIP***

Before concluding this chapter, we would like to compare the performance of the different models formulated in the literature as well as in this dissertation. The different models that we would like to compare are

1. Network design and inventory problem (Jeet (2006)),
2. Network design and inventory problem with dedicated facilities (Chapter 2),
3. Network design and inventory sharing problem (Chapter 3), and
4. Network design and inventory sharing problem with dedicated facilities (Chapter 4).

We now compare the performance of each of the above models for two different customer networks; a sparse distribution as seen in Figure 25, and a relatively denser distribution (Figure 26). The sparse network is generated by simply increasing the spacing between customers. Both networks consist of 8 facilities and 80 customers out of which 20 are potential dedicated facilities.

In terms of solution procedures, model (2) is solved using formulation  $\mathbf{P}_2$  in Chapter 2, and model (1) is solved using the same formulation but the set of dedicated facilities  $I'=\emptyset$  is empty. When experimenting with models (3) and (4), we first group the customers and shared facilities into 4 pools such that each pool has 2 facilities. Then model (4) is solved using formulation  $\mathbf{P}_{5''}$ , and model (3) uses the same formulation with  $J^p=\emptyset \quad \forall p \in P$ .

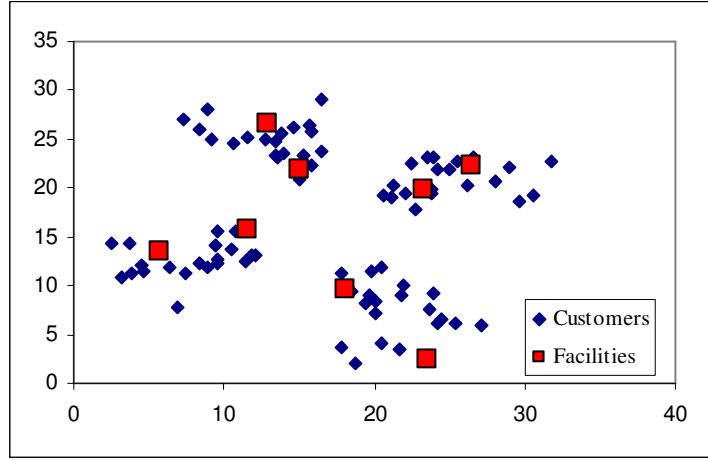


Figure 25. Sparse distribution of customers

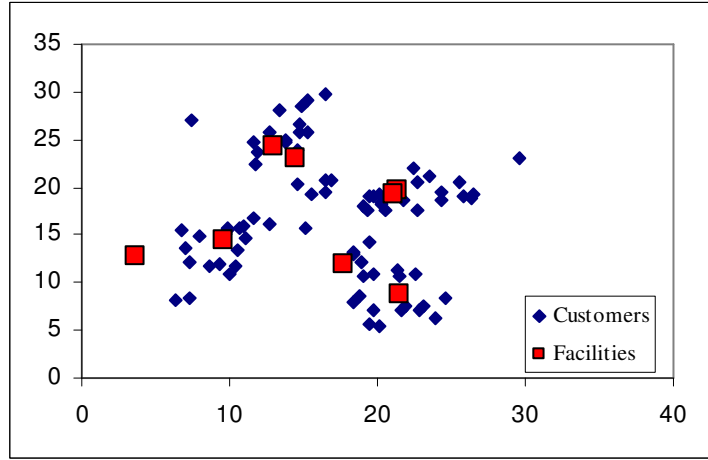


Figure 26. Dense distribution of customers

In order to perform a fair comparison of each of the models above, we set  $c^e = 0$  in models (3) and (4). Moreover, in models (1) and (2), we replace  $c_{i''j}$  with  $c^{in} = 0.05$  if customer  $j$  is within the time window of shared facility  $i''$  and with  $c^{out} = 0.075$  if not. By doing so, we can now compare the objective function values across models (1)-(4).

We run an experiment varying  $f$ ,  $\hat{f}$ ,  $h$ , and  $\alpha$ , as well as the mean demand rate of each customer. For the following ranges of parameter values

- $f = \{10, 20\}$
- $\hat{f} = \{1, 2\}$
- $h = \{0.5, 1.0\}$
- $\alpha = \{0.70, 0.75\}$
- $d_j = \{low, high\}$

where a “*low*” value for  $d_j$  corresponds to demand rates in the range of  $[0.0025, 0.005]$  for customers with dedicated facilities and demand in the range of  $[0.00025, 0.0005]$  for the rest of the customers, and a “*high*” value of  $d_j$  corresponds to demand rates ranging from  $[0.005, 0.01]$  for customers with dedicated facilities and  $[0.0005, 0.001]$  for the rest. Remember that these are all weekly demand rates, which is why the values are fairly small. The replenishment rate is  $\mu = 4$  per week for these experiments.

The experimental results for the sparse network are given in Table 25, and Table 26 shows the results for the dense network. In each of the experiments, we are interested in the objective value and solution time of models (1)-(4). Note that all the models were run on a Pentium M 1.4 GHz processor with 512 MB of RAM.

Table 25. Model comparison results for sparse network

Exp #	Input					Output							
	$f$	$\hat{f}$	$h$	$\alpha$	$d_j$	(1) NDIP		(2) NDIP w/ded facs		(3) Inv Sharing		(4) Inv Sharing w/ded facs	
						Obj	Time	Obj	Time	Obj	Time	Obj	Time
1	10	1	0.5	0.6	<i>low</i>	43.505	20.349	21.003	2.814	52.504	0.07	16.5	0.141
2	10	1	0.5	0.7	<i>low</i>	63.004	9.784	24.002	3.385	63.004	0.06	19.5	0.1
3	10	1	1	0.6	<i>low</i>	47.005	26.638	25.003	0.741	55.004	0.06	22	0.13
4	10	1	1	0.7	<i>low</i>	66.004	8.683	29.002	4.757	66.004	0.06	26	0.09
5	10	2	0.5	0.6	<i>low</i>	43.505	19.758	28.003	2.273	52.504	0.05	27.5	0.13
6	10	2	0.5	0.7	<i>low</i>	63.004	9.804	33.002	3.285	63.004	0.06	32.5	0.09
7	10	2	1	0.6	<i>low</i>	47.005	26.749	32.003	3.215	55.004	0.06	32.001	0.211
8	10	2	1	0.7	<i>low</i>	66.004	8.662	38.002	4.787	66.004	0.06	38.001	0.15
9	20	1	0.5	0.6	<i>low</i>	83.505	14.131	31.003	2.704	102.5	0.06	16.5	0.12
10	20	1	0.5	0.7	<i>low</i>	123	11.186	34.002	3.354	123	0.06	19.5	0.09
11	20	1	1	0.6	<i>low</i>	87.005	27.9	35.003	0.741	105	0.051	22	0.13
12	20	1	1	0.7	<i>low</i>	126	9.934	39.002	4.196	126	0.05	26	0.091
13	20	2	0.5	0.6	<i>low</i>	83.505	14.12	38.003	2.724	102.5	0.06	27.5	0.12
14	20	2	0.5	0.7	<i>low</i>	123	11.216	43.002	3.625	123	0.06	32.5	0.09
15	20	2	1	0.6	<i>low</i>	87.005	28.08	42.003	2.774	105	0.06	33	0.13
16	20	2	1	0.7	<i>low</i>	126	9.954	48.002	3.375	126	0.06	39	0.1
17	10	1	0.5	0.6	<i>high</i>	52.509	28.891	21.006	2.343	52.509	0.06	16.5	0.17
18	10	1	0.5	0.7	<i>high</i>	63.009	5.378	24.005	5.368	63.009	0.051	19.5	0.1
19	10	1	1	0.6	<i>high</i>	55.009	50.613	25.006	2.283	55.009	0.07	22	0.13
20	10	1	1	0.7	<i>high</i>	66.009	8.983	29.005	3.785	66.009	0.06	26	0.1
21	10	2	0.5	0.6	<i>high</i>	52.509	27.93	28.006	1.823	52.509	0.05	27.5	0.131
22	10	2	0.5	0.7	<i>high</i>	63.009	5.358	33.005	4.667	63.009	0.05	32.5	0.11
23	10	2	1	0.6	<i>high</i>	55.009	50.873	32.006	5.708	55.009	0.06	32.001	0.34
24	10	2	1	0.7	<i>high</i>	66.009	8.983	38.005	4.386	66.009	0.06	38.001	0.17
25	20	1	0.5	0.6	<i>high</i>	102.51	18.907	31.006	2.254	102.51	0.06	16.5	0.121
26	20	1	0.5	0.7	<i>high</i>	123.01	8.893	34.005	5.307	123.01	0.05	19.5	0.1
27	20	1	1	0.6	<i>high</i>	105.01	33.568	35.006	2.273	105.01	0.05	22	0.15
28	20	1	1	0.7	<i>high</i>	126.01	5.448	39.005	4.015	126.01	0.05	26	0.11
29	20	2	0.5	0.6	<i>high</i>	102.51	20.029	38.006	6.229	102.51	0.05	27.5	0.13
30	20	2	0.5	0.7	<i>high</i>	123.01	9.033	43.005	4.186	123.01	0.05	32.5	0.111
31	20	2	1	0.6	<i>high</i>	105.01	32.817	42.006	2.274	105.01	0.05	33	0.13
32	20	2	1	0.7	<i>high</i>	126.01	5.127	48.005	3.565	126.01	0.06	39	0.1

Table 26. Model comparison results for dense network

Exp #	Input					Output							
	$f$	$\hat{f}$	$h$	$\alpha$	$d_j$	(1) NDIP		(2) NDIP w/ded facs		(3) Inv Sharing		(4) Inv Sharing w/ded facs	
						Obj	Time	Obj	Time	Obj	Time	Obj	Time
1	10	1	0.5	0.6	low	31.505	11.827	20.004	5.037	31.503	0.07	16.5	0.13
2	10	1	0.5	0.7	low	42.004	27.74	22.503	0.881	42.003	0.06	19.5	0.11
3	10	1	1	0.6	low	33.005	23.654	24.004	5.268	33.003	0.07	22	0.12
4	10	1	1	0.7	low	44.005	64.773	27.003	0.931	44.003	0.07	26	0.12
5	10	2	0.5	0.6	low	31.505	11.757	26.004	4.437	31.503	0.06	25.501	0.051
6	10	2	0.5	0.7	low	42.004	27.569	30.503	1.622	42.003	0.061	30.501	0.06
7	10	2	1	0.6	low	33.005	23.745	30.004	82.839	33.003	0.06	29.001	0.06
8	10	2	1	0.7	low	44.005	64.382	35.003	41.179	44.003	0.05	35.001	0.06
9	20	1	0.5	0.6	low	61.505	19.689	30.004	4.897	61.503	0.06	16.5	0.13
10	20	1	0.5	0.7	low	82.005	22.061	32.503	0.872	82.003	0.06	19.5	0.16
11	20	1	1	0.6	low	63.005	56.572	34.004	5.147	63.003	0.06	22	0.151
12	20	1	1	0.7	low	84.004	21.631	37.003	0.891	84.003	0.06	26	0.15
13	20	2	0.5	0.6	low	61.505	19.698	36.004	6.019	61.503	0.05	27.5	0.15
14	20	2	0.5	0.7	low	82.005	22.172	40.503	0.871	82.003	0.06	32.5	0.15
15	20	2	1	0.6	low	63.005	56.401	40.004	3.585	63.003	0.06	33	0.14
16	20	2	1	0.7	low	84.004	21.481	45.003	0.882	84.003	0.06	39	0.131
17	10	1	0.5	0.6	high	31.509	6.449	21.006	123.16	31.506	0.06	16.5	0.13
18	10	1	0.5	0.7	high	42.009	43.263	24.005	8.012	42.006	0.06	19.5	0.07
19	10	1	1	0.6	high	33.009	6.779	25.006	34.73	33.006	0.06	22	0.13
20	10	1	1	0.7	high	44.009	33.729	29.005	5.568	44.006	0.06	26	0.071
21	10	2	0.5	0.6	high	31.509	6.329	28.006	20.439	31.506	0.06	27.5	0.31
22	10	2	0.5	0.7	high	42.009	43.643	32.007	32.056	42.006	0.07	32.5	0.28
23	10	2	1	0.6	high	33.009	7.09	31.008	183.22	33.006	0.061	31.003	0.341
24	10	2	1	0.7	high	44.009	34.51	36.007	39.186	44.006	0.06	36.006	0.26
25	20	1	0.5	0.6	high	61.509	14.821	31.006	52.766	61.506	0.06	16.5	0.121
26	20	1	0.5	0.7	high	82.009	57.122	34.005	4.927	82.006	0.06	19.5	0.06
27	20	1	1	0.6	high	63.009	6.539	35.006	56.201	63.006	0.06	22	0.13
28	20	1	1	0.7	high	84.009	47.929	39.005	7.911	84.006	0.06	26	0.07
29	20	2	0.5	0.6	high	61.509	14.671	38.006	41.079	61.506	0.06	27.5	0.12
30	20	2	0.5	0.7	high	82.009	56.461	43.005	6.51	82.006	0.07	32.5	0.07
31	20	2	1	0.6	high	63.009	6.499	42.006	37.113	63.006	0.06	33	0.161
32	20	2	1	0.7	high	84.009	46.637	48.005	8.482	84.006	0.061	39	0.07

Across both sparse and dense networks, we see that model (2) always gives the same or better solutions than model (1) in less time. This supports the observation in Chapter 2 that adding dedicated facilities to the model can help with respect to solution time as well (although the model is in fact a generalization of the model without dedicated facilities). In Chapter 2, we also observed that more dedicated facilities are opened in sparse

networks. A comparison of the reduction in the objective value from model (1) to model (2) in both networks supports this observation.

Similarly, compared to model (1), model (3) is always solved almost instantly. However, this solution is worse than that of model (1) when demand is low in the sparse network. Intuitively, this makes sense because demand in the overlapping region of both facilities is low, and hence the degree of sharing is reduced (which we also observed in Section 4 of Chapter 3).

Most importantly, a comparison of models (1) and (4) reflects the contribution of this dissertation. Compared to model (1), model (4) provides an average cost reduction of 63.8% in the sparse network and 46.5% in the dense network. Model (4) achieves this within 1% of the time taken by model (1). Figure 27 is a plot of the objective value versus solution time for each of the models in the dense network. The results of model (4) are clustered in the lower left corner of the plot. Therefore, the main contribution of this dissertation is that we provide a framework to solve a more realistic problem (NDIP with dedicated facilities and inventory sharing) such that we get a better solution in much less time.

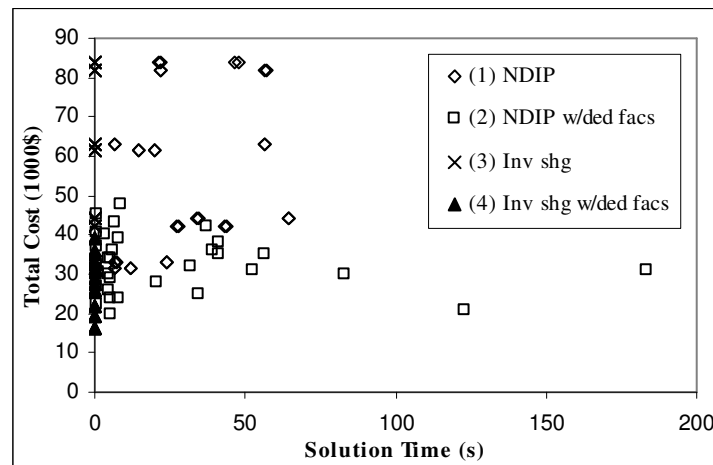


Figure 27. Solution quality and time of each model



Note that models (3) and (4) have certain restrictions; stock level at each facility can be at most 1 unit, and customers cannot be assigned to facilities outside of their pool. However, in a sparse network with low demand customers, the stock level required is low enough that the unit stock level restriction does not apply to models (1) and (2) anyway. Moreover, since the network is sparse, customers in models (1) and (2) are too far from the facilities in the other pools. Therefore, they are not assigned to facilities outside of their pool anyway. As a result, these restrictions do not hinder us from deriving conclusions from the experimental results.

## **4 Conclusions**

In this chapter we formulate the network design and inventory problem with inventory sharing and dedicated facilities. Although the formulation is nonlinear, we provide an alternative formulation that has a binary knapsack structure. However, this formulation has a large number of variables.

In an attempt to find a better solution procedure, we first identified an algorithm to solve a special case problem (single pool with one potential dedicated facility). Then we constructed another heuristic for the multiple pool problem by combining the greedy heuristic for multiple pools (from Chapter 3) and extending the single pool algorithm (from this chapter). Using branch and bound (in XpressMP) to solve a problem with 2 pools and 13 dedicated facilities takes almost a minute, whereas the heuristic solves the same problem within 0.01 seconds.

While comparing the different formulations in this dissertation with respect to a given distribution of customers, we find that the multiple pool inventory sharing problem with dedicated facilities (from Chapter 4) provides an average cost reduction of 40-60% over the network design and inventory problem from the literature (Jeet (2006)). This reduction is obtained within 1% of the solution time. Experimental results also show that

adding dedicated facilities to the solution procedure always helps with respect to the objective value and/or solution time, whereas inventory sharing may hurt with respect to the objective value especially in sparse networks with very low demand customers.

Another interesting non-intuitive result is that in some cases, additional demand to the system helps reduce cost and/or increase service. This is due to the assumption that each shared facility has to share inventory with the other shared facility in the pool.

## Chapter 5: Conclusions and Future Research

In this dissertation, we added two features to the existing network design and inventory optimization problem. We allow some customers to have dedicated facilities on-site, and we allow shared facilities to share inventory with one other facility. By taking advantage of the low demand nature of parts in SPL, we were able to formulate the problem with a binary knapsack structure.

Some of the major contributions of this dissertation are as follows.

- In the risk pooling problem, we discovered that the constraint was non-decreasing with respect to one of the variables. The non-linear integer problem could then be solved by simply evaluating a small set of undominated solutions. Moreover, we identify conditions where the optimal solution is complete centralization or complete decentralization. We also observe that the range of parameter values for which partial decentralization is optimal is very small.
- In the inventory sharing problem, we discovered that for given stock levels, demand allocation decisions are trivial. This is due to the dominance of certain variables over others with respect to the objective function and constraint coefficients. As a result, we were able to formulate the multiple pool sharing problem as a binary knapsack problem which can be solved easily.
- We formulated the combined problem of inventory sharing with customer dedicated facilities and constructed a heuristic that solves the problem in a short amount of time.

The main limitations of the model in Chapter 4 are that we assume small pool sizes of just two facilities each, and each facility being able to stock at most one unit of inventory. However, as a follow up to the work in this dissertation, we hope to generalize our results to cases with

- more than two potential shared facilities in a pool, and
- each shared facility being able to stock more than one unit of inventory.

In Chapter 4, we constructed a heuristic to obtain upper bounds, but we did not revise stock level decisions after making decisions on dedicated facilities. In the future, we would like to modify the heuristic so that we can obtain better upper bounds. As an alternative solution procedure, we would also like attempt to solve the multiple pool problem in Chapter 4 using branch and price since the problem has a large number of variables.

Furthermore, we would like to extend the formulation in Chapter 4 to include multiple parts with part commonality. The benefit of inventory sharing is further enhanced by part commonality. This could be achieved in combination with the work of Jeet (2006) in part commonality.

In the future, the model from Chapter 4 could be used in contract pricing for new customers. The additional demand could potentially improve service and/or reduce cost, as we have seen in Chapter 4.

## Appendices

### Appendix A – Linearized Formulation for NDIP (with sos2 variables)

$$\text{Minimize } \sum_{i' \in I'} (f_{i'} + h_{i'}) Y_{i'} + \sum_{i'' \in I''} (f_{i''} Y_{i''} + h_{i''} S_{i''}) + \sum_{i' \in I'} \sum_{j \in J} c_{i'j} d_j X_{i'j} \quad (\text{A-a})$$

$$\text{Subject to } Y_{i'} + \sum_{i'' \in I''} X_{i'j} = 1 \quad \forall j \in I' \quad (\text{A-b})$$

$$\sum_{i'' \in I''} X_{i'j} = 1 \quad \forall j \in J \setminus I' \quad (\text{A-c})$$

$$X_{i''j} \leq Y_{i''} \quad \forall i'' \in I'', j \in J \quad (\text{A-d})$$

$$\sum_{\substack{i' \in I', \\ j \in J \\ i'=j}} d_j Y_{i'} + \sum_{i'' \in I''} \sum_{j \in J_r} \delta_{i''j} d_j Z_{i''j} \geq \alpha_r \sum_{j \in J_r} d_j \quad \forall r \in R \quad (\text{A-e})$$

$$S_{i''} \leq s_{\max} Y_{i''} \quad \forall i'' \in I'' \quad (\text{A-f})$$

$$\lambda_{i''} = t_{i''} \sum_{j \in J} d_j X_{i''j} \quad \forall i'' \in I'' \quad (\text{A-g})$$

$$\lambda_{i''} \leq \sum_{b \in B} db_b U_{i''b} \quad \forall i'' \in I'' \quad (\text{A-h})$$

$$S_{i''} \geq \sum_{\bar{s} \in \bar{S}} \bar{s} V_{i''\bar{s}} \quad \forall i'' \in I'' \quad (\text{A-i})$$

$$\beta_{i''} \leq \sum_{b \in B} \sum_{\bar{s} \in \bar{S}} p_{b\bar{s}} w_{i''b\bar{s}} \quad \forall i'' \in I'' \quad (\text{A-j})$$

$$\sum_{b \in B} U_{i''b} = 1 \quad \forall i'' \in I'' \quad (\text{A-k})$$

$$\sum_{\bar{s} \in \bar{S}} V_{i''\bar{s}} = 1 \quad \forall i'' \in I'' \quad (\text{A-l})$$

$$W_{i''b\bar{s}} \geq U_{i''b} + V_{i''\bar{s}} - 1 \quad \forall i'' \in I'', b \in B, \bar{s} \in \bar{S} \quad (\text{A-m1})$$

$$W_{i''b\bar{s}} \leq U_{i''b} - V_{i''\bar{s}} + 1 \quad \forall i'' \in I'', b \in B, \bar{s} \in \bar{S} \quad (\text{A-m2})$$

$$W_{i''b\bar{s}} \leq U_{i''b} \quad \forall i'' \in I'', b \in B, \bar{s} \in \bar{S} \quad (\text{A-m3})$$

$$W_{i''b\bar{s}} \leq V_{i''\bar{s}} \quad \forall i'' \in I'', b \in B, \bar{s} \in \bar{S} \quad (\text{A-m4})$$

$$Z_{i'j} \geq \beta_{i'} + X_{i'j} - 1 \quad \forall i' \in I'', j \in J \quad (\text{A-n1})$$

$$Z_{i''j} \leq \beta_{i''} - X_{i''j} + 1 \quad \forall i'' \in I'', j \in J \quad (\text{A-n2})$$

$$Z_{i''j} \leq \beta_{i''} \quad \forall i'' \in I'', j \in J \quad (\text{A-n3})$$

$$Z_{i''j} \leq X_{i''j} \quad \forall i'' \in I'', j \in J \quad (\text{A-n4})$$

$$X_{i''j} \in \{0,1\} \quad \forall i'' \in I'', j \in J \quad (\text{A-o})$$

$$Y_{i'} \in \{0,1\} \quad \forall i' \in I' \quad (\text{A-p})$$

$$Y_{i''} \in \{0,1\} \quad \forall i'' \in I'' \quad (\text{A-q})$$

$$S_{i''} \in \bar{S} \quad \forall i'' \in I'' \quad (\text{A-r})$$

$$\lambda_{i''} \geq 0 \quad \forall i'' \in I'' \quad (\text{A-s})$$

$$\beta_{i''} \geq 0 \quad \forall i'' \in I'' \quad (\text{A-t})$$

$$0 \leq U_{i''b} \leq 1 \quad \forall i'' \in I'', b \in B \quad (\text{A-u})$$

$$V_{i''\bar{s}} \in \{0,1\} \quad \forall i'' \in I'', \bar{s} \in \bar{S} \quad (\text{A-v})$$

$$W_{i''b\bar{s}} \in \{0,1\} \quad \forall i'' \in I'', b \in B, \bar{s} \in \bar{S} \quad (\text{A-w})$$

$$0 \leq Z_{i''j} \leq 1 \quad \forall i'' \in I'', j \in J \quad (\text{A-x})$$

where  $\bar{S} = \{0,1,2,\dots,s_{\max}\}$  is the set of feasible base stock levels,

$B$  is the set of demand break points,

$db_b$  is the demand at break point  $b$ ,

$p_{b\bar{s}}$  is the fill rate when mean demand is  $b$  and a base stock level is  $\bar{s}$ ,

$V_{i''\bar{s}}$  is a binary variable set to 1 if shared facility  $i''$  is stocked with  $\bar{s}$  units,

$U_{i''b}$  is a sos2 variable used for interpolation,

$W_{i''b\bar{s}}$  is a temporary binary variable for linearization purposes, and

$Z_{i''j}$  is a temporary continuous variable for linearization purposes.

Constraints (A-a) through (A-g) have already been discussed in the NDIP nonlinear formulation. For each shared facility, constraint (A-h) assigns a mean demand value, constraint (A-i) assigns a base stock level, and constraint (A-j) assigns a fill rate.

Constraint (A-k) ensures that each shared facility is assigned a convex combination of two consecutive demand break points, and Constraint (A-l) ensures that every shared facility is assigned exactly one value as base stock level. For linearization purposes, constraints (A-m1) through (A-m4) set variable  $W_{i^*b\bar{s}}$  to the product of variables  $U_{i^*b}$  and  $V_{i^*\bar{s}}$ . Similarly, constraints (A-n1) through (A-n4) set variable  $Z_{i^*j}$  to the product of variables  $\beta_{i^*}$  and  $X_{i^*j}$ . The rest are non-negativity constraints.

Note that a sos2 variable is an ordered set of variables containing at most two non-zero elements, both of which have to be consecutive in their ordering. This enables us to easily interpolate between consecutive demand break points such that we obtain a convex combination of the two points.

**Appendix B – NDIP Formulation for Customer-Centric Service Levels and no dedicated facilities**

$$\text{Minimize } \sum_{i' \in I'} (f_{i'} + h_{i'}) Y_{i'} + \sum_{i'' \in I''} f_{i''} Y_{i''} + \sum_{i'' \in I''} \sum_{j \in J} \sum_{g \in G_{i''}} c_{i''j} d_j X_{i''jg} + \sum_{i'' \in I''} \sum_{g \in G_{i''}} \sum_{s \in S} sh_{i''} W_{i''gs} \quad (\text{B-a})$$

$$\text{Subject to } Y_{i'} + \sum_{i'' \in I''} \sum_{g \in G_{i''}: g \geq \alpha_j} X_{i''jg} = 1 \quad \forall j \in I' \quad (\text{B-b})$$

$$\sum_{i'' \in I''} \sum_{g \in G_{i''}: g \geq \alpha_j} X_{i''jg} = 1 \quad \forall j \in J \setminus I' \quad (\text{B-c})$$

$$Y_{i''} \geq \sum_{g \in G_{i''}} \sum_{s \in S} W_{i''gs} \quad \forall i'' \in I'' \quad (\text{B-d})$$

$$M \cdot \sum_{k=s+1}^{\hat{s}_{i''g}} W_{i''gs} \geq t_{i''} \sum_{j \in J_{i''}} d_j X_{i''jg} - b_{gs} \quad \forall i'' \in I'', g \in G_{i''}, s \in S \quad (\text{B-e})$$

$$X_{i''jg} \in \{0,1\} \quad \forall i'' \in I'', j \in J, g \in G_{i''} \quad (\text{B-f})$$

$$y_{i'} \in \{0,1\} \quad \forall i' \in I' \quad (\text{B-g})$$

$$y_{i''} \in \{0,1\} \quad \forall i'' \in I'' \quad (\text{B-h})$$

$$w_{i''gs} \in \{0,1\} \quad \forall i'' \in I'', g \in G_{i''}, s \in S \quad (\text{B-i})$$

where

$$J_{i''} = \{j \in J : \delta_{i''j} = 1\}$$

$$I''_j = \{i'' \in I'' : \delta_{i''j} = 1\}$$

$$G_{i''} = \{\alpha_j : j \in J_{i''}\}$$

$$1 - \frac{\frac{b_{gs}^s}{s!}}{\sum_{k=0}^s \frac{b_{gs}^k}{k!}} = g \quad \forall g \in G_{i''}, s \in S$$

$$1 - \frac{\frac{b_{g\hat{s}_{i''g}}^{\hat{s}_{i''g}}}{\hat{s}_{i''g}!}}{\sum_{k=0}^{\hat{s}_{i''g}} \frac{b_{gk}}{k!}} = g \quad \forall i'' \in I'', g \in G_{i''}$$



In the above formulation, the binary assignment variable  $X_{ijg}$  is 1 if customer  $j$  is assigned to shared facility  $i$  that has fill rate  $g$ , and 0 otherwise. The lead time demand corresponding to base stock level  $s$  and fill rate  $g$  is a parameter denoted by  $b_{gs}$ , and  $\hat{s}_{ig}$  is another parameter that denotes the maximum potential inventory level at shared facility  $i$  to guarantee fill rate  $g$ . A new stock picking binary variable  $W_{igs}$  is also included in the model.

The updated objective function is seen as constraint (B-a). Constraints (B-b) and (B-c) are the combined assignment and service level constraints. Constraint (B-d) ensures that shared facilities are stocked only if they are opened, and constraint (B-e) assigns the stock picking variable appropriately. The rest are non-negativity constraints.

## Appendix C – DOE Results for a High Density Network

Exp	INPUT						OUTPUT											
	$f_r$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
1	0	0	0.6	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	7.411	Opt	45	0
2	0	0	0.6	0.005	50	100	25	9	25	45	0	1.15266	0	1.1527	7.14	Opt	54	0
3	0	0	0.6	0.005	100	0	50	0	50	0	0	0	0	0	0.181	Opt	1	0
4	0	0	0.6	0.005	100	100	50	0	50	0	0	0	0	0	0.26	Opt	1	0
5	0	0	0.6	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	8.652	Opt	102	0
6	0	0	0.6	0.01	50	100	25	9	25	45	0	2.30531	0	2.3053	6.86	Opt	55	0
7	0	0	0.6	0.01	100	0	50	0	50	0	0	0	0	0	0.181	Opt	1	0
8	0	0	0.6	0.01	100	100	50	0	50	0	0	0	0	0	0.25	Opt	1	0
9	0	0	0.8	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	8.082	Opt	156	0
10	0	0	0.8	0.005	50	100	25	9	25	45	0	1.15266	0	1.1527	8.191	Opt	62	0
11	0	0	0.8	0.005	100	0	50	0	50	0	0	0	0	0	0.191	Opt	1	0
12	0	0	0.8	0.005	100	100	50	0	50	0	0	0	0	0	0.26	Opt	1	0
13	0	0	0.8	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	8.693	Opt	154	0
14	0	0	0.8	0.01	50	100	25	9	25	45	0	2.30531	0	2.3053	9.463	Opt	313	0
15	0	0	0.8	0.01	100	0	50	0	50	0	0	0	0	0	0.181	Opt	1	0
16	0	0	0.8	0.01	100	100	50	0	50	0	0	0	0	0	0.27	Opt	1	0
17	0	0.1	0.6	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	7.841	Opt	128	0
18	0	0.1	0.6	0.005	50	100	2	8	2	8	0	2.1507	1	3.1507	11.557	Opt	145	0
19	0	0.1	0.6	0.005	100	0	50	0	50	0	0	0	5	5	0.19	Opt	1	0
20	0	0.1	0.6	0.005	100	100	4	8	4	8	0	1.93606	1.2	3.1361	6.109	Opt	38	0
21	0	0.1	0.6	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	8.062	Opt	72	0
22	0	0.1	0.6	0.01	50	100	11	8	11	8	0	3.08283	1.9	4.9828	8.161	Opt	37	0
23	0	0.1	0.6	0.01	100	0	50	0	50	0	0	0	5	5	0.201	Opt	1	0
24	0	0.1	0.6	0.01	100	100	30	4	30	4	0	0.8982	3.4	4.2982	3.705	Opt	22	0
25	0	0.1	0.8	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	6.129	Opt	37	0
26	0	0.1	0.8	0.005	50	100	2	8	2	8	0	2.1507	1	3.1507	5.307	Opt	21	0
27	0	0.1	0.8	0.005	100	0	50	0	50	0	0	0	5	5	0.21	Opt	1	0
28	0	0.1	0.8	0.005	100	100	4	8	4	8	0	1.93606	1.2	3.1361	8.202	Opt	36	0
29	0	0.1	0.8	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	8.492	Opt	63	0
30	0	0.1	0.8	0.01	50	100	11	8	11	8	0	3.08283	1.9	4.9828	11.386	Opt	123	0
31	0	0.1	0.8	0.01	100	0	50	0	50	0	0	0	5	5	0.211	Opt	1	0
32	0	0.1	0.8	0.01	100	100	30	4	30	4	0	0.8982	3.4	4.2982	4.015	Opt	17	0
33	0	0.2	0.6	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	5.448	Opt	26	0
34	0	0.2	0.6	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	7.451	Opt	93	0
35	0	0.2	0.6	0.005	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
36	0	0.2	0.6	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	8.232	Opt	64	0
37	0	0.2	0.6	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	7.861	Opt	36	0
38	0	0.2	0.6	0.01	50	100	2	8	2	8	0	4.3014	2	6.3014	8.423	Opt	71	0
39	0	0.2	0.6	0.01	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
40	0	0.2	0.6	0.01	100	100	4	8	4	8	0	3.87212	2.4	6.2721	8.622	Opt	75	0
41	0	0.2	0.8	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	7.371	Opt	51	0
42	0	0.2	0.8	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	6.099	Opt	17	0
43	0	0.2	0.8	0.005	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
44	0	0.2	0.8	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	9.694	Opt	104	0
45	0	0.2	0.8	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	9.123	Opt	75	0
46	0	0.2	0.8	0.01	50	100	2	8	2	8	0	4.3014	2	6.3014	7.972	Opt	26	0
47	0	0.2	0.8	0.01	100	0	50	0	50	0	0	0	10	10	0.22	Opt	1	0
48	0	0.2	0.8	0.01	100	100	4	8	4	8	0	3.87212	2.4	6.2721	9.063	Opt	71	0

Exp	INPUT						OUTPUT											
	$f_i$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
49	0.2	0	0.6	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	7.361	Opt	45	0
50	0.2	0	0.6	0.005	50	100	0	10	0	50	0	2.41733	0	2.4173	6.729	Opt	13	0
51	0.2	0	0.6	0.005	100	0	50	0	50	0	10	0	0	10	0.221	Opt	1	0
52	0.2	0	0.6	0.005	100	100	0	10	0	50	0	2.41733	0	2.4173	8.532	Opt	181	0
53	0.2	0	0.6	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	8.943	Opt	102	0
54	0.2	0	0.6	0.01	50	100	2	10	2	50	0.4	4.24274	0	4.6427	7.391	Opt	34	0
55	0.2	0	0.6	0.01	100	0	50	0	50	0	10	0	0	10	0.22	Opt	1	0
56	0.2	0	0.6	0.01	100	100	4	10	4	50	0.8	3.81347	0	4.6135	24.876	Opt	636	0
57	0.2	0	0.8	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	8.492	Opt	156	0
58	0.2	0	0.8	0.005	50	100	0	10	0	50	0	2.41733	0	2.4173	8.773	Opt	185	0
59	0.2	0	0.8	0.005	100	0	50	0	50	0	10	0	0	10	0.22	Opt	1	0
60	0.2	0	0.8	0.005	100	100	0	10	0	50	0	2.41733	0	2.4173	12.668	Opt	189	0
61	0.2	0	0.8	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	9.013	Opt	154	0
62	0.2	0	0.8	0.01	50	100	2	10	2	50	0.4	4.24274	0	4.6427	8.162	Opt	24	0
63	0.2	0	0.8	0.01	100	0	50	0	50	0	10	0	0	10	0.23	Opt	1	0
64	0.2	0	0.8	0.01	100	100	4	10	4	50	0.8	3.81347	0	4.6135	8.813	Opt	98	0
65	0.2	0.1	0.6	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	8.242	Opt	128	0
66	0.2	0.1	0.6	0.005	50	100	0	8	0	8	0	2.44666	0.8	3.2467	5.898	Opt	21	0
67	0.2	0.1	0.6	0.005	100	0	50	0	50	0	10	0	5	15	0.231	Opt	1	0
68	0.2	0.1	0.6	0.005	100	100	0	8	0	8	0	2.44666	0.8	3.2467	6.759	Opt	21	0
69	0.2	0.1	0.6	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	8.362	Opt	72	0
70	0.2	0.1	0.6	0.01	50	100	0	8	0	8	0	4.89332	0.8	5.6933	10.556	Opt	83	0
71	0.2	0.1	0.6	0.01	100	0	50	0	50	0	10	0	5	15	0.23	Opt	1	0
72	0.2	0.1	0.6	0.01	100	100	0	8	0	8	0	4.89332	0.8	5.6933	7.561	Opt	118	0
73	0.2	0.1	0.8	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	6.459	Opt	37	0
74	0.2	0.1	0.8	0.005	50	100	0	8	0	8	0	2.44666	0.8	3.2467	7.12	Opt	25	0
75	0.2	0.1	0.8	0.005	100	0	50	0	50	0	10	0	5	15	0.231	Opt	1	0
76	0.2	0.1	0.8	0.005	100	100	0	8	0	8	0	2.44666	0.8	3.2467	9.023	Opt	51	0
77	0.2	0.1	0.8	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	8.782	Opt	63	0
78	0.2	0.1	0.8	0.01	50	100	0	8	0	8	0	4.89332	0.8	5.6933	17.235	Opt	149	0
79	0.2	0.1	0.8	0.01	100	0	50	0	50	0	10	0	5	15	0.241	Opt	1	0
80	0.2	0.1	0.8	0.01	100	100	0	8	0	8	0	4.89332	0.8	5.6933	7.26	Opt	20	0
81	0.2	0.2	0.6	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	5.608	Opt	26	0
82	0.2	0.2	0.6	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	12.178	Opt	241	0
83	0.2	0.2	0.6	0.005	100	0	50	0	50	0	10	0	10	20	0.24	Opt	1	0
84	0.2	0.2	0.6	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	5.448	Opt	19	0
85	0.2	0.2	0.6	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	8.122	Opt	36	0
86	0.2	0.2	0.6	0.01	50	100	0	8	0	8	0	4.89332	1.6	6.4933	6.309	Opt	28	0
87	0.2	0.2	0.6	0.01	100	0	50	0	50	0	10	0	10	20	0.25	Opt	1	0
88	0.2	0.2	0.6	0.01	100	100	0	8	0	8	0	4.89332	1.6	6.4933	10.716	Opt	77	0
89	0.2	0.2	0.8	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	7.651	Opt	51	0
90	0.2	0.2	0.8	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	8.472	Opt	40	0
91	0.2	0.2	0.8	0.005	100	0	50	0	50	0	10	0	10	20	0.24	Opt	1	0
92	0.2	0.2	0.8	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	9.374	Opt	43	0
93	0.2	0.2	0.8	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	9.644	Opt	75	0
94	0.2	0.2	0.8	0.01	50	100	0	8	0	8	0	4.89332	1.6	6.4933	6.068	Opt	33	0
95	0.2	0.2	0.8	0.01	100	0	50	0	50	0	10	0	10	20	0.251	Opt	1	0
96	0.2	0.2	0.8	0.01	100	100	0	8	0	8	0	4.89332	1.6	6.4933	4.386	Opt	1	0

Exp	INPUT						OUTPUT											
	$f_r$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
97	0.4	0	0.6	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	7.861	Opt	45	0
98	0.4	0	0.6	0.005	50	100	0	10	0	50	0	2.41733	0	2.4173	6.46	Opt	13	0
99	0.4	0	0.6	0.005	100	0	50	0	50	0	20	0	0	20	0.26	Opt	1	0
100	0.4	0	0.6	0.005	100	100	0	10	0	50	0	2.41733	0	2.4173	10.525	Opt	312	0
101	0.4	0	0.6	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	9.464	Opt	102	0
102	0.4	0	0.6	0.01	50	100	0	10	0	50	0	4.83466	0	4.8347	7.951	Opt	30	0
103	0.4	0	0.6	0.01	100	0	50	0	50	0	20	0	0	20	0.251	Opt	1	0
104	0.4	0	0.6	0.01	100	100	0	10	0	50	0	4.83466	0	4.8347	8.061	Opt	38	0
105	0.4	0	0.8	0.005	0	100	0	10	0	50	0	2.41733	0	2.4173	9.063	Opt	156	0
106	0.4	0	0.8	0.005	50	100	0	10	0	50	0	2.41733	0	2.4173	8.883	Opt	174	0
107	0.4	0	0.8	0.005	100	0	50	0	50	0	20	0	0	20	0.261	Opt	1	0
108	0.4	0	0.8	0.005	100	100	0	10	0	50	0	2.41733	0	2.4173	9.874	Opt	59	0
109	0.4	0	0.8	0.01	0	100	0	10	0	50	0	4.83466	0	4.8347	9.453	Opt	154	0
110	0.4	0	0.8	0.01	50	100	0	10	0	50	0	4.83466	0	4.8347	32.337	Opt	841	0
111	0.4	0	0.8	0.01	100	0	50	0	50	0	20	0	0	20	0.26	Opt	1	0
112	0.4	0	0.8	0.01	100	100	0	10	0	50	0	4.83466	0	4.8347	8.863	Opt	53	0
113	0.4	0.1	0.6	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	8.572	Opt	128	0
114	0.4	0.1	0.6	0.005	50	100	0	8	0	8	0	2.44666	0.8	3.2467	6.159	Opt	21	0
115	0.4	0.1	0.6	0.005	100	0	50	0	50	0	20	0	5	25	0.271	Opt	1	0
116	0.4	0.1	0.6	0.005	100	100	0	8	0	8	0	2.44666	0.8	3.2467	6.97	Opt	21	0
117	0.4	0.1	0.6	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	8.712	Opt	72	0
118	0.4	0.1	0.6	0.01	50	100	0	8	0	8	0	4.89332	0.8	5.6933	11.026	Opt	83	0
119	0.4	0.1	0.6	0.01	100	0	50	0	50	0	20	0	5	25	0.271	Opt	1	0
120	0.4	0.1	0.6	0.01	100	100	0	8	0	8	0	4.89332	0.8	5.6933	7.991	Opt	40	0
121	0.4	0.1	0.8	0.005	0	100	0	8	0	8	0	2.44666	0.8	3.2467	6.59	Opt	37	0
122	0.4	0.1	0.8	0.005	50	100	0	8	0	8	0	2.44666	0.8	3.2467	7.28	Opt	25	0
123	0.4	0.1	0.8	0.005	100	0	50	0	50	0	20	0	5	25	0.27	Opt	1	0
124	0.4	0.1	0.8	0.005	100	100	0	8	0	8	0	2.44666	0.8	3.2467	9.374	Opt	51	0
125	0.4	0.1	0.8	0.01	0	100	0	8	0	8	0	4.89332	0.8	5.6933	9.033	Opt	63	0
126	0.4	0.1	0.8	0.01	50	100	0	8	0	8	0	4.89332	0.8	5.6933	17.055	Opt	141	0
127	0.4	0.1	0.8	0.01	100	0	50	0	50	0	20	0	5	25	0.28	Opt	1	0
128	0.4	0.1	0.8	0.01	100	100	0	8	0	8	0	4.89332	0.8	5.6933	12.898	Opt	103	0
129	0.4	0.2	0.6	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	5.789	Opt	26	0
130	0.4	0.2	0.6	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	15.132	Opt	324	0
131	0.4	0.2	0.6	0.005	100	0	50	0	50	0	20	0	10	30	0.29	Opt	1	0
132	0.4	0.2	0.6	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	5.668	Opt	19	0
133	0.4	0.2	0.6	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	8.372	Opt	36	0
134	0.4	0.2	0.6	0.01	50	100	0	8	0	8	0	4.89332	1.6	6.4933	6.63	Opt	28	0
135	0.4	0.2	0.6	0.01	100	0	50	0	50	0	20	0	10	30	0.3	Opt	1	0
136	0.4	0.2	0.6	0.01	100	100	0	8	0	8	0	4.89332	1.6	6.4933	8.683	Opt	91	0
137	0.4	0.2	0.8	0.005	0	100	0	6	0	6	0	2.70759	1.2	3.9076	7.971	Opt	51	0
138	0.4	0.2	0.8	0.005	50	100	0	6	0	6	0	2.70759	1.2	3.9076	8.763	Opt	40	0
139	0.4	0.2	0.8	0.005	100	0	50	0	50	0	20	0	10	30	0.28	Opt	1	0
140	0.4	0.2	0.8	0.005	100	100	0	6	0	6	0	2.70759	1.2	3.9076	9.604	Opt	43	0
141	0.4	0.2	0.8	0.01	0	100	0	8	0	8	0	4.89332	1.6	6.4933	9.984	Opt	75	0
142	0.4	0.2	0.8	0.01	50	100	0	8	0	8	0	4.89332	1.6	6.4933	7.951	Opt	39	0
143	0.4	0.2	0.8	0.01	100	0	50	0	50	0	20	0	10	30	0.29	Opt	1	0
144	0.4	0.2	0.8	0.01	100	100	0	8	0	8	0	4.89332	1.6	6.4933	8.072	Opt	41	0

## Appendix D – DOE Results for System-Wide Service Level Scenario

Exp	INPUT						OUTPUT											
	$f_i$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd					Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
	#	ded	#	shd	s	ded	s	shd										
1	0	0	0.6	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	9.624	Opt	125	0
2	0	0	0.6	0.005	50	100	25	9	25	45	0	1.73119	0	1.7312	3.205	Opt	11	0
3	0	0	0.6	0.005	100	0	50	0	50	0	0	0	0	0	0.19	Opt	1	0
4	0	0	0.6	0.005	100	100	50	0	50	0	0	0	0	0	0.26	Opt	1	0
5	0	0	0.6	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	7.191	Opt	56	0
6	0	0	0.6	0.01	50	100	25	9	25	45	0	3.46237	0	3.4624	2.583	Opt	11	0
7	0	0	0.6	0.01	100	0	50	0	50	0	0	0	0	0	0.181	Opt	1	0
8	0	0	0.6	0.01	100	100	50	0	50	0	0	0	0	0	0.27	Opt	1	0
9	0	0	0.8	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	8.973	Opt	50	0
10	0	0	0.8	0.005	50	100	25	9	25	45	0	1.73119	0	1.7312	5.778	Opt	18	0
11	0	0	0.8	0.005	100	0	50	0	50	0	0	0	0	0	0.191	Opt	1	0
12	0	0	0.8	0.005	100	100	50	1	50	5	0	0	0	0	0.821	Opt	1	0
13	0	0	0.8	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	7.521	Opt	32	0
14	0	0	0.8	0.01	50	100	25	9	25	45	0	3.46237	0	3.4624	4.086	Opt	3	0
15	0	0	0.8	0.01	100	0	50	0	50	0	0	0	0	0	0.19	Opt	1	0
16	0	0	0.8	0.01	100	100	50	1	50	5	0	0	0	0	0.831	Opt	1	0
17	0	0.1	0.6	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	4.517	Opt	28	0
18	0	0.1	0.6	0.005	50	100	4	7	4	7	0	2.85746	1.1	3.9575	10.094	Opt	157	0
19	0	0.1	0.6	0.005	100	0	50	0	50	0	0	0	5	5	0.19	Opt	1	0
20	0	0.1	0.6	0.005	100	100	11	7	11	7	0	1.86172	1.8	3.6617	5.629	Opt	103	0
21	0	0.1	0.6	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	6.038	Opt	44	0
22	0	0.1	0.6	0.01	50	100	14	8	14	8	0	4.24476	2.2	6.4448	4.997	Opt	9	0
23	0	0.1	0.6	0.01	100	0	50	0	50	0	0	0	5	5	0.201	Opt	1	0
24	0	0.1	0.6	0.01	100	100	31	4	31	4	0	1.22778	3.5	4.7278	1.091	Opt	1	0
25	0	0.1	0.8	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	6.69	Opt	49	0
26	0	0.1	0.8	0.005	50	100	4	7	4	7	0	2.85746	1.1	3.9575	9.123	Opt	41	0
27	0	0.1	0.8	0.005	100	0	50	0	50	0	0	0	5	5	0.2	Opt	1	0
28	0	0.1	0.8	0.005	100	100	11	7	11	7	0	1.86172	1.8	3.6617	6.43	Opt	67	0
29	0	0.1	0.8	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	10.725	Opt	153	0
30	0	0.1	0.8	0.01	50	100	14	8	14	8	0	4.24476	2.2	6.4448	4.316	Opt	6	0
31	0	0.1	0.8	0.01	100	0	50	0	50	0	0	0	5	5	0.201	Opt	1	0
32	0	0.1	0.8	0.01	100	100	31	4	31	4	0	1.22778	3.5	4.7278	3.675	Opt	3	0
33	0	0.2	0.6	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	10.545	Opt	149	0
34	0	0.2	0.6	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	6.099	Opt	54	0
35	0	0.2	0.6	0.005	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
36	0	0.2	0.6	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	5.228	Opt	10	0
37	0	0.2	0.6	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	4.987	Opt	18	0
38	0	0.2	0.6	0.01	50	100	4	7	4	7	0	5.71491	2.2	7.9149	5.628	Opt	25	0
39	0	0.2	0.6	0.01	100	0	50	0	50	0	0	0	10	10	0.2	Opt	1	0
40	0	0.2	0.6	0.01	100	100	11	7	11	7	0	3.72344	3.6	7.3234	9.965	Opt	97	0
41	0	0.2	0.8	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	6.9	Opt	29	0
42	0	0.2	0.8	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	16.964	Opt	269	0
43	0	0.2	0.8	0.005	100	0	50	0	50	0	0	0	10	10	0.22	Opt	1	0
44	0	0.2	0.8	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	8.573	Opt	73	0
45	0	0.2	0.8	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	7.851	Opt	85	0
46	0	0.2	0.8	0.01	50	100	4	7	4	7	0	5.71491	2.2	7.9149	6.219	Opt	35	0
47	0	0.2	0.8	0.01	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
48	0	0.2	0.8	0.01	100	100	11	7	11	7	0	3.72344	3.6	7.3234	9.684	Opt	137	0

Exp	INPUT						OUTPUT											
	$f_r$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
49	0.2	0	0.6	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	10.245	Opt	125	0
50	0.2	0	0.6	0.005	50	100	0	10	0	50	0	3.2748	0	3.2748	6.87	Opt	21	0
51	0.2	0	0.6	0.005	100	0	50	0	50	0	10	0	0	10	0.22	Opt	1	0
52	0.2	0	0.6	0.005	100	100	0	10	0	50	0	3.2748	0	3.2748	11.026	Opt	126	0
53	0.2	0	0.6	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	7.581	Opt	56	0
54	0.2	0	0.6	0.01	50	100	4	10	4	50	0.8	5.47648	0	6.2765	6.65	Opt	30	0
55	0.2	0	0.6	0.01	100	0	50	0	50	0	10	0	0	10	0.22	Opt	1	0
56	0.2	0	0.6	0.01	100	100	10	10	10	50	2	3.81669	0	5.8167	7.591	Opt	35	0
57	0.2	0	0.8	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	9.504	Opt	50	0
58	0.2	0	0.8	0.005	50	100	0	10	0	50	0	3.2748	0	3.2748	8.842	Opt	52	0
59	0.2	0	0.8	0.005	100	0	50	0	50	0	10	0	0	10	0.221	Opt	1	0
60	0.2	0	0.8	0.005	100	100	0	10	0	50	0	3.2748	0	3.2748	8.632	Opt	43	0
61	0.2	0	0.8	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	7.922	Opt	32	0
62	0.2	0	0.8	0.01	50	100	4	10	4	50	0.8	5.47648	0	6.2765	8.602	Opt	62	0
63	0.2	0	0.8	0.01	100	0	50	0	50	0	10	0	0	10	0.23	Opt	1	0
64	0.2	0	0.8	0.01	100	100	10	10	10	50	2	3.81669	0	5.8167	10.556	Opt	121	0
65	0.2	0.1	0.6	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	4.646	Opt	28	0
66	0.2	0.1	0.6	0.005	50	100	0	7	0	7	0	3.39806	0.7	4.0981	5.078	Opt	12	0
67	0.2	0.1	0.6	0.005	100	0	50	0	50	0	10	0	5	15	0.23	Opt	1	0
68	0.2	0.1	0.6	0.005	100	100	0	7	0	7	0	3.39806	0.7	4.0981	3.715	Opt	16	0
69	0.2	0.1	0.6	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	6.289	Opt	44	0
70	0.2	0.1	0.6	0.01	50	100	1	8	1	8	0.2	6.32973	0.9	7.4297	7.251	Opt	23	0
71	0.2	0.1	0.6	0.01	100	0	50	0	50	0	10	0	5	15	0.24	Opt	1	0
72	0.2	0.1	0.6	0.01	100	100	3	7	3	7	0.6	5.75431	1	7.3543	6.61	Opt	51	0
73	0.2	0.1	0.8	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	6.97	Opt	49	0
74	0.2	0.1	0.8	0.005	50	100	0	7	0	7	0	3.39806	0.7	4.0981	7.981	Opt	32	0
75	0.2	0.1	0.8	0.005	100	0	50	0	50	0	10	0	5	15	0.231	Opt	1	0
76	0.2	0.1	0.8	0.005	100	100	0	7	0	7	0	3.39806	0.7	4.0981	14.611	Opt	216	0
77	0.2	0.1	0.8	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	11.136	Opt	153	0
78	0.2	0.1	0.8	0.01	50	100	1	8	1	8	0.2	6.32973	0.9	7.4297	7.821	Opt	63	0
79	0.2	0.1	0.8	0.01	100	0	50	0	50	0	10	0	5	15	0.25	Opt	1	0
80	0.2	0.1	0.8	0.01	100	100	3	7	3	7	0.6	5.75431	1	7.3543	8.042	Opt	92	0
81	0.2	0.2	0.6	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	10.896	Opt	149	0
82	0.2	0.2	0.6	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	6.419	Opt	54	0
83	0.2	0.2	0.6	0.005	100	0	50	0	50	0	10	0	10	20	0.25	Opt	1	0
84	0.2	0.2	0.6	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	5.618	Opt	10	0
85	0.2	0.2	0.6	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	5.268	Opt	18	0
86	0.2	0.2	0.6	0.01	50	100	0	7	0	7	0	6.79612	1.4	8.1961	8.041	Opt	89	0
87	0.2	0.2	0.6	0.01	100	0	50	0	50	0	10	0	10	20	0.25	Opt	1	0
88	0.2	0.2	0.6	0.01	100	100	0	7	0	7	0	6.79612	1.4	8.1961	7.781	Opt	69	0
89	0.2	0.2	0.8	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	7.21	Opt	29	0
90	0.2	0.2	0.8	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	17.426	Opt	226	0
91	0.2	0.2	0.8	0.005	100	0	50	0	50	0	10	0	10	20	0.26	Opt	1	0
92	0.2	0.2	0.8	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	8.913	Opt	73	0
93	0.2	0.2	0.8	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	8.252	Opt	85	0
94	0.2	0.2	0.8	0.01	50	100	0	7	0	7	0	6.79612	1.4	8.1961	7.26	Opt	29	0
95	0.2	0.2	0.8	0.01	100	0	50	0	50	0	10	0	10	20	0.261	Opt	1	0
96	0.2	0.2	0.8	0.01	100	100	0	7	0	7	0	6.79612	1.4	8.1961	5.507	Opt	9	0

Exp	INPUT						OUTPUT											
	$f_r$	$h_i$	$\alpha_r$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
97	0.4	0	0.6	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	10.676	Opt	125	0
98	0.4	0	0.6	0.005	50	100	0	10	0	50	0	3.2748	0	3.2748	7.09	Opt	34	0
99	0.4	0	0.6	0.005	100	0	50	0	50	0	20	0	0	20	0.25	Opt	1	0
100	0.4	0	0.6	0.005	100	100	0	10	0	50	0	3.2748	0	3.2748	11.337	Opt	126	0
101	0.4	0	0.6	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	7.871	Opt	56	0
102	0.4	0	0.6	0.01	50	100	0	10	0	50	0	6.54961	0	6.5496	8.162	Opt	61	0
103	0.4	0	0.6	0.01	100	0	50	0	50	0	20	0	0	20	0.26	Opt	1	0
104	0.4	0	0.6	0.01	100	100	0	10	0	50	0	6.54961	0	6.5496	8.292	Opt	45	0
105	0.4	0	0.8	0.005	0	100	0	10	0	50	0	3.2748	0	3.2748	9.644	Opt	50	0
106	0.4	0	0.8	0.005	50	100	0	10	0	50	0	3.2748	0	3.2748	9.003	Opt	52	0
107	0.4	0	0.8	0.005	100	0	50	0	50	0	20	0	0	20	0.27	Opt	1	0
108	0.4	0	0.8	0.005	100	100	0	10	0	50	0	3.2748	0	3.2748	10.546	Opt	232	0
109	0.4	0	0.8	0.01	0	100	0	10	0	50	0	6.54961	0	6.5496	8.101	Opt	32	0
110	0.4	0	0.8	0.01	50	100	0	10	0	50	0	6.54961	0	6.5496	9.514	Opt	51	0
111	0.4	0	0.8	0.01	100	0	50	0	50	0	20	0	0	20	0.28	Opt	1	0
112	0.4	0	0.8	0.01	100	100	0	10	0	50	0	6.54961	0	6.5496	9.354	Opt	49	0
113	0.4	0.1	0.6	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	4.917	Opt	28	0
114	0.4	0.1	0.6	0.005	50	100	0	7	0	7	0	3.39806	0.7	4.0981	5.318	Opt	12	0
115	0.4	0.1	0.6	0.005	100	0	50	0	50	0	20	0	5	25	0.26	Opt	1	0
116	0.4	0.1	0.6	0.005	100	100	0	7	0	7	0	3.39806	0.7	4.0981	3.976	Opt	16	0
117	0.4	0.1	0.6	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	6.509	Opt	44	0
118	0.4	0.1	0.6	0.01	50	100	0	8	0	8	0	6.64784	0.8	7.4478	8.492	Opt	110	0
119	0.4	0.1	0.6	0.01	100	0	50	0	50	0	20	0	5	25	0.271	Opt	1	0
120	0.4	0.1	0.6	0.01	100	100	0	8	0	8	0	6.64784	0.8	7.4478	10.745	Opt	129	0
121	0.4	0.1	0.8	0.005	0	100	0	7	0	7	0	3.39806	0.7	4.0981	7.231	Opt	49	0
122	0.4	0.1	0.8	0.005	50	100	0	7	0	7	0	3.39806	0.7	4.0981	8.292	Opt	32	0
123	0.4	0.1	0.8	0.005	100	0	50	0	50	0	20	0	5	25	0.29	Opt	1	0
124	0.4	0.1	0.8	0.005	100	100	0	7	0	7	0	3.39806	0.7	4.0981	13.94	Opt	195	0
125	0.4	0.1	0.8	0.01	0	100	0	8	0	8	0	6.64784	0.8	7.4478	11.447	Opt	153	0
126	0.4	0.1	0.8	0.01	50	100	0	8	0	8	0	6.64784	0.8	7.4478	5.988	Opt	15	0
127	0.4	0.1	0.8	0.01	100	0	50	0	50	0	20	0	5	25	0.271	Opt	1	0
128	0.4	0.1	0.8	0.01	100	100	0	8	0	8	0	6.64784	0.8	7.4478	8.322	Opt	103	0
129	0.4	0.2	0.6	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	11.216	Opt	149	0
130	0.4	0.2	0.6	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	6.629	Opt	54	0
131	0.4	0.2	0.6	0.005	100	0	50	0	50	0	20	0	10	30	0.271	Opt	1	0
132	0.4	0.2	0.6	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	5.788	Opt	10	0
133	0.4	0.2	0.6	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	5.498	Opt	18	0
134	0.4	0.2	0.6	0.01	50	100	0	7	0	7	0	6.79612	1.4	8.1961	9.063	Opt	58	0
135	0.4	0.2	0.6	0.01	100	0	50	0	50	0	20	0	10	30	0.28	Opt	1	0
136	0.4	0.2	0.6	0.01	100	100	0	7	0	7	0	6.79612	1.4	8.1961	6.8	Opt	33	0
137	0.4	0.2	0.8	0.005	0	100	0	7	0	7	0	3.39806	1.4	4.7981	7.441	Opt	29	0
138	0.4	0.2	0.8	0.005	50	100	0	7	0	7	0	3.39806	1.4	4.7981	17.876	Opt	226	0
139	0.4	0.2	0.8	0.005	100	0	50	0	50	0	20	0	10	30	0.29	Opt	1	0
140	0.4	0.2	0.8	0.005	100	100	0	7	0	7	0	3.39806	1.4	4.7981	9.133	Opt	73	0
141	0.4	0.2	0.8	0.01	0	100	0	7	0	7	0	6.79612	1.4	8.1961	8.412	Opt	85	0
142	0.4	0.2	0.8	0.01	50	100	0	7	0	7	0	6.79612	1.4	8.1961	7.541	Opt	29	0
143	0.4	0.2	0.8	0.01	100	0	50	0	50	0	20	0	10	30	0.291	Opt	1	0
144	0.4	0.2	0.8	0.01	100	100	0	7	0	7	0	6.79612	1.4	8.1961	7	Opt	18	0

## Appendix E – DOE Results for Customer-Centric Service Level Scenario

Exp	INPUT						OUTPUT											
	$f_i$	$h_i$	$\alpha_j$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
1	0	0	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.1	Inf	0	0
2	0	0	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.1	Inf	0	0
3	0	0	0.6	0.005	100	0	50	0	50	0	0	0	0	0	0.19	Opt	1	0
4	0	0	0.6	0.005	100	100	50	0	50	0	0	0	0	0	0.251	Opt	1	0
5	0	0	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.1	Inf	1	0
6	0	0	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.11	Inf	1	0
7	0	0	0.6	0.01	100	0	50	0	50	0	0	0	0	0	0.17	Opt	1	0
8	0	0	0.6	0.01	100	100	50	0	50	0	0	0	0	0	0.251	Opt	1	0
9	0	0	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.11	Inf	1	0
10	0	0	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.12	Inf	1	0
11	0	0	0.8	0.005	100	0	50	0	50	0	0	0	0	0	0.221	Opt	1	0
12	0	0	0.8	0.005	100	100	50	0	50	0	0	0	0	0	0.28	Opt	1	0
13	0	0	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.13	Inf	1	0
14	0	0	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.11	Inf	1	0
15	0	0	0.8	0.01	100	0	50	0	50	0	0	0	0	0	0.201	Opt	1	0
16	0	0	0.8	0.01	100	100	50	0	50	0	0	0	0	0	0.27	Opt	1	0
17	0	0.1	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.12	Inf	1	0
18	0	0.1	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.11	Inf	1	0
19	0	0.1	0.6	0.005	100	0	50	0	50	0	0	0	5	5	0.201	Opt	1	0
20	0	0.1	0.6	0.005	100	100	11	7	11	7	0	1.86172	1.8	3.6617	3.825	Opt	7	0
21	0	0.1	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.11	Inf	7	0
22	0	0.1	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.121	Inf	7	0
23	0	0.1	0.6	0.01	100	0	50	0	50	0	0	0	5	5	0.2	Opt	1	0
24	0	0.1	0.6	0.01	100	100	31	4	31	4	0	1.22778	3.5	4.7278	2.834	Opt	3	0
25	0	0.1	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.13	Inf	3	0
26	0	0.1	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.12	Inf	3	0
27	0	0.1	0.8	0.005	100	0	50	0	50	0	0	0	5	5	0.271	Opt	1	0
28	0	0.1	0.8	0.005	100	100	11	7	11	7	0	1.86172	1.8	3.6617	1.893	Opt	1	0
29	0	0.1	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.12	Inf	1	0
30	0	0.1	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.13	Inf	1	0
31	0	0.1	0.8	0.01	100	0	50	0	50	0	0	0	5	5	0.24	Opt	1	0
32	0	0.1	0.8	0.01	100	100	31	4	31	4	0	1.22778	3.5	4.7278	2.093	Opt	1	0
33	0	0.2	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.131	Inf	1	0
34	0	0.2	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.13	Inf	1	0
35	0	0.2	0.6	0.005	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
36	0	0.2	0.6	0.005	100	100	3	7	3	7	0	2.87716	2	4.8772	4.937	Opt	28	0
37	0	0.2	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.13	Inf	28	0
38	0	0.2	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.121	Inf	28	0
39	0	0.2	0.6	0.01	100	0	50	0	50	0	0	0	10	10	0.22	Opt	1	0
40	0	0.2	0.6	0.01	100	100	11	7	11	7	0	3.72344	3.6	7.3234	4.346	Opt	20	0
41	0	0.2	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.13	Inf	20	0
42	0	0.2	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.141	Inf	20	0
43	0	0.2	0.8	0.005	100	0	50	0	50	0	0	0	10	10	0.21	Opt	1	0
44	0	0.2	0.8	0.005	100	100	3	7	3	7	0	2.87716	2	4.8772	6.579	Opt	58	0
45	0	0.2	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.141	Inf	58	0
46	0	0.2	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.14	Inf	58	0
47	0	0.2	0.8	0.01	100	0	50	0	50	0	0	0	10	10	0.22	Opt	1	0
48	0	0.2	0.8	0.01	100	100	11	7	11	7	0	3.72344	3.6	7.3234	6.66	Opt	59	0



Exp	INPUT						OUTPUT											
	$f_i$	$h_i$	$\alpha_j$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
49	0.2	0	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.14	Inf	59	0
50	0.2	0	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.15	Inf	59	0
51	0.2	0	0.6	0.005	100	0	50	0	50	0	10	0	0	10	0.221	Opt	1	0
52	0.2	0	0.6	0.005	100	100	2	10	2	50	0.4	2.95059	0	3.3506	6.359	Opt	49	0
53	0.2	0	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.14	Inf	49	0
54	0.2	0	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.14	Inf	49	0
55	0.2	0	0.6	0.01	100	0	50	0	50	0	10	0	0	10	0.23	Opt	1	0
56	0.2	0	0.6	0.01	100	100	10	10	10	50	2	3.81669	0	5.8167	6.709	Opt	59	0
57	0.2	0	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.14	Inf	59	0
58	0.2	0	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.151	Inf	59	0
59	0.2	0	0.8	0.005	100	0	50	0	50	0	10	0	0	10	0.23	Opt	1	0
60	0.2	0	0.8	0.005	100	100	2	10	2	50	0.4	2.95059	0	3.3506	8.092	Opt	144	0
61	0.2	0	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.14	Inf	144	0
62	0.2	0	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.15	Inf	144	0
63	0.2	0	0.8	0.01	100	0	50	0	50	0	10	0	0	10	0.24	Opt	1	0
64	0.2	0	0.8	0.01	100	100	10	10	10	50	2	3.81669	0	5.8167	9.204	Opt	155	0
65	0.2	0.1	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.15	Inf	155	0
66	0.2	0.1	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.15	Inf	155	0
67	0.2	0.1	0.6	0.005	100	0	50	0	50	0	10	0	5	15	0.231	Opt	1	0
68	0.2	0.1	0.6	0.005	100	100	2	7	2	7	0.4	3.07855	0.9	4.3786	6.96	Opt	48	0
69	0.2	0.1	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.15	Inf	48	0
70	0.2	0.1	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.15	Inf	48	0
71	0.2	0.1	0.6	0.01	100	0	50	0	50	0	10	0	5	15	0.24	Opt	1	0
72	0.2	0.1	0.6	0.01	100	100	3	7	3	7	0.6	5.75431	1	7.3543	3.956	Opt	3	0
73	0.2	0.1	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.16	Inf	3	0
74	0.2	0.1	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.161	Inf	3	0
75	0.2	0.1	0.8	0.005	100	0	50	0	50	0	10	0	5	15	0.24	Opt	1	0
76	0.2	0.1	0.8	0.005	100	100	2	7	2	7	0.4	3.07855	0.9	4.3786	5.688	Opt	33	0
77	0.2	0.1	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.16	Inf	33	0
78	0.2	0.1	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.161	Inf	33	0
79	0.2	0.1	0.8	0.01	100	0	50	0	50	0	10	0	5	15	0.24	Opt	1	0
80	0.2	0.1	0.8	0.01	100	100	3	7	3	7	0.6	5.75431	1	7.3543	5.478	Opt	44	0
81	0.2	0.2	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.16	Inf	44	0
82	0.2	0.2	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.16	Inf	44	0
83	0.2	0.2	0.6	0.005	100	0	50	0	50	0	10	0	10	20	0.241	Opt	1	0
84	0.2	0.2	0.6	0.005	100	100	2	7	2	7	0.4	3.07855	1.8	5.2786	4.606	Opt	23	0
85	0.2	0.2	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.161	Inf	23	0
86	0.2	0.2	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.16	Inf	23	0
87	0.2	0.2	0.6	0.01	100	0	50	0	50	0	10	0	10	20	0.25	Opt	1	0
88	0.2	0.2	0.6	0.01	100	100	3	7	3	7	0.6	5.75431	2	8.3543	4.947	Opt	12	0
89	0.2	0.2	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.161	Inf	12	0
90	0.2	0.2	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.16	Inf	12	0
91	0.2	0.2	0.8	0.005	100	0	50	0	50	0	10	0	10	20	0.27	Opt	1	0
92	0.2	0.2	0.8	0.005	100	100	2	7	2	7	0.4	3.07855	1.8	5.2786	7.621	Opt	60	0
93	0.2	0.2	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.171	Inf	60	0
94	0.2	0.2	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.17	Inf	60	0
95	0.2	0.2	0.8	0.01	100	0	50	0	50	0	10	0	10	20	0.25	Opt	1	0
96	0.2	0.2	0.8	0.01	100	100	3	7	3	7	0.6	5.75431	2	8.3543	4.276	Opt	32	0

Exp	INPUT						OUTPUT											
	$f_i$	$h_i$	$\alpha_j$	$d_j$	% ded	% shd	# ded	# shd	s ded	s shd	Fixed Cost	Transp Cost	Inv Cost	Obj Val	Sol Time	Status	B&B nodes	Opt Gap
97	0.4	0	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.171	Inf	32	0
98	0.4	0	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.18	Inf	32	0
99	0.4	0	0.6	0.005	100	0	50	0	50	0	20	0	0	20	0.26	Opt	1	0
100	0.4	0	0.6	0.005	100	100	2	10	2	50	0.8	2.95059	0	3.7506	6.7	Opt	49	0
101	0.4	0	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.17	Inf	49	0
102	0.4	0	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.16	Inf	49	0
103	0.4	0	0.6	0.01	100	0	50	0	50	0	20	0	0	20	0.251	Opt	1	0
104	0.4	0	0.6	0.01	100	100	2	10	2	50	0.8	5.90119	0	6.7012	7	Opt	51	0
105	0.4	0	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.17	Inf	51	0
106	0.4	0	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.17	Inf	51	0
107	0.4	0	0.8	0.005	100	0	50	0	50	0	20	0	0	20	0.261	Opt	1	0
108	0.4	0	0.8	0.005	100	100	2	10	2	50	0.8	2.95059	0	3.7506	8.432	Opt	132	0
109	0.4	0	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.18	Inf	132	0
110	0.4	0	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.181	Inf	132	0
111	0.4	0	0.8	0.01	100	0	50	0	50	0	20	0	0	20	0.26	Opt	1	0
112	0.4	0	0.8	0.01	100	100	2	10	2	50	0.8	5.90119	0	6.7012	7.881	Opt	71	0
113	0.4	0.1	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.171	Inf	71	0
114	0.4	0.1	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.17	Inf	71	0
115	0.4	0.1	0.6	0.005	100	0	50	0	50	0	20	0	5	25	0.28	Opt	1	0
116	0.4	0.1	0.6	0.005	100	100	2	7	2	7	0.8	3.07855	0.9	4.7786	7.461	Opt	52	0
117	0.4	0.1	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.18	Inf	52	0
118	0.4	0.1	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.191	Inf	52	0
119	0.4	0.1	0.6	0.01	100	0	50	0	50	0	20	0	5	25	0.27	Opt	1	0
120	0.4	0.1	0.6	0.01	100	100	2	8	2	8	0.8	5.99942	1	7.7994	4.847	Opt	21	0
121	0.4	0.1	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.19	Inf	21	0
122	0.4	0.1	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.191	Inf	21	0
123	0.4	0.1	0.8	0.005	100	0	50	0	50	0	20	0	5	25	0.27	Opt	1	0
124	0.4	0.1	0.8	0.005	100	100	2	7	2	7	0.8	3.07855	0.9	4.7786	6.71	Opt	41	0
125	0.4	0.1	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.19	Inf	41	0
126	0.4	0.1	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.19	Inf	41	0
127	0.4	0.1	0.8	0.01	100	0	50	0	50	0	20	0	5	25	0.281	Opt	1	0
128	0.4	0.1	0.8	0.01	100	100	2	8	2	8	0.8	5.99942	1	7.7994	5.357	Opt	42	0
129	0.4	0.2	0.6	0.005	0	100	0	0	0	0	0	0	0	0	0.191	Inf	42	0
130	0.4	0.2	0.6	0.005	50	100	0	0	0	0	0	0	0	0	0.19	Inf	42	0
131	0.4	0.2	0.6	0.005	100	0	50	0	50	0	20	0	10	30	0.29	Opt	1	0
132	0.4	0.2	0.6	0.005	100	100	2	7	2	7	0.8	3.07855	1.8	5.6786	4.707	Opt	23	0
133	0.4	0.2	0.6	0.01	0	100	0	0	0	0	0	0	0	0	0.2	Inf	23	0
134	0.4	0.2	0.6	0.01	50	100	0	0	0	0	0	0	0	0	0.201	Inf	23	0
135	0.4	0.2	0.6	0.01	100	0	50	0	50	0	20	0	10	30	0.28	Opt	1	0
136	0.4	0.2	0.6	0.01	100	100	2	7	2	7	0.8	6.15709	1.8	8.7571	5.568	Opt	26	0
137	0.4	0.2	0.8	0.005	0	100	0	0	0	0	0	0	0	0	0.191	Inf	26	0
138	0.4	0.2	0.8	0.005	50	100	0	0	0	0	0	0	0	0	0.2	Inf	26	0
139	0.4	0.2	0.8	0.005	100	0	50	0	50	0	20	0	10	30	0.28	Opt	1	0
140	0.4	0.2	0.8	0.005	100	100	2	7	2	7	0.8	3.07855	1.8	5.6786	7.892	Opt	60	0
141	0.4	0.2	0.8	0.01	0	100	0	0	0	0	0	0	0	0	0.19	Inf	60	0
142	0.4	0.2	0.8	0.01	50	100	0	0	0	0	0	0	0	0	0.2	Inf	60	0
143	0.4	0.2	0.8	0.01	100	0	50	0	50	0	20	0	10	30	0.291	Opt	1	0
144	0.4	0.2	0.8	0.01	100	100	2	7	2	7	0.8	6.15709	1.8	8.7571	6.479	Opt	33	0

## Appendix F – Risk Pooling DOE

<i>n</i>	$\alpha$	<i>d</i>	<i>LB</i>	<i>UB</i>	<i>Gap</i>	<i>n</i>	$\alpha$	<i>d</i>	<i>LB</i>	<i>UB</i>	<i>Gap</i>
100	0.75	0.001	1.0135	1.014	0	100	0.95	0.001	1.0149	1.038	0.0235
100	0.75	0.002	1.0135	1.014	0	100	0.95	0.002	1.0215	1.022	0
100	0.75	0.003	1.0135	1.014	0	100	0.95	0.003	1.0215	1.022	0
100	0.75	0.004	1.0152	1.143	0.1277	100	0.95	0.004	1.0222	1.5	0.4778
100	0.75	0.005	1.0172	1.067	0.0494	100	0.95	0.005	1.026	1.067	0.0407
100	0.75	0.006	1.0192	1.048	0.0284	100	0.95	0.006	1.0294	1.042	0.0123
100	0.75	0.007	1.0213	1.038	0.0172	100	0.95	0.007	1.0326	1.033	0
100	0.75	0.008	1.0233	1.033	0.0101	100	0.95	0.008	1.0326	1.033	0
100	0.75	0.009	1.025	1.03	0.0053	100	0.95	0.009	1.033	1.051	0.0183
100	0.75	0.01	1.0263	1.029	0.0023	100	0.95	0.01	1.0353	1.167	0.1314
100	0.8	0.001	1.0127	1.013	0	100	0.96	0.001	1.0167	1.029	0.0127
100	0.8	0.002	1.0127	1.013	0	100	0.96	0.002	1.0213	1.021	0
100	0.8	0.003	1.0141	1.143	0.1288	100	0.96	0.003	1.0213	1.021	0
100	0.8	0.004	1.0167	1.056	0.0389	100	0.96	0.004	1.0241	1.1	0.0759
100	0.8	0.005	1.0189	1.04	0.0211	100	0.96	0.005	1.0282	1.045	0.0173
100	0.8	0.006	1.0213	1.032	0.011	100	0.96	0.006	1.0317	1.033	0.0016
100	0.8	0.007	1.0233	1.029	0.0053	100	0.96	0.007	1.0323	1.032	0
100	0.8	0.008	1.0256	1.026	0	100	0.96	0.008	1.0323	1.032	0
100	0.8	0.009	1.0256	1.026	0	100	0.96	0.009	1.0349	1.167	0.1318
100	0.8	0.01	1.0256	1.026	0	100	0.96	0.01	1.038	1.077	0.0389
100	0.85	0.001	1.0119	1.012	0	100	0.97	0.001	1.0192	1.023	0.004
100	0.85	0.002	1.0128	1.2	0.1872	100	0.97	0.002	1.0211	1.021	0
100	0.85	0.003	1.0161	1.048	0.0315	100	0.97	0.003	1.022	1.333	0.3114
100	0.85	0.004	1.0189	1.033	0.0145	100	0.97	0.004	1.0267	1.053	0.026
100	0.85	0.005	1.0217	1.027	0.0053	100	0.97	0.005	1.0313	1.033	0.0021
100	0.85	0.006	1.0238	1.024	0.0006	100	0.97	0.006	1.0319	1.032	0
100	0.85	0.007	1.0241	1.024	0	100	0.97	0.007	1.0319	1.032	0
100	0.85	0.008	1.0244	1.043	0.0182	100	0.97	0.008	1.0349	1.143	0.108
100	0.85	0.009	1.0263	1.167	0.1404	100	0.97	0.009	1.038	1.071	0.0335
100	0.85	0.01	1.0286	1.083	0.0548	100	0.97	0.01	1.0411	1.05	0.0089
100	0.9	0.001	1.0112	1.011	0	100	0.98	0.001	1.0208	1.021	0
100	0.9	0.002	1.0156	1.042	0.026	100	0.98	0.002	1.0208	1.021	0
100	0.9	0.003	1.0196	1.027	0.0074	100	0.98	0.003	1.0256	1.059	0.0332
100	0.9	0.004	1.0227	1.023	0	100	0.98	0.004	1.0308	1.033	0.0026
100	0.9	0.005	1.0227	1.023	0	100	0.98	0.005	1.0316	1.032	0
100	0.9	0.006	1.023	1.038	0.0155	100	0.98	0.006	1.0316	1.032	0
100	0.9	0.007	1.0256	1.111	0.0855	100	0.98	0.007	1.0357	1.1	0.0643
100	0.9	0.008	1.0278	1.067	0.0389	100	0.98	0.008	1.0395	1.056	0.0161
100	0.9	0.009	1.0303	1.048	0.0173	100	0.98	0.009	1.0426	1.043	0
100	0.9	0.01	1.0328	1.038	0.0057	100	0.98	0.01	1.0426	1.043	0
100	0.94	0.001	1.0137	1.053	0.0389	100	0.99	0.001	1.0206	1.021	0
100	0.94	0.002	1.02	1.024	0.0038	100	0.99	0.002	1.025	1.063	0.0375
100	0.94	0.003	1.0217	1.022	0	100	0.99	0.003	1.0313	1.031	0
100	0.94	0.004	1.0217	1.022	0	100	0.99	0.004	1.0313	1.031	0
100	0.94	0.005	1.0244	1.111	0.0867	100	0.99	0.005	1.0337	1.167	0.133
100	0.94	0.006	1.0274	1.056	0.0282	100	0.99	0.006	1.0385	1.059	0.0204
100	0.94	0.007	1.0308	1.038	0.0077	100	0.99	0.007	1.0421	1.042	0
100	0.94	0.008	1.033	1.033	0	100	0.99	0.008	1.0421	1.042	0
100	0.94	0.009	1.033	1.033	0	100	0.99	0.009	1.0435	1.5	0.4565
100	0.94	0.01	1.0337	2	0.9663	100	0.99	0.01	1.0476	1.1	0.0524

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
200	0.75	0.001	1.0067	1.007	0
200	0.75	0.002	1.0075	1.071	0.064
200	0.75	0.003	1.0095	1.023	0.0137
200	0.75	0.004	1.0114	1.017	0.0053
200	0.75	0.005	1.013	1.014	0.0011
200	0.75	0.006	1.0135	1.014	0
200	0.75	0.007	1.015	1.071	0.0564
200	0.75	0.008	1.0165	1.038	0.0219
200	0.75	0.009	1.018	1.028	0.0098
200	0.75	0.01	1.0194	1.023	0.0033
200	0.8	0.001	1.0063	1.006	0
200	0.8	0.002	1.0083	1.027	0.0188
200	0.8	0.003	1.0104	1.016	0.0057
200	0.8	0.004	1.0125	1.013	0.0003
200	0.8	0.005	1.0127	1.013	0
200	0.8	0.006	1.0144	1.056	0.0412
200	0.8	0.007	1.0161	1.03	0.0142
200	0.8	0.008	1.0177	1.023	0.005
200	0.8	0.009	1.0191	1.019	0
200	0.8	0.01	1.0197	1.25	0.2303
200	0.85	0.001	1.0064	1.091	0.0845
200	0.85	0.002	1.0093	1.016	0.007
200	0.85	0.003	1.0118	1.012	0.0003
200	0.85	0.004	1.012	1.021	0.0089
200	0.85	0.005	1.014	1.042	0.0277
200	0.85	0.006	1.0159	1.024	0.0085
200	0.85	0.007	1.0175	1.019	0.0013
200	0.85	0.008	1.018	1.018	0
200	0.85	0.009	1.0196	1.077	0.0573
200	0.85	0.01	1.0213	1.04	0.0187
200	0.9	0.001	1.0077	1.021	0.0131
200	0.9	0.002	1.0112	1.011	0
200	0.9	0.003	1.0113	1.019	0.0076
200	0.9	0.004	1.0137	1.032	0.0186
200	0.9	0.005	1.016	1.019	0.0032
200	0.9	0.006	1.0169	1.017	0
200	0.9	0.007	1.0183	1.083	0.065
200	0.9	0.008	1.0201	1.037	0.0169
200	0.9	0.009	1.0221	1.025	0.0029
200	0.9	0.01	1.0227	1.023	0
200	0.94	0.001	1.0098	1.012	0.0021
200	0.94	0.002	1.0108	1.011	0
200	0.94	0.003	1.0135	1.027	0.0135
200	0.94	0.004	1.0162	1.016	0
200	0.94	0.005	1.0165	1.5	0.4835
200	0.94	0.006	1.0189	1.04	0.0211
200	0.94	0.007	1.0211	1.024	0.0027
200	0.94	0.008	1.0217	1.022	0
200	0.94	0.009	1.0234	1.083	0.0599
200	0.94	0.01	1.0255	1.038	0.013

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
200	0.95	0.001	1.0106	1.011	0
200	0.95	0.002	1.011	1.2	0.189
200	0.95	0.003	1.0144	1.021	0.0064
200	0.95	0.004	1.016	1.016	0
200	0.95	0.005	1.0173	1.077	0.0596
200	0.95	0.006	1.0199	1.029	0.0087
200	0.95	0.007	1.0215	1.022	0
200	0.95	0.008	1.0223	1.167	0.1443
200	0.95	0.009	1.0245	1.045	0.0209
200	0.95	0.01	1.0267	1.029	0.0019
200	0.96	0.001	1.0105	1.011	0
200	0.96	0.002	1.0119	1.048	0.0357
200	0.96	0.003	1.0156	1.016	0.0008
200	0.96	0.004	1.0159	1.016	0
200	0.96	0.005	1.0185	1.038	0.0199
200	0.96	0.006	1.0211	1.022	0.0006
200	0.96	0.007	1.0214	1.033	0.0114
200	0.96	0.008	1.0237	1.056	0.0319
200	0.96	0.009	1.026	1.03	0.0043
200	0.96	0.01	1.0267	1.027	0
200	0.97	0.001	1.0104	1.01	0
200	0.97	0.002	1.0132	1.026	0.0125
200	0.97	0.003	1.0157	1.016	0
200	0.97	0.004	1.0171	1.067	0.0495
200	0.97	0.005	1.0201	1.024	0.0043
200	0.97	0.006	1.0211	1.021	0
200	0.97	0.007	1.023	1.067	0.0437
200	0.97	0.008	1.0255	1.031	0.0058
200	0.97	0.009	1.0265	1.026	0
200	0.97	0.01	1.0279	1.111	0.0832
200	0.98	0.001	1.0103	1.01	0
200	0.98	0.002	1.0152	1.016	0.0012
200	0.98	0.003	1.0155	1.016	0
200	0.98	0.004	1.0192	1.028	0.0085
200	0.98	0.005	1.0208	1.021	0
200	0.98	0.006	1.0225	1.077	0.0545
200	0.98	0.007	1.0253	1.03	0.005
200	0.98	0.008	1.0262	1.026	0
200	0.98	0.009	1.0281	1.083	0.0552
200	0.98	0.01	1.0305	1.038	0.008
200	0.99	0.001	1.0123	1.031	0.019
200	0.99	0.002	1.0154	1.015	0
200	0.99	0.003	1.0189	1.029	0.0097
200	0.99	0.004	1.0206	1.021	0
200	0.99	0.005	1.0231	1.05	0.0269
200	0.99	0.006	1.0259	1.026	0
200	0.99	0.007	1.0266	1.25	0.2234
200	0.99	0.008	1.0296	1.043	0.0139
200	0.99	0.009	1.0313	1.031	0
200	0.99	0.01	1.0326	1.143	0.1102

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
300	0.75	0.001	1.0045	1.004	0
300	0.75	0.002	1.0063	1.015	0.0091
300	0.75	0.003	1.0081	1.01	0.002
300	0.75	0.004	1.009	1.009	0
300	0.75	0.005	1.0104	1.033	0.0229
300	0.75	0.006	1.0119	1.019	0.0066
300	0.75	0.007	1.0133	1.014	0.0006
300	0.75	0.008	1.0142	1.111	0.097
300	0.75	0.009	1.0155	1.037	0.0216
300	0.75	0.01	1.0168	1.024	0.007
300	0.8	0.001	1.0047	1.043	0.0388
300	0.8	0.002	1.0069	1.011	0.0037
300	0.8	0.003	1.0084	1.008	0
300	0.8	0.004	1.0096	1.036	0.0261
300	0.8	0.005	1.0112	1.017	0.0061
300	0.8	0.006	1.0127	1.013	0
300	0.8	0.007	1.0135	1.071	0.0579
300	0.8	0.008	1.0149	1.029	0.0136
300	0.8	0.009	1.0164	1.019	0.0025
300	0.8	0.01	1.0172	1.333	0.3161
300	0.85	0.001	1.0053	1.016	0.0103
300	0.85	0.002	1.0078	1.008	0.0002
300	0.85	0.003	1.0086	1.05	0.0414
300	0.85	0.004	1.0105	1.016	0.0059
300	0.85	0.005	1.0119	1.012	0
300	0.85	0.006	1.013	1.05	0.037
300	0.85	0.007	1.0146	1.022	0.0077
300	0.85	0.008	1.0159	1.016	0
300	0.85	0.009	1.0169	1.071	0.0545
300	0.85	0.01	1.0184	1.03	0.0119
300	0.9	0.001	1.0064	1.009	0.0026
300	0.9	0.002	1.0075	2	0.9925
300	0.9	0.003	1.0099	1.016	0.0058
300	0.9	0.004	1.0112	1.011	0
300	0.9	0.005	1.0127	1.033	0.0206
300	0.9	0.006	1.0146	1.017	0.0021
300	0.9	0.007	1.0154	1.2	0.1846
300	0.9	0.008	1.017	1.033	0.0163
300	0.9	0.009	1.0187	1.02	0.0009
300	0.9	0.01	1.0195	1.125	0.1055
300	0.94	0.001	1.0071	1.007	0
300	0.94	0.002	1.009	1.018	0.0089
300	0.94	0.003	1.0108	1.011	0
300	0.94	0.004	1.0125	1.026	0.0138
300	0.94	0.005	1.0144	1.014	0
300	0.94	0.006	1.0155	1.053	0.0371
300	0.94	0.007	1.0175	1.021	0.0034
300	0.94	0.008	1.0183	1.333	0.315
300	0.94	0.009	1.0201	1.037	0.017
300	0.94	0.01	1.0217	1.022	0

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
300	0.95	0.001	1.0071	1.007	0
300	0.95	0.002	1.0096	1.014	0.0041
300	0.95	0.003	1.0107	1.017	0.0059
300	0.95	0.004	1.0132	1.019	0.0057
300	0.95	0.005	1.0142	1.014	0
300	0.95	0.006	1.0162	1.03	0.0141
300	0.95	0.007	1.0179	1.018	0
300	0.95	0.008	1.0191	1.059	0.0397
300	0.95	0.009	1.0209	1.025	0.0041
300	0.95	0.01	1.0218	1.333	0.3115
300	0.96	0.001	1.007	1.007	0
300	0.96	0.002	1.0103	1.011	0.0007
300	0.96	0.003	1.0114	1.05	0.0386
300	0.96	0.004	1.014	1.014	0.0003
300	0.96	0.005	1.0149	1.071	0.0566
300	0.96	0.006	1.0171	1.02	0.0033
300	0.96	0.007	1.018	1.25	0.232
300	0.96	0.008	1.02	1.031	0.0113
300	0.96	0.009	1.0213	1.021	0
300	0.96	0.01	1.0228	1.056	0.0327
300	0.97	0.001	1.0072	1.091	0.0837
300	0.97	0.002	1.0104	1.01	0
300	0.97	0.003	1.0123	1.023	0.0104
300	0.97	0.004	1.0139	1.014	0
300	0.97	0.005	1.016	1.028	0.0118
300	0.97	0.006	1.0175	1.017	0
300	0.97	0.007	1.0192	1.042	0.0225
300	0.97	0.008	1.0211	1.021	0
300	0.97	0.009	1.0221	1.077	0.0548
300	0.97	0.01	1.0242	1.028	0.0036
300	0.98	0.001	1.0083	1.02	0.0113
300	0.98	0.002	1.0103	1.01	0
300	0.98	0.003	1.0138	1.014	0
300	0.98	0.004	1.0149	1.05	0.0351
300	0.98	0.005	1.0173	1.017	0
300	0.98	0.006	1.0185	1.056	0.037
300	0.98	0.007	1.0208	1.021	0
300	0.98	0.008	1.0218	1.083	0.0615
300	0.98	0.009	1.024	1.027	0.003
300	0.98	0.01	1.0249	1.2	0.1751
300	0.99	0.001	1.0102	1.01	0
300	0.99	0.002	1.0125	1.019	0.0064
300	0.99	0.003	1.014	1.143	0.1288
300	0.99	0.004	1.0171	1.017	0
300	0.99	0.005	1.0186	1.045	0.0269
300	0.99	0.006	1.0206	1.021	0
300	0.99	0.007	1.0224	1.045	0.0231
300	0.99	0.008	1.0241	1.024	0
300	0.99	0.009	1.0258	1.056	0.0297
300	0.99	0.01	1.0277	1.028	0

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
400	0.75	0.001	1.0037	1.034	0.0308
400	0.75	0.002	1.0056	1.008	0.0027
400	0.75	0.003	1.0067	1.007	0
400	0.75	0.004	1.0082	1.019	0.0111
400	0.75	0.005	1.0096	1.011	0.0018
400	0.75	0.006	1.0106	1.083	0.0728
400	0.75	0.007	1.0119	1.023	0.0108
400	0.75	0.008	1.0132	1.015	0.0015
400	0.75	0.009	1.0142	1.077	0.0627
400	0.75	0.01	1.0154	1.028	0.0123
400	0.8	0.001	1.0041	1.014	0.0094
400	0.8	0.002	1.0062	1.006	0.0002
400	0.8	0.003	1.0071	1.027	0.0199
400	0.8	0.004	1.0087	1.011	0.0026
400	0.8	0.005	1.0097	1.125	0.1153
400	0.8	0.006	1.0112	1.021	0.0101
400	0.8	0.007	1.0126	1.013	0.0004
400	0.8	0.008	1.0136	1.05	0.0364
400	0.8	0.009	1.0149	1.022	0.0069
400	0.8	0.01	1.0159	1.016	0
400	0.85	0.001	1.0047	1.008	0.0035
400	0.85	0.002	1.006	2	0.994
400	0.85	0.003	1.0078	1.012	0.0044
400	0.85	0.004	1.0089	1.009	0
400	0.85	0.005	1.0105	1.02	0.0095
400	0.85	0.006	1.0119	1.012	0
400	0.85	0.007	1.013	1.036	0.0227
400	0.85	0.008	1.0144	1.017	0.0028
400	0.85	0.009	1.0154	1.1	0.0846
400	0.85	0.01	1.0168	1.027	0.0102
400	0.9	0.001	1.0056	1.006	0
400	0.9	0.002	1.0068	1.016	0.0091
400	0.9	0.003	1.0084	1.008	0
400	0.9	0.004	1.01	1.018	0.0082
400	0.9	0.005	1.0112	1.011	0
400	0.9	0.006	1.0127	1.024	0.0117
400	0.9	0.007	1.0141	1.014	0
400	0.9	0.008	1.0153	1.036	0.0204
400	0.9	0.009	1.0168	1.018	0.0007
400	0.9	0.01	1.0179	1.059	0.041
400	0.94	0.001	1.0053	1.005	0
400	0.94	0.002	1.008	1.008	0
400	0.94	0.003	1.0093	1.02	0.0107
400	0.94	0.004	1.0108	1.011	0
400	0.94	0.005	1.0125	1.019	0.0067
400	0.94	0.006	1.0137	1.25	0.2363
400	0.94	0.007	1.0154	1.022	0.0063
400	0.94	0.008	1.0165	1.2	0.1835
400	0.94	0.009	1.0182	1.026	0.0075
400	0.94	0.01	1.0192	1.25	0.2308

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
400	0.95	0.001	1.0055	1.091	0.0854
400	0.95	0.002	1.008	1.008	0
400	0.95	0.003	1.0098	1.014	0.0042
400	0.95	0.004	1.011	1.077	0.0659
400	0.95	0.005	1.0131	1.014	0.0012
400	0.95	0.006	1.0142	1.045	0.0313
400	0.95	0.007	1.016	1.016	0
400	0.95	0.008	1.0171	1.045	0.0284
400	0.95	0.009	1.0188	1.019	0
400	0.95	0.01	1.0199	1.05	0.0301
400	0.96	0.001	1.0059	1.023	0.0173
400	0.96	0.002	1.0079	1.008	0
400	0.96	0.003	1.0105	1.011	0.0003
400	0.96	0.004	1.0117	1.027	0.0153
400	0.96	0.005	1.0132	1.013	0
400	0.96	0.006	1.0149	1.023	0.0083
400	0.96	0.007	1.016	1.333	0.3173
400	0.96	0.008	1.0179	1.024	0.0059
400	0.96	0.009	1.019	1.143	0.1239
400	0.96	0.01	1.0207	1.026	0.0056
400	0.97	0.001	1.0065	1.013	0.0061
400	0.97	0.002	1.0085	1.033	0.0249
400	0.97	0.003	1.0104	1.01	0
400	0.97	0.004	1.0125	1.016	0.0031
400	0.97	0.005	1.0138	1.053	0.0389
400	0.97	0.006	1.0157	1.016	0
400	0.97	0.007	1.017	1.036	0.0187
400	0.97	0.008	1.0184	1.018	0
400	0.97	0.009	1.0201	1.032	0.0122
400	0.97	0.01	1.0212	2	0.9788
400	0.98	0.001	1.0075	1.008	0.0006
400	0.98	0.002	1.0095	1.014	0.0044
400	0.98	0.003	1.0111	1.037	0.0259
400	0.98	0.004	1.0129	1.013	0
400	0.98	0.005	1.015	1.019	0.0039
400	0.98	0.006	1.0163	1.063	0.0462
400	0.98	0.007	1.0182	1.018	0
400	0.98	0.008	1.0196	1.038	0.0189
400	0.98	0.009	1.0208	1.021	0
400	0.98	0.01	1.0227	1.033	0.0107
400	0.99	0.001	1.0076	1.008	0
400	0.99	0.002	1.0102	1.01	0
400	0.99	0.003	1.0128	1.013	0
400	0.99	0.004	1.0146	1.021	0.0067
400	0.99	0.005	1.016	1.071	0.0554
400	0.99	0.006	1.018	1.018	0
400	0.99	0.007	1.0198	1.029	0.0087
400	0.99	0.008	1.0211	1.143	0.1218
400	0.99	0.009	1.0233	1.023	0
400	0.99	0.01	1.0245	1.056	0.0311

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
500	0.75	0.001	1.0034	1.013	0.0094
500	0.75	0.002	1.0052	1.006	0.0004
500	0.75	0.003	1.0062	1.02	0.0134
500	0.75	0.004	1.0077	1.009	0.0013
500	0.75	0.005	1.0087	1.038	0.0298
500	0.75	0.006	1.01	1.014	0.0041
500	0.75	0.007	1.011	1.125	0.114
500	0.75	0.008	1.0123	1.022	0.0099
500	0.75	0.009	1.0135	1.014	0
500	0.75	0.01	1.0145	1.04	0.0255
500	0.8	0.001	1.0037	1.008	0.004
500	0.8	0.002	1.005	1.005	0
500	0.8	0.003	1.0067	1.01	0.0036
500	0.8	0.004	1.0078	1.1	0.0922
500	0.8	0.005	1.0092	1.014	0.0051
500	0.8	0.006	1.0103	1.2	0.1897
500	0.8	0.007	1.0116	1.02	0.0084
500	0.8	0.008	1.0127	1.013	0
500	0.8	0.009	1.0139	1.029	0.0146
500	0.8	0.01	1.0152	1.015	0.0002
500	0.85	0.001	1.0042	1.005	0.0012
500	0.85	0.002	1.0055	1.017	0.0111
500	0.85	0.003	1.0071	1.007	0
500	0.85	0.004	1.0084	1.016	0.0075
500	0.85	0.005	1.0095	1.01	0
500	0.85	0.006	1.011	1.018	0.0072
500	0.85	0.007	1.012	1.25	0.238
500	0.85	0.008	1.0134	1.022	0.0083
500	0.85	0.009	1.0145	1.25	0.2355
500	0.85	0.01	1.0158	1.026	0.0105
500	0.9	0.001	1.0045	1.004	0
500	0.9	0.002	1.0063	1.008	0.0014
500	0.9	0.003	1.0076	1.02	0.0124
500	0.9	0.004	1.009	1.009	0
500	0.9	0.005	1.0105	1.016	0.0054
500	0.9	0.006	1.0116	1.071	0.0598
500	0.9	0.007	1.0131	1.016	0.0027
500	0.9	0.008	1.0142	1.048	0.0334
500	0.9	0.009	1.0157	1.017	0.001
500	0.9	0.01	1.0167	1.042	0.0249
500	0.94	0.001	1.0048	1.022	0.017
500	0.94	0.002	1.0065	1.167	0.1601
500	0.94	0.003	1.0086	1.009	0
500	0.94	0.004	1.01	1.015	0.0054
500	0.94	0.005	1.0112	1.053	0.0414
500	0.94	0.006	1.0129	1.013	0
500	0.94	0.007	1.0142	1.026	0.0115
500	0.94	0.008	1.0153	1.2	0.1847
500	0.94	0.009	1.0169	1.021	0.0044
500	0.94	0.01	1.018	1.059	0.0408

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
500	0.95	0.001	1.0051	1.013	0.0079
500	0.95	0.002	1.0069	1.029	0.0225
500	0.95	0.003	1.0085	1.008	0
500	0.95	0.004	1.0105	1.011	0.0009
500	0.95	0.005	1.0117	1.024	0.0121
500	0.95	0.006	1.013	1.2	0.187
500	0.95	0.007	1.0147	1.017	0.0023
500	0.95	0.008	1.0158	1.04	0.0242
500	0.95	0.009	1.0171	1.017	0
500	0.95	0.01	1.0186	1.028	0.0092
500	0.96	0.001	1.0055	1.009	0.0035
500	0.96	0.002	1.0073	1.015	0.0078
500	0.96	0.003	1.0089	1.042	0.0328
500	0.96	0.004	1.0105	1.011	0
500	0.96	0.005	1.0123	1.015	0.0026
500	0.96	0.006	1.0135	1.033	0.0198
500	0.96	0.007	1.0148	1.015	0
500	0.96	0.008	1.0165	1.021	0.0043
500	0.96	0.009	1.0177	1.053	0.0349
500	0.96	0.01	1.0191	1.019	0
500	0.97	0.001	1.006	1.007	0.0006
500	0.97	0.002	1.0079	1.01	0.0018
500	0.97	0.003	1.0095	1.017	0.0071
500	0.97	0.004	1.011	1.043	0.0325
500	0.97	0.005	1.0125	1.013	0
500	0.97	0.006	1.0144	1.017	0.0023
500	0.97	0.007	1.0156	1.036	0.0201
500	0.97	0.008	1.0168	2	0.9832
500	0.97	0.009	1.0186	1.022	0.0031
500	0.97	0.01	1.0198	1.05	0.0302
500	0.98	0.001	1.0062	1.006	0
500	0.98	0.002	1.0082	1.008	0
500	0.98	0.003	1.0103	1.01	0
500	0.98	0.004	1.012	1.015	0.0029
500	0.98	0.005	1.0134	1.029	0.0152
500	0.98	0.006	1.0148	1.125	0.1102
500	0.98	0.007	1.0166	1.017	0
500	0.98	0.008	1.0181	1.026	0.0083
500	0.98	0.009	1.0193	1.071	0.0521
500	0.98	0.01	1.0208	1.021	0
500	0.99	0.001	1.0065	1.031	0.0247
500	0.99	0.002	1.0091	1.02	0.0109
500	0.99	0.003	1.011	1.028	0.0167
500	0.99	0.004	1.0128	1.056	0.0428
500	0.99	0.005	1.0143	1.014	0
500	0.99	0.006	1.0164	1.016	0
500	0.99	0.007	1.0181	1.023	0.0046
500	0.99	0.008	1.0194	1.045	0.026
500	0.99	0.009	1.0208	1.333	0.3125
500	0.99	0.01	1.0227	1.023	0

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
600	0.75	0.001	1.0031	1.008	0.0045
600	0.75	0.002	1.0045	1.004	0
600	0.75	0.003	1.0059	1.009	0.0034
600	0.75	0.004	1.007	1.056	0.0485
600	0.75	0.005	1.0083	1.012	0.0035
600	0.75	0.006	1.0094	1.053	0.0432
600	0.75	0.007	1.0106	1.014	0.0039
600	0.75	0.008	1.0117	1.063	0.0508
600	0.75	0.009	1.0129	1.018	0.005
600	0.75	0.01	1.014	1.077	0.063
600	0.8	0.001	1.0034	1.005	0.0019
600	0.8	0.002	1.0048	1.018	0.0131
600	0.8	0.003	1.0063	1.006	0
600	0.8	0.004	1.0074	1.014	0.0067
600	0.8	0.005	1.0085	1.167	0.1581
600	0.8	0.006	1.0099	1.014	0.0046
600	0.8	0.007	1.0109	1.059	0.0479
600	0.8	0.008	1.0122	1.016	0.0034
600	0.8	0.009	1.0133	1.048	0.0343
600	0.8	0.01	1.0145	1.017	0.0025
600	0.85	0.001	1.0039	1.004	9E-05
600	0.85	0.002	1.0052	1.008	0.0029
600	0.85	0.003	1.0065	1.024	0.0179
600	0.85	0.004	1.0079	1.008	0
600	0.85	0.005	1.0091	1.015	0.006
600	0.85	0.006	1.0102	1.063	0.0523
600	0.85	0.007	1.0116	1.014	0.0021
600	0.85	0.008	1.0127	1.033	0.0206
600	0.85	0.009	1.0139	1.014	0
600	0.85	0.01	1.0151	1.026	0.0112
600	0.9	0.001	1.0037	1.5	0.4963
600	0.9	0.002	1.0056	1.006	0
600	0.9	0.003	1.0072	1.008	0.0011
600	0.9	0.004	1.0084	1.016	0.008
600	0.9	0.005	1.0097	1.063	0.0528
600	0.9	0.006	1.0112	1.012	0.0005
600	0.9	0.007	1.0123	1.022	0.0094
600	0.9	0.008	1.0135	1.083	0.0699
600	0.9	0.009	1.0148	1.017	0.0018
600	0.9	0.01	1.016	1.033	0.0174
600	0.94	0.001	1.0045	1.009	0.0045
600	0.94	0.002	1.0062	1.013	0.007
600	0.94	0.003	1.0077	1.026	0.0186
600	0.94	0.004	1.0091	1.167	0.1576
600	0.94	0.005	1.0108	1.011	0
600	0.94	0.006	1.012	1.017	0.0052
600	0.94	0.007	1.0133	1.036	0.0225
600	0.94	0.008	1.0145	1.5	0.4855
600	0.94	0.009	1.016	1.019	0.0026
600	0.94	0.01	1.0171	1.036	0.0186

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
600	0.95	0.001	1.0048	1.007	0.0021
600	0.95	0.002	1.0065	1.009	0.0029
600	0.95	0.003	1.008	1.015	0.0069
600	0.95	0.004	1.0094	1.029	0.02
600	0.95	0.005	1.0108	1.167	0.1559
600	0.95	0.006	1.0124	1.012	0
600	0.95	0.007	1.0137	1.02	0.0059
600	0.95	0.008	1.0149	1.04	0.0251
600	0.95	0.009	1.0161	1.5	0.4839
600	0.95	0.01	1.0176	1.02	0.0024
600	0.96	0.001	1.0051	1.005	0.0003
600	0.96	0.002	1.0069	1.007	0.0002
600	0.96	0.003	1.0085	1.01	0.0016
600	0.96	0.004	1.0099	1.015	0.0055
600	0.96	0.005	1.0113	1.028	0.0165
600	0.96	0.006	1.0126	1.091	0.0783
600	0.96	0.007	1.0141	1.014	0
600	0.96	0.008	1.0155	1.02	0.0041
600	0.96	0.009	1.0167	1.036	0.019
600	0.96	0.01	1.018	1.125	0.107
600	0.97	0.001	1.0052	1.005	0
600	0.97	0.002	1.0069	1.007	0
600	0.97	0.003	1.0087	1.009	0
600	0.97	0.004	1.0104	1.01	0
600	0.97	0.005	1.0119	1.014	0.002
600	0.97	0.006	1.0133	1.022	0.0085
600	0.97	0.007	1.0146	1.042	0.0271
600	0.97	0.008	1.0159	1.2	0.1841
600	0.97	0.009	1.0175	1.017	0
600	0.97	0.01	1.0188	1.026	0.0076
600	0.98	0.001	1.0051	1.005	0
600	0.98	0.002	1.0074	1.025	0.0176
600	0.98	0.003	1.0092	1.027	0.0179
600	0.98	0.004	1.0108	1.042	0.0309
600	0.98	0.005	1.0123	1.1	0.0877
600	0.98	0.006	1.0138	1.014	0
600	0.98	0.007	1.0155	1.016	0
600	0.98	0.008	1.0169	1.021	0.0043
600	0.98	0.009	1.0182	1.034	0.0162
600	0.98	0.01	1.0195	1.077	0.0574
600	0.99	0.001	1.0062	1.009	0.0031
600	0.99	0.002	1.0085	1.008	0
600	0.99	0.003	1.0102	1.01	0
600	0.99	0.004	1.0119	1.012	0
600	0.99	0.005	1.0137	1.014	0
600	0.99	0.006	1.0154	1.015	0
600	0.99	0.007	1.0169	1.02	0.0031
600	0.99	0.008	1.0183	1.028	0.0095
600	0.99	0.009	1.0196	1.045	0.0258
600	0.99	0.01	1.021	1.1	0.079



$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
700	0.75	0.001	1.003	1.005	0.0024
700	0.75	0.002	1.0042	1.02	0.0162
700	0.75	0.003	1.0056	1.006	0.0003
700	0.75	0.004	1.0068	1.013	0.0062
700	0.75	0.005	1.0079	1.091	0.0831
700	0.75	0.006	1.0091	1.013	0.0034
700	0.75	0.007	1.0102	1.037	0.0269
700	0.75	0.008	1.0114	1.013	0.0013
700	0.75	0.009	1.0124	1.029	0.0161
700	0.75	0.01	1.0135	1.014	0
700	0.8	0.001	1.0032	1.004	0.0008
700	0.8	0.002	1.0045	1.009	0.0042
700	0.8	0.003	1.0057	1.029	0.0237
700	0.8	0.004	1.0071	1.007	0.0003
700	0.8	0.005	1.0082	1.014	0.006
700	0.8	0.006	1.0094	1.05	0.0406
700	0.8	0.007	1.0106	1.012	0.0014
700	0.8	0.008	1.0117	1.025	0.0133
700	0.8	0.009	1.0128	1.2	0.1872
700	0.8	0.01	1.014	1.019	0.0052
700	0.85	0.001	1.0034	1.003	0
700	0.85	0.002	1.005	1.005	0.0004
700	0.85	0.003	1.0062	1.009	0.0032
700	0.85	0.004	1.0074	1.02	0.013
700	0.85	0.005	1.0086	1.167	0.1581
700	0.85	0.006	1.0099	1.012	0.0018
700	0.85	0.007	1.011	1.022	0.0112
700	0.85	0.008	1.0122	1.083	0.0712
700	0.85	0.009	1.0134	1.015	0.0017
700	0.85	0.01	1.0145	1.029	0.0141
700	0.9	0.001	1.0035	1.016	0.0123
700	0.9	0.002	1.0051	1.024	0.0187
700	0.9	0.003	1.0065	1.083	0.0768
700	0.9	0.004	1.008	1.008	0
700	0.9	0.005	1.0093	1.011	0.0019
700	0.9	0.006	1.0105	1.019	0.0083
700	0.9	0.007	1.0117	1.042	0.03
700	0.9	0.008	1.0129	1.023	0.0104
700	0.9	0.009	1.0142	1.017	0.0027
700	0.9	0.01	1.0154	1.029	0.0141
700	0.94	0.001	1.0042	1.005	0.0013
700	0.94	0.002	1.0059	1.007	0.0008
700	0.94	0.003	1.0074	1.009	0.0015
700	0.94	0.004	1.0088	1.012	0.0036
700	0.94	0.005	1.0101	1.018	0.0081
700	0.94	0.006	1.0113	1.031	0.0199
700	0.94	0.007	1.0126	1.077	0.0643
700	0.94	0.008	1.0139	1.014	0
700	0.94	0.009	1.0153	1.017	0.002
700	0.94	0.01	1.0164	1.026	0.0092

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
700	0.95	0.001	1.0045	1.005	8E-05
700	0.95	0.002	1.0061	1.006	0
700	0.95	0.003	1.0076	1.008	0
700	0.95	0.004	1.0091	1.009	0
700	0.95	0.005	1.0104	1.012	0.0016
700	0.95	0.006	1.0117	1.017	0.0049
700	0.95	0.007	1.013	1.025	0.012
700	0.95	0.008	1.0142	1.045	0.0312
700	0.95	0.009	1.0155	1.143	0.1274
700	0.95	0.01	1.0168	1.017	0
700	0.96	0.001	1.0045	1.004	0
700	0.96	0.002	1.006	1.009	0.0033
700	0.96	0.003	1.0076	1.1	0.0924
700	0.96	0.004	1.0091	1.167	0.1576
700	0.96	0.005	1.0105	1.011	0
700	0.96	0.006	1.012	1.012	0
700	0.96	0.007	1.0135	1.014	0.0008
700	0.96	0.008	1.0148	1.019	0.0045
700	0.96	0.009	1.016	1.028	0.0118
700	0.96	0.01	1.0172	1.045	0.0282
700	0.97	0.001	1.0044	1.004	0
700	0.97	0.002	1.0064	1.019	0.0128
700	0.97	0.003	1.0081	1.018	0.0094
700	0.97	0.004	1.0096	1.02	0.0104
700	0.97	0.005	1.0111	1.026	0.0146
700	0.97	0.006	1.0125	1.036	0.0233
700	0.97	0.007	1.0138	1.059	0.045
700	0.97	0.008	1.0151	1.143	0.1277
700	0.97	0.009	1.0165	1.016	0
700	0.97	0.01	1.018	1.018	0
700	0.98	0.001	1.0049	1.014	0.0094
700	0.98	0.002	1.0071	1.009	0.0015
700	0.98	0.003	1.0088	1.009	0
700	0.98	0.004	1.0103	1.01	0
700	0.98	0.005	1.0118	1.012	0
700	0.98	0.006	1.0133	1.013	0
700	0.98	0.007	1.0148	1.015	0.0004
700	0.98	0.008	1.0161	1.019	0.0024
700	0.98	0.009	1.0174	1.023	0.0058
700	0.98	0.01	1.0187	1.031	0.0125
700	0.99	0.001	1.0058	1.006	0
700	0.99	0.002	1.0074	1.067	0.0592
700	0.99	0.003	1.0094	1.02	0.0102
700	0.99	0.004	1.0112	1.016	0.0052
700	0.99	0.005	1.0129	1.016	0.0033
700	0.99	0.006	1.0144	1.017	0.0028
700	0.99	0.007	1.0159	1.019	0.003
700	0.99	0.008	1.0174	1.021	0.0039
700	0.99	0.009	1.0188	1.025	0.0062
700	0.99	0.01	1.0202	1.029	0.0093

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
800	0.75	0.001	1.0028	1.004	0.0013
800	0.75	0.002	1.0041	1.01	0.0055
800	0.75	0.003	1.0052	1.042	0.0364
800	0.75	0.004	1.0065	1.007	0.0008
800	0.75	0.005	1.0076	1.014	0.0062
800	0.75	0.006	1.0087	1.045	0.0367
800	0.75	0.007	1.0099	1.011	0.0012
800	0.75	0.008	1.011	1.021	0.0098
800	0.75	0.009	1.0121	1.083	0.0713
800	0.75	0.01	1.0132	1.016	0.0026
800	0.8	0.001	1.0031	1.003	0.0001
800	0.8	0.002	1.0043	1.006	0.0013
800	0.8	0.003	1.0055	1.011	0.005
800	0.8	0.004	1.0067	1.025	0.0183
800	0.8	0.005	1.0079	1.008	0
800	0.8	0.006	1.0091	1.012	0.0025
800	0.8	0.007	1.0102	1.022	0.0115
800	0.8	0.008	1.0113	1.071	0.0601
800	0.8	0.009	1.0125	1.014	0.0012
800	0.8	0.01	1.0136	1.023	0.0097
800	0.85	0.001	1.003	1.5	0.497
800	0.85	0.002	1.0044	1.004	0
800	0.85	0.003	1.0059	1.006	0
800	0.85	0.004	1.0072	1.009	0.0014
800	0.85	0.005	1.0083	1.014	0.0052
800	0.85	0.006	1.0095	1.024	0.0149
800	0.85	0.007	1.0106	1.077	0.0663
800	0.85	0.008	1.0119	1.012	0.0002
800	0.85	0.009	1.013	1.018	0.0048
800	0.85	0.01	1.0141	1.031	0.0171
800	0.9	0.001	1.0034	1.008	0.0045
800	0.9	0.002	1.005	1.009	0.0041
800	0.9	0.003	1.0063	1.012	0.0059
800	0.9	0.004	1.0076	1.018	0.0103
800	0.9	0.005	1.0088	1.029	0.0197
800	0.9	0.006	1.0101	1.063	0.0524
800	0.9	0.007	1.0113	1.02	0.0092
800	0.9	0.008	1.0126	1.013	0.0008
800	0.9	0.009	1.0137	1.018	0.0044
800	0.9	0.01	1.0149	1.027	0.0121
800	0.94	0.001	1.004	1.004	0
800	0.94	0.002	1.0053	1.005	0
800	0.94	0.003	1.0068	1.125	0.1182
800	0.94	0.004	1.0082	1.091	0.0827
800	0.94	0.005	1.0095	1.125	0.1155
800	0.94	0.006	1.0108	1.5	0.4892
800	0.94	0.007	1.0121	1.012	0
800	0.94	0.008	1.0135	1.013	0
800	0.94	0.009	1.0147	1.016	0.0017
800	0.94	0.01	1.0159	1.021	0.0049

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
800	0.95	0.001	1.004	1.004	0
800	0.95	0.002	1.0055	1.037	0.0315
800	0.95	0.003	1.0071	1.022	0.0152
800	0.95	0.004	1.0085	1.022	0.0137
800	0.95	0.005	1.0098	1.025	0.0152
800	0.95	0.006	1.0111	1.03	0.0192
800	0.95	0.007	1.0124	1.038	0.026
800	0.95	0.008	1.0137	1.056	0.0419
800	0.95	0.009	1.0149	1.091	0.076
800	0.95	0.01	1.0162	1.25	0.2338
800	0.96	0.001	1.0039	1.004	0
800	0.96	0.002	1.0058	1.014	0.0077
800	0.96	0.003	1.0074	1.011	0.0041
800	0.96	0.004	1.0089	1.012	0.003
800	0.96	0.005	1.0102	1.013	0.0027
800	0.96	0.006	1.0116	1.014	0.0029
800	0.96	0.007	1.0129	1.017	0.0038
800	0.96	0.008	1.0142	1.02	0.0054
800	0.96	0.009	1.0154	1.023	0.0078
800	0.96	0.01	1.0167	1.029	0.0119
800	0.97	0.001	1.0042	1.017	0.0125
800	0.97	0.002	1.0062	1.008	0.0016
800	0.97	0.003	1.0078	1.008	0
800	0.97	0.004	1.0091	1.009	0
800	0.97	0.005	1.0105	1.5	0.4895
800	0.97	0.006	1.0119	1.143	0.131
800	0.97	0.007	1.0132	1.125	0.1118
800	0.97	0.008	1.0145	1.143	0.1283
800	0.97	0.009	1.0158	1.2	0.1842
800	0.97	0.01	1.0171	1.5	0.4829
800	0.98	0.001	1.0047	1.007	0.0022
800	0.98	0.002	1.0064	1.006	0
800	0.98	0.003	1.0081	1.031	0.0232
800	0.98	0.004	1.0097	1.019	0.0092
800	0.98	0.005	1.0112	1.016	0.0052
800	0.98	0.006	1.0127	1.016	0.0032
800	0.98	0.007	1.014	1.016	0.0023
800	0.98	0.008	1.0154	1.017	0.0015
800	0.98	0.009	1.0168	1.018	0.0014
800	0.98	0.01	1.0181	1.02	0.0015
800	0.99	0.001	1.0051	1.005	0
800	0.99	0.002	1.0072	1.011	0.0033
800	0.99	0.003	1.0089	1.009	0
800	0.99	0.004	1.0104	1.067	0.0562
800	0.99	0.005	1.0121	1.028	0.0157
800	0.99	0.006	1.0136	1.021	0.0072
800	0.99	0.007	1.0152	1.019	0.0034
800	0.99	0.008	1.0166	1.018	0.0013
800	0.99	0.009	1.018	1.018	0
800	0.99	0.01	1.0193	1.019	0

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
900	0.75	0.001	1.0027	1.003	0.0007
900	0.75	0.002	1.0039	1.006	0.0023
900	0.75	0.003	1.0051	1.012	0.0069
900	0.75	0.004	1.0062	1.034	0.0282
900	0.75	0.005	1.0075	1.007	0
900	0.75	0.006	1.0085	1.012	0.0034
900	0.75	0.007	1.0096	1.022	0.0126
900	0.75	0.008	1.0107	1.071	0.0607
900	0.75	0.009	1.0119	1.013	0.0011
900	0.75	0.01	1.0129	1.021	0.0084
900	0.8	0.001	1.0028	1.003	0
900	0.8	0.002	1.0042	1.004	0
900	0.8	0.003	1.0054	1.006	0.0009
900	0.8	0.004	1.0065	1.01	0.0031
900	0.8	0.005	1.0077	1.016	0.0082
900	0.8	0.006	1.0088	1.031	0.0224
900	0.8	0.007	1.0099	1.167	0.1568
900	0.8	0.008	1.0111	1.012	0.0011
900	0.8	0.009	1.0122	1.018	0.006
900	0.8	0.01	1.0133	1.031	0.018
900	0.85	0.001	1.0028	1.017	0.0138
900	0.85	0.002	1.0043	1.016	0.0118
900	0.85	0.003	1.0056	1.023	0.0177
900	0.85	0.004	1.0068	1.042	0.0349
900	0.85	0.005	1.008	1.143	0.1349
900	0.85	0.006	1.0092	1.009	0
900	0.85	0.007	1.0104	1.012	0.0013
900	0.85	0.008	1.0115	1.016	0.0043
900	0.85	0.009	1.0127	1.023	0.0101
900	0.85	0.01	1.0138	1.036	0.0219
900	0.9	0.001	1.0033	1.005	0.0019
900	0.9	0.002	1.0048	1.006	0.0008
900	0.9	0.003	1.0061	1.006	0.0003
900	0.9	0.004	1.0074	1.008	0.0003
900	0.9	0.005	1.0086	1.009	0.0005
900	0.9	0.006	1.0098	1.011	0.0011
900	0.9	0.007	1.011	1.013	0.0023
900	0.9	0.008	1.0122	1.016	0.0039
900	0.9	0.009	1.0134	1.02	0.0066
900	0.9	0.01	1.0145	1.026	0.0111
900	0.94	0.001	1.0036	1.004	0
900	0.94	0.002	1.0051	1.018	0.0124
900	0.94	0.003	1.0066	1.012	0.0054
900	0.94	0.004	1.008	1.011	0.0034
900	0.94	0.005	1.0093	1.012	0.0023
900	0.94	0.006	1.0106	1.012	0.0018
900	0.94	0.007	1.0118	1.013	0.0015
900	0.94	0.008	1.0131	1.014	0.0014
900	0.94	0.009	1.0143	1.016	0.0016
900	0.94	0.01	1.0155	1.018	0.0021

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
900	0.95	0.001	1.0035	1.005	0.0019
900	0.95	0.002	1.0053	1.01	0.0047
900	0.95	0.003	1.0069	1.008	0.0014
900	0.95	0.004	1.0083	1.008	0
900	0.95	0.005	1.0094	1.009	0
900	0.95	0.006	1.0107	1.333	0.3226
900	0.95	0.007	1.012	1.111	0.0991
900	0.95	0.008	1.0132	1.083	0.0701
900	0.95	0.009	1.0145	1.077	0.0624
900	0.95	0.01	1.0157	1.077	0.0612
900	0.96	0.001	1.0038	1.016	0.0126
900	0.96	0.002	1.0056	1.007	0.0011
900	0.96	0.003	1.007	1.007	0
900	0.96	0.004	1.0083	1.059	0.0505
900	0.96	0.005	1.0097	1.029	0.0197
900	0.96	0.006	1.0111	1.023	0.0122
900	0.96	0.007	1.0124	1.021	0.0089
900	0.96	0.008	1.0137	1.021	0.0072
900	0.96	0.009	1.0149	1.021	0.0059
900	0.96	0.01	1.0162	1.021	0.0051
900	0.97	0.001	1.0041	1.008	0.0035
900	0.97	0.002	1.0058	1.006	0
900	0.97	0.003	1.0073	1.024	0.0171
900	0.97	0.004	1.0088	1.014	0.0055
900	0.97	0.005	1.0102	1.012	0.0018
900	0.97	0.006	1.0116	1.012	0
900	0.97	0.007	1.0128	1.013	0
900	0.97	0.008	1.0141	1.167	0.1526
900	0.97	0.009	1.0153	1.083	0.068
900	0.97	0.01	1.0166	1.063	0.0459
900	0.98	0.001	1.0046	1.005	0
900	0.98	0.002	1.0061	1.018	0.0121
900	0.98	0.003	1.0079	1.009	0.001
900	0.98	0.004	1.0092	1.009	0
900	0.98	0.005	1.0106	1.04	0.0294
900	0.98	0.006	1.0121	1.023	0.0106
900	0.98	0.007	1.0135	1.018	0.0047
900	0.98	0.008	1.0149	1.016	0.0013
900	0.98	0.009	1.0161	1.016	0
900	0.98	0.01	1.0173	1.017	0
900	0.99	0.001	1.0046	1.043	0.0388
900	0.99	0.002	1.0068	1.007	0
900	0.99	0.003	1.0084	1.019	0.0101
900	0.99	0.004	1.0102	1.01	0
900	0.99	0.005	1.0114	1.167	0.1552
900	0.99	0.006	1.013	1.029	0.0164
900	0.99	0.007	1.0145	1.019	0.0047
900	0.99	0.008	1.016	1.016	0
900	0.99	0.009	1.0171	1.017	0
900	0.99	0.01	1.0185	1.1	0.0815

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
1000	0.75	0.001	1.0026	1.003	0.0002
1000	0.75	0.002	1.0038	1.005	0.0007
1000	0.75	0.003	1.005	1.007	0.002
1000	0.75	0.004	1.0061	1.011	0.005
1000	0.75	0.005	1.0072	1.02	0.0124
1000	0.75	0.006	1.0083	1.048	0.0393
1000	0.75	0.007	1.0094	1.009	0
1000	0.75	0.008	1.0105	1.013	0.0023
1000	0.75	0.009	1.0116	1.019	0.0072
1000	0.75	0.01	1.0127	1.032	0.0196
1000	0.8	0.001	1.0025	1.003	0
1000	0.8	0.002	1.0039	1.05	0.0461
1000	0.8	0.003	1.0051	1.091	0.0858
1000	0.8	0.004	1.0063	1.006	0
1000	0.8	0.005	1.0075	1.008	0.0002
1000	0.8	0.006	1.0086	1.01	0.0015
1000	0.8	0.007	1.0097	1.014	0.0038
1000	0.8	0.008	1.0108	1.019	0.008
1000	0.8	0.009	1.0119	1.028	0.0158
1000	0.8	0.01	1.013	1.048	0.0346
1000	0.85	0.001	1.0028	1.008	0.0056
1000	0.85	0.002	1.0042	1.008	0.0037
1000	0.85	0.003	1.0054	1.009	0.0036
1000	0.85	0.004	1.0067	1.011	0.0041
1000	0.85	0.005	1.0078	1.013	0.0052
1000	0.85	0.006	1.009	1.016	0.0069
1000	0.85	0.007	1.0101	1.02	0.0095
1000	0.85	0.008	1.0113	1.025	0.0137
1000	0.85	0.009	1.0124	1.032	0.0199
1000	0.85	0.01	1.0135	1.045	0.032
1000	0.9	0.001	1.0031	1.004	0.0007
1000	0.9	0.002	1.0045	1.004	0
1000	0.9	0.003	1.0058	1.036	0.0299
1000	0.9	0.004	1.0071	1.023	0.0162
1000	0.9	0.005	1.0083	1.02	0.0121
1000	0.9	0.006	1.0095	1.02	0.0105
1000	0.9	0.007	1.0107	1.02	0.0097
1000	0.9	0.008	1.0119	1.022	0.0099
1000	0.9	0.009	1.013	1.023	0.0097
1000	0.9	0.01	1.0142	1.024	0.0102
1000	0.94	0.001	1.0033	1.077	0.0737
1000	0.94	0.002	1.005	1.008	0.0027
1000	0.94	0.003	1.0064	1.006	0
1000	0.94	0.004	1.0076	1.1	0.0924
1000	0.94	0.005	1.0089	1.029	0.0205
1000	0.94	0.006	1.0102	1.021	0.0106
1000	0.94	0.007	1.0115	1.018	0.0064
1000	0.94	0.008	1.0127	1.016	0.0037
1000	0.94	0.009	1.0139	1.016	0.002
1000	0.94	0.01	1.0151	1.015	0.0003

$n$	$\alpha$	$d$	$LB$	$UB$	$Gap$
1000	0.95	0.001	1.0034	1.014	0.0111
1000	0.95	0.002	1.0052	1.006	0.0005
1000	0.95	0.003	1.0064	1.1	0.0936
1000	0.95	0.004	1.0079	1.02	0.0118
1000	0.95	0.005	1.0092	1.014	0.0047
1000	0.95	0.006	1.0105	1.012	0.0014
1000	0.95	0.007	1.0117	1.012	0
1000	0.95	0.008	1.0129	1.2	0.1871
1000	0.95	0.009	1.0141	1.067	0.0526
1000	0.95	0.01	1.0153	1.045	0.0301
1000	0.96	0.001	1.0036	1.008	0.0039
1000	0.96	0.002	1.0052	1.005	0
1000	0.96	0.003	1.0067	1.017	0.0099
1000	0.96	0.004	1.0082	1.01	0.0021
1000	0.96	0.005	1.0095	1.009	0
1000	0.96	0.006	1.0107	1.071	0.0607
1000	0.96	0.007	1.012	1.031	0.0192
1000	0.96	0.008	1.0133	1.023	0.0094
1000	0.96	0.009	1.0145	1.019	0.0047
1000	0.96	0.01	1.0158	1.017	0.0015
1000	0.97	0.001	1.004	1.005	0.0009
1000	0.97	0.002	1.0055	1.021	0.0158
1000	0.97	0.003	1.0071	1.008	0.0012
1000	0.97	0.004	1.0083	1.5	0.4917
1000	0.97	0.005	1.0098	1.024	0.0146
1000	0.97	0.006	1.0112	1.016	0.0045
1000	0.97	0.007	1.0125	1.013	0
1000	0.97	0.008	1.0136	1.333	0.3197
1000	0.97	0.009	1.0149	1.056	0.0406
1000	0.97	0.01	1.0162	1.034	0.0183
1000	0.98	0.001	1.0041	1.004	0
1000	0.98	0.002	1.006	1.007	0.0015
1000	0.98	0.003	1.0073	1.059	0.0515
1000	0.98	0.004	1.0089	1.013	0.0042
1000	0.98	0.005	1.0103	1.01	0
1000	0.98	0.006	1.0116	1.045	0.0338
1000	0.98	0.007	1.013	1.022	0.0087
1000	0.98	0.008	1.0144	1.016	0.0012
1000	0.98	0.009	1.0155	1.016	0
1000	0.98	0.01	1.0169	1.071	0.0546
1000	0.99	0.001	1.0045	1.01	0.0055
1000	0.99	0.002	1.0063	1.028	0.0214
1000	0.99	0.003	1.0081	1.008	0
1000	0.99	0.004	1.0096	1.022	0.0126
1000	0.99	0.005	1.0112	1.011	0
1000	0.99	0.006	1.0125	1.059	0.0463
1000	0.99	0.007	1.014	1.021	0.0068
1000	0.99	0.008	1.0154	1.015	0
1000	0.99	0.009	1.0166	1.083	0.0667
1000	0.99	0.01	1.018	1.033	0.0153

## Appendix G – Conditions where Sharing is more beneficial than No-Sharing

Sharing is beneficial with respect to service if  $u(1,1)_{\text{sharing}} \geq u(1,1)_{\text{no-sharing}}$ . This can be rewritten as a function of  $d_0$  as follows.

$$\begin{aligned} & \left( 2(d_1 + \mu)(d_1\mu + (\bar{\lambda} + \mu)^2) \right) d_0^2 \\ & + \left( 2(d_1 + 2d_2)\mu^3 + (4d_1^2 + 10d_1d_2 - 2d_1\bar{\lambda} + 6d_2\bar{\lambda} - \bar{\lambda}^2)\mu^2 \right. \\ & + d_1(d_1 + 3d_2 - 2\bar{\lambda})\bar{\lambda}^2 + (6d_1^2d_2 + 2d_1(d_1 + 3d_2)\bar{\lambda} - 3(d_1 - d_2)\bar{\lambda}^2 - \bar{\lambda}^3)\mu \\ & \left. + 2d_{-1}(d_1 + \mu)(d_1\mu + (\bar{\lambda} + \mu)^2) \right) d_0 \\ & + \left( 2(d_{-1}d_2 + (d_1 + d_2)(d_1 + d_2 - \bar{\lambda}))\mu^3 \right. \\ & + 2(d_1(3d_2(d_1 + d_2) + d_{-1}(d_1 + 3d_2)) - (d_1 - d_2)(d_{-1} - d_1 + d_2)\bar{\lambda} - (d_1 + d_2)\bar{\lambda}^2)\mu^2 \\ & + \left( 4d_1^2d_2(d_{-1} + d_2) + 2d_1(d_{-1} + d_2)(d_1 + d_2)\bar{\lambda} \right. \\ & + (d_1^2 - 4d_1d_2 + d_2^2 + d_{-1}(-2d_1 + d_2))\bar{\lambda}^2 - (d_1 + d_2)\bar{\lambda}^3 \Big) \mu \\ & \left. + d_1\bar{\lambda}^2((d_{-1} + d_2)(d_1 + d_2) - (d_{-1} + 2d_2)\bar{\lambda}) \right) \geq 0 \end{aligned}$$

Similarly, sharing is beneficial with respect to cost only when  $z(1,1)_{\text{sharing}} \leq z(1,1)_{\text{no-sharing}}$ .

This can be rewritten as a function of  $\mu$  as follows.

$$\begin{aligned}
& \left( \begin{aligned} & 2d_{-1}^2 c^{out} + d_1^2 (c^{in} + c^{out}) + (d_0 + d_2)(2d_0 c^{in} + d_2(c^{in} + c^{out})) + 2d_1(d_0 + d_2)(c^{in} + c^e) \\ & + d_{-1}(d_2 c^{in} + 3d_2 c^{out} + 2d_0(c^{in} + c^{out}) + d_1(c^{in} + c^{out} + 2c^e) - c^{out} \bar{\lambda} + c^e \bar{\lambda}) \\ & - d_1(c^{in} - c^e) \bar{\lambda} - (d_0 + d_2)(c^{in} - c^e) \bar{\lambda} - 2c^e \bar{\lambda}^2 \end{aligned} \right) \mu^3 \\
& + \left( \begin{aligned} & 2d_{-1}^3 c^{out} + 2(d_1 + d_2 + d_0)((3d_1 + d_0)(d_0 + d_2)c^{in} + (d_1^2 + d_2(d_0 + d_2))c^{out}) \\ & + 2((d_0 + d_2 - d_1)^2 c^{in} + 3d_1(d_0 + d_2)c^e) \bar{\lambda} \\ & - (2d_1 c^{in} + d_0 c^{in} + 2d_2 c^{in} - d_1 c^{out} - d_2 c^{out} + (d_1 + d_2 + d_0)c^e) \bar{\lambda}^2 \\ & - 2c^e \bar{\lambda}^3 + 2d_{-1}^2 (d_0 c^{in} + 2d_0 c^{out} + 3d_2 c^{out} + d_1(c^{in} + 3c^{out}) + c^{out} \bar{\lambda}) \\ & + d_{-1} \left( \begin{aligned} & 4d_1^2 (c^{in} + c^{out}) + 2(d_0 + d_2)(3d_2 c^{out} + d_0(2c^{in} + c^{out})) + 2(d_0 + d_2)(c^{in} + c^{out}) \bar{\lambda} \\ & - (c^{out} + c^e) \bar{\lambda}^2 + 2d_1(4d_2(c^{in} + c^{out}) + d_0(5c^{in} + 3c^{out}) - (c^{in} + c^{out} - 3c^e) \bar{\lambda}) \end{aligned} \right) \end{aligned} \right) \mu^2 \\
& + \left( \begin{aligned} & 2d_1(d_{-1} + d_0 + d_2) \left( \begin{aligned} & (3d_1 + d_0)(d_0 + d_2)c^{in} + (d_1^2 + d_2(d_0 + d_2))c^{in} \\ & + (d_{-1}^2 + d_1^2 + d_2(d_0 + d_2) + d_{-1}(d_1 + d_0 + 2d_2))c^{out} \\ & + ((d_1 + d_0 + d_2)c^{in} + d_{-1}c^{out}) \bar{\lambda} \end{aligned} \right) \\ & + \left( \begin{aligned} & 2d_{-1}^2 c^{out} + d_1^2 (c^{in} + c^{out}) + (d_0 + d_2)(2d_0 c^{in} + d_2(c^{in} + c^{out})) + d_{-1} \left( \begin{aligned} & 2d_0(c^{in} + c^{out}) \\ & + d_2(c^{in} + 3c^{out}) \\ & - 2d_1(c^{in} - c^e) \end{aligned} \right) \\ & + d_1(2d_2(c^{out} - 2c^{in} + c^e) + d_0(c^{out} - 3c^{in} + 2c^e)) \\ & - ((d_1 + d_0 + d_2)(c^{in} + c^e) + d_{-1}(c^{out} + c^e)) \bar{\lambda}^3 \end{aligned} \right) \bar{\lambda}^2 \end{aligned} \right) \mu \\
& + d_1 \bar{\lambda}^2 \left( \begin{aligned} & (d_{-1} + d_0 + d_2)((d_1 + 2d_0 + d_2)c^{in} + (2d_{-1} + d_1 + d_2)c^{out}) \\ & - (2(d_0 + d_2)c^{in} + d_{-1}(c^{in} + c^{out})) \bar{\lambda} \end{aligned} \right) \leq 0
\end{aligned}$$

## Appendix H – DOE Results for Multiple Pool Problem

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0	Opt	0.421	0	0.01	0
0	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0	Opt	0.04	0	0	0
0	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0	Opt	0.03	0	0.01	0
0	0	0	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0	Opt	0.04	0	0	0
0	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0	Opt	0.04	0	0	0
0	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0	Opt	0.031	0	0	0
0	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0	Opt	0.02	0	0	0
0	0	0	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	0	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0	Opt	0.03	0	0	0
0	0	0	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0	Opt	0.02	0	0.01	0
0	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.0247	Opt	0.02	0.2876	0.01	10.665
0	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.0331	Opt	0.02	0.1411	0.01	3.2619
0	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.0775	Opt	0.02	0.9584	0.01	11.367
0	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.0952	Opt	0.03	0.6472	0	5.7965
0	0	0	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0.2045	Opt	0.03	0.8099	0.01	2.9613
0	0	0	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.2364	Opt	0.02	0.6806	0.01	1.8792
0	0	0	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.3719	Opt	0.03	1.4434	0	2.8811
0	0	0	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.4182	Opt	0.03	1.2908	0	2.0866
0	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.0247	Opt	0.03	0.0992	0	3.022
0	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.0775	Opt	0.02	0.3892	0.01	4.0226
0	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.0952	Opt	0.03	0.1336	0	0.4034
0	0	0	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0.2045	Opt	0.03	0.3557	0	0.7396
0	0	0	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	0	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.3719	Opt	0.03	0.6994	0	0.8805
0	0	0	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.4182	Opt	0.03	0.4182	0	0
0	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.0493	Opt	0.03	0.5752	0	10.665
0	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.0662	Opt	0.03	0.2823	0	3.2619
0	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.155	Opt	0.031	1.9168	0	11.367
0	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.1905	Opt	0.04	1.2944	0	5.7965
0	0	0	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0.4089	Opt	0.08	1.6199	0.01	2.9613
0	0	0	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.4728	Opt	0.33	1.3612	0	1.8792
0	0	0	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.7438	Opt	0.03	2.8868	0	2.8811
0	0	0	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.8364	Opt	0.03	2.5815	0.01	2.0866
0	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.0493	Opt	0.03	0.1983	0	3.0219
0	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.155	Opt	0.03	0.7785	0.01	4.0225
0	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.1905	Opt	0.02	0.2673	0.01	0.4034
0	0	0	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	0.4089	Opt	0.03	0.7114	0	0.7396
0	0	0	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	0	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.7438	Opt	0.031	1.3988	0	0.8805
0	0	0	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.8364	Opt	0.03	0.8364	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	1	38	0.2286	Opt	0.29	0.7663	0	2.352
0	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	0.739	Opt	0.17	0.9597	0	0.2986
0	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	1	38	0.2492	Opt	0.531	0.8802	0	2.5323
0	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	0.7195	Opt	0.05	1.0995	0	0.5283
0	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	0.646	Opt	0.04	1.5982	0	1.4741
0	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	1.1663	Opt	0.12	1.7888	0	0.5338
0	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	8	0	42	0.7271	Opt	0.201	1.7105	0.01	1.3526
0	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	6	0	44	1.2334	Opt	0.47	1.9336	0	0.5677
0	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	1	44	0.2882	Opt	0.121	0.4672	0	0.6208
0	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	5	1	44	0.3112	Opt	0.14	0.5411	0	0.739
0	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	1	0	49	0.8626	Opt	0.03	0.8782	0.01	0.0182
0	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	0.7702	Opt	0.21	1.0437	0	0.3552
0	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	3	0	47	0.862	Opt	0.291	1.1285	0	0.3092
0	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.4373	Opt	0.03	1.4373	0	0
0	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.3646	Opt	0.04	1.1233	0	2.0805
0	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.8873	Opt	0.04	1.183	0.01	0.3332
0	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.448	Opt	0.03	1.9258	0	3.2985
0	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.9772	Opt	0.04	1.9039	0	0.9483
0	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.0268	Opt	0.04	2.5229	0	1.457
0	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	1.5824	Opt	0.03	2.6266	0.01	0.6599
0	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	1.2912	Opt	0.03	3.2832	0	1.5427
0	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.8555	Opt	0.04	3.321	0	0.7898
0	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.3646	Opt	0.03	0.65	0.01	0.7825
0	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
0	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.448	Opt	0.03	1.0805	0	1.4117
0	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	0.9772	Opt	0.04	1.0564	0	0.081
0	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.0268	Opt	0.03	1.4379	0	0.4003
0	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	1.2912	Opt	0.07	1.9329	0	0.497
0	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.8555	Opt	0.04	1.8555	0	0
0	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.3893	Opt	0.051	1.3904	0	2.5716
0	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	0.9205	Opt	0.05	1.3364	0	0.4519
0	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.5255	Opt	0.04	2.8803	0	4.481
0	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.0724	Opt	0.06	2.5777	0	1.4036
0	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.2313	Opt	0.03	3.3253	0.01	1.7007
0	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	1.8188	Opt	0.1	3.2748	0	0.8005
0	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	1.6631	Opt	0.06	4.7099	0.01	1.832
0	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	2.2737	Opt	0.08	4.6821	0	1.0593
0	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.3893	Opt	0.15	0.7329	0	0.8825
0	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.5255	Opt	0.071	1.4697	0.01	1.7967
0	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.0724	Opt	0.06	1.19	0	0.1096
0	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.2313	Opt	0.03	1.7935	0	0.4566
0	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	1.6631	Opt	0.05	2.6323	0.01	0.5827
0	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	2.2737	Opt	0.03	2.2737	0	0



Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	1	38	0.4572	Opt	0.28	1.5326	0	2.352
0	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	1.478	Opt	0.291	1.9194	0	0.2986
0	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	1	38	0.4984	Opt	0.32	1.7603	0	2.5323
0	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	1.4389	Opt	0.09	2.199	0	0.5283
0	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	1.292	Opt	0.07	3.1965	0	1.4741
0	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	2.3325	Opt	0.191	3.5777	0.01	0.5338
0	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	8	0	42	1.4541	Opt	0.41	3.421	0	1.3526
0	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	6	0	44	2.4667	Opt	0.611	3.8672	0	0.5677
0	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	1	44	0.5765	Opt	0.16	0.9344	0	0.6208
0	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	5	1	44	0.6223	Opt	0.161	1.0823	0.01	0.7391
0	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	1	0	49	1.7252	Opt	0.03	1.7565	0.01	0.0181
0	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	1.5403	Opt	0.23	2.0874	0	0.3552
0	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	3	0	47	1.724	Opt	0.34	2.2571	0	0.3092
0	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	2.8746	Opt	0.041	2.8746	0	0
0	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.7046	Opt	0.05	1.8996	0	1.6958
0	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	1.7416	Opt	0.04	2.2117	0	0.2699
0	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.8185	Opt	0.03	2.8095	0	2.4323
0	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.8592	Opt	0.04	3.137	0	0.6873
0	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.8492	Opt	0.04	4.1819	0	1.2615
0	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	2.9284	Opt	0.03	4.4738	0.01	0.5277
0	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	2.2105	Opt	0.03	5.0132	0	1.2679
0	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.2928	Opt	0.03	5.383	0.01	0.6348
0	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.7046	Opt	0.03	1.1143	0	0.5814
0	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.8185	Opt	0.03	1.6669	0.01	1.0365
0	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.8592	Opt	0.03	1.9719	0	0.0606
0	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	1.8492	Opt	0.04	2.467	0	0.3341
0	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	2.2105	Opt	0.03	3.1283	0	0.4152
0	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.2928	Opt	0.03	3.2928	0.01	0
0	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.7293	Opt	0.03	2.2466	0	2.0805
0	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	1.7747	Opt	0.03	2.3659	0.01	0.3332
0	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.896	Opt	0.03	3.8516	0	3.2986
0	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.9544	Opt	0.041	3.8079	0	0.9483
0	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	2.0537	Opt	0.03	5.0459	0	1.457
0	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	3.1648	Opt	0.03	5.2531	0	0.6599
0	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	2.5824	Opt	0.03	6.5663	0	1.5427
0	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.711	Opt	0.03	6.6419	0	0.7898
0	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	0.7293	Opt	0.03	1.3	0	0.7825
0	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	0.896	Opt	0.04	2.1609	0	1.4117
0	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1.9544	Opt	0.03	2.1127	0	0.081
0	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	2.0537	Opt	0.04	2.8757	0	0.4003
0	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	2.5824	Opt	0.03	3.8658	0	0.497
0	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.711	Opt	0.08	3.711	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	2	37	1.8042	Opt	0.17	2.3446	0.01	0.2995
0	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	2.5124	Opt	0.171	2.7447	0	0.0925
0	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	2	37	2.6709	Opt	0.26	3.3165	0	0.2417
0	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	3.3387	Opt	0.11	3.7336	0	0.1183
0	0.5	1	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	4.1099	Opt	0.341	5.0625	0	0.2318
0	0.5	1	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	4.8326	Opt	0.13	5.4902	0	0.1361
0	0.5	1	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	8	0	42	5.0347	Opt	0.39	6.0231	0	0.1963
0	0.5	1	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	6	0	44	5.7438	Opt	1.232	6.4773	0	0.1277
0	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	2	43	2.0752	Opt	0.18	2.2624	0.01	0.0902
0	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0.01	0
0	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	5	2	43	3.0562	Opt	0.211	3.2885	0	0.076
0	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	1	0	49	3.8323	Opt	0.05	3.848	0	0.0041
0	0.5	1	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	4.6948	Opt	0.24	4.9737	0	0.0594
0	0.5	1	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	1	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	3	0	47	5.7446	Opt	0.411	6.0441	0	0.0521
0	0.5	1	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	6.5701	Opt	0.03	6.5701	0	0
0	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.2843	Opt	0.03	2.7001	0	0.182
0	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	2.8016	Opt	0.03	2.9666	0	0.0589
0	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.463	Opt	0.04	4.3481	0	0.2556
0	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.9851	Opt	0.03	4.5375	0	0.1386
0	0.5	1	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.1555	Opt	0.03	6.004	0	0.1646
0	0.5	1	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	5.6932	Opt	0.03	6.2919	0	0.1052
0	0.5	1	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.4439	Opt	0.03	7.6202	0	0.1825
0	0.5	1	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	6.9883	Opt	0.03	7.8409	0	0.122
0	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.2843	Opt	0.04	2.4312	0	0.0643
0	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.463	Opt	0.03	3.8312	0	0.1063
0	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	3.9851	Opt	0.03	4.0311	0.01	0.0115
0	0.5	1	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.1555	Opt	0.03	5.3862	0	0.0448
0	0.5	1	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	1	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.4439	Opt	0.031	6.8193	0.01	0.0583
0	0.5	1	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	6.9883	Opt	0.03	6.9883	0	0
0	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.3089	Opt	0.03	2.9993	0.01	0.299
0	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	2.8347	Opt	0.03	3.1146	0	0.0988
0	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.5405	Opt	0.03	5.3026	0.01	0.4977
0	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.0804	Opt	0.03	5.201	0	0.2746
0	0.5	1	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.36	Opt	0.04	6.7941	0	0.2676
0	0.5	1	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	5.9295	Opt	0.03	6.9537	0.01	0.1727
0	0.5	1	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.8158	Opt	0.03	9.0536	0	0.3283
0	0.5	1	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	7.4065	Opt	0.04	9.1924	0	0.2411
0	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.3089	Opt	0.03	2.5304	0	0.0959
0	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.5405	Opt	0.04	4.2205	0	0.192
0	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.0804	Opt	0.03	4.1647	0.01	0.0207
0	0.5	1	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.36	Opt	0.03	5.7419	0	0.0713
0	0.5	1	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	0.5	1	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.8158	Opt	0.04	7.5187	0	0.1031
0	0.5	1	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	7.4065	Opt	0.03	7.4065	0.01	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	2	37	2.033	Opt	0.211	3.1109	0	0.5302
0	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	3.2514	Opt	0.19	3.7044	0	0.1393
0	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	2	37	2.9203	Opt	0.451	4.1967	0	0.4371
0	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	4.0584	Opt	0.15	4.8339	0.01	0.1911
0	0.5	2	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	4.757	Opt	0.29	6.6607	0	0.4002
0	0.5	2	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	5.9988	Opt	0.11	7.3136	0	0.2192
0	0.5	2	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	8	0	42	5.762	Opt	0.241	7.7337	0	0.3422
0	0.5	2	0	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	6	0	44	6.9772	Opt	1.482	8.4109	0	0.2055
0	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	2	43	2.3642	Opt	0.16	2.7296	0.01	0.1546
0	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0.01	0
0	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	5	2	43	3.3676	Opt	0.19	3.8296	0	0.1372
0	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	1	0	49	4.6949	Opt	0.05	4.7262	0.01	0.0067
0	0.5	2	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	5.465	Opt	0.231	6.0174	0	0.1011
0	0.5	2	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	2	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	3	0	47	6.607	Opt	0.611	7.1727	0	0.0856
0	0.5	2	0	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	8.0074	Opt	0.04	8.0074	0	0
0	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.6243	Opt	0.04	3.52	0	0.3413
0	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	3.6558	Opt	0.04	4.0041	0	0.0953
0	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.8336	Opt	0.04	5.2458	0	0.3684
0	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.8671	Opt	0.04	5.7574	0	0.1829
0	0.5	2	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.9779	Opt	0.03	7.6596	0	0.2813
0	0.5	2	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	7.0392	Opt	0.04	8.1451	0	0.1571
0	0.5	2	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	7.3632	Opt	0.04	9.4515	0	0.2836
0	0.5	2	1.5	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	8.4256	Opt	0.04	9.9052	0	0.1756
0	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.6243	Opt	0.04	2.917	0	0.1116
0	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.8336	Opt	0.03	4.4259	0.01	0.1545
0	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.8671	Opt	0.04	4.9416	0	0.0153
0	0.5	2	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	5.9779	Opt	0.03	6.4219	0.01	0.0743
0	0.5	2	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
0	0.5	2	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	7.3632	Opt	0.031	8.0145	0.01	0.0884
0	0.5	2	1.5	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	8.4256	Opt	0.03	8.4256	0.01	0
0	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.6489	Opt	0.03	3.8117	0.01	0.439
0	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	3.6889	Opt	0.03	4.1496	0	0.1249
0	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.9111	Opt	0.03	6.2739	0.01	0.6041
0	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.9624	Opt	0.03	6.4414	0	0.2981
0	0.5	2	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	6.1823	Opt	0.04	8.5203	0	0.3782
0	0.5	2	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	7.2756	Opt	0.03	8.9185	0.01	0.2258
0	0.5	2	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	7.7351	Opt	0.04	10.903	0	0.4096
0	0.5	2	3	0.75	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	8.8438	Opt	0.03	11.181	0.01	0.2642
0	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	2.6489	Opt	0.03	3.0649	0	0.157
0	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
0	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	3.9111	Opt	0.04	4.9117	0	0.2558
0	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	4.9624	Opt	0.04	5.0874	0	0.0252
0	0.5	2	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	6.1823	Opt	0.04	6.8241	0	0.1038
0	0.5	2	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	0.5	2	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	7.7351	Opt	0.03	8.7523	0.01	0.1315
0	0.5	2	3	0.85	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	8.8438	Opt	0.03	8.8438	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	2	37	3.3797	Opt	0.181	3.9324	0	0.1635
0	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	4.2857	Opt	0.17	4.5296	0	0.0569
0	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	2	37	5.0926	Opt	0.36	5.7528	0	0.1297
0	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	5.9574	Opt	0.171	6.367	0	0.0688
0	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	7.571	Opt	0.731	8.5267	0	0.1262
0	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	8.4989	Opt	0.19	9.1571	0	0.0774
0	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	8	0	42	9.3415	Opt	0.601	10.336	0	0.1065
0	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	6	0	44	10.254	Opt	1.061	10.988	0	0.0715
0	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	2	43	3.8615	Opt	0.261	4.0616	0	0.0518
0	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	5	2	43	5.8009	Opt	0.15	6.0358	0.01	0.0405
0	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	1	0	49	6.802	Opt	0.05	6.8177	0	0.0023
0	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	8.6194	Opt	0.371	8.9038	0	0.033
0	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	3	0	47	10.627	Opt	0.46	10.96	0.01	0.0313
0	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	11.703	Opt	0.03	11.703	0	0
0	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.2039	Opt	0.03	4.2915	0	0.0208
0	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	4.7158	Opt	0.04	4.7518	0	0.0076
0	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.4781	Opt	0.031	6.7717	0	0.0453
0	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	6.993	Opt	0.03	7.177	0	0.0263
0	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	9.2842	Opt	0.04	9.486	0	0.0217
0	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	9.8039	Opt	0.05	9.952	0	0.0151
0	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	11.597	Opt	0.03	11.954	0	0.0308
0	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	12.121	Opt	0.03	12.412	0	0.024
0	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.2039	Opt	0.03	4.2287	0	0.0059
0	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.4781	Opt	0.03	6.582	0	0.016
0	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	6.993	Opt	0.03	7.0058	0.01	0.0018
0	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	9.2842	Opt	0.03	9.3346	0	0.0054
0	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	11.597	Opt	0.03	11.706	0	0.0094
0	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	12.121	Opt	0.04	12.121	0	0
0	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.2285	Opt	0.04	4.5791	0	0.0829
0	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	4.7489	Opt	0.03	4.8929	0	0.0303
0	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.5556	Opt	0.03	7.7301	0	0.1792
0	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	7.0883	Opt	0.04	7.8242	0	0.1038
0	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	9.4887	Opt	0.04	10.296	0	0.0851
0	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	10.04	Opt	0.041	10.633	0	0.059
0	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	11.969	Opt	0.04	13.397	0	0.1194
0	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	12.539	Opt	0.04	13.703	0	0.0928
0	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.2285	Opt	0.03	4.3279	0.01	0.0235
0	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
0	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	0	50	6.5556	Opt	0.03	6.9712	0.01	0.0634
0	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	7.0883	Opt	0.03	7.1395	0	0.0072
0	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	9.4887	Opt	0.04	9.6903	0	0.0212
0	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	0	50	11.969	Opt	0.03	12.405	0.01	0.0365
0	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	12.539	Opt	0.03	12.539	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
0	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	11	2	37	3.6085	Opt	0.16	4.6892	0	0.2995
0	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	6	2	42	5.0248	Opt	0.16	5.4893	0.01	0.0925
0	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	11	2	37	5.3419	Opt	0.231	6.633	0	0.2417
0	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	8	1	41	6.6775	Opt	0.12	7.4673	0	0.1183
0	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	8	0	42	8.2198	Opt	0.35	10.125	0	0.2318
0	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	6	0	44	9.6652	Opt	0.131	10.98	0	0.1361
0	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	8	0	42	10.07	Opt	0.37	12.046	0	0.1963
0	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	6	0	44	11.488	Opt	2.444	12.955	0	0.1277
0	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	2	43	4.1504	Opt	0.19	4.5249	0	0.0902
0	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	1	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	5	2	43	6.1124	Opt	0.19	6.5769	0	0.076
0	1	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	1	0	49	7.6646	Opt	0.06	7.6959	0	0.0041
0	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	0	47	9.3896	Opt	0.261	9.9475	0	0.0594
0	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	3	0	47	11.489	Opt	0.41	12.088	0	0.0521
0	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	13.14	Opt	0.04	13.14	0	0
0	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.5439	Opt	0.03	5.0983	0.01	0.122
0	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	5.57	Opt	0.031	5.7748	0	0.0368
0	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	0	50	6.8486	Opt	0.03	7.6821	0	0.1217
0	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	7.875	Opt	0.04	8.3778	0	0.0638
0	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	10.107	Opt	0.03	11.137	0.01	0.102
0	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	11.15	Opt	0.03	11.786	0	0.057
0	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	0	50	12.516	Opt	0.03	13.752	0	0.0987
0	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	13.558	Opt	0.04	14.396	0	0.0617
0	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.5439	Opt	0.04	4.729	0	0.0407
0	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	0	50	6.8486	Opt	0.04	7.2016	0	0.0515
0	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	7.875	Opt	0.03	7.9113	0.01	0.0046
0	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	10.107	Opt	0.03	10.427	0	0.0317
0	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
0	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	0	50	12.516	Opt	0.04	12.856	0	0.0272
0	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	13.558	Opt	0.04	13.558	0	0
0	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.5685	Opt	0.04	5.4002	0	0.182
0	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	0	50	5.6031	Opt	0.03	5.9332	0.01	0.0589
0	1	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	0	50	6.9261	Opt	0.03	8.6962	0	0.2556
0	1	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	7.9703	Opt	0.03	9.0749	0	0.1386
0	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	10.311	Opt	0.04	12.008	0	0.1646
0	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	0	50	11.386	Opt	0.031	12.584	0.01	0.1052
0	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	0	50	12.888	Opt	0.03	15.241	0	0.1826
0	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	13.977	Opt	0.03	15.682	0	0.122
0	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	0	50	4.5685	Opt	0.04	4.8624	0	0.0643
0	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0	0	0	0
0	1	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	0	50	6.9261	Opt	0.03	7.6625	0	0.1063
0	1	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	7.9703	Opt	0.04	8.0622	0	0.0115
0	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	0	50	10.311	Opt	0.03	10.773	0.01	0.0448
0	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
0	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	0	50	12.888	Opt	0.04	13.639	0	0.0583
0	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	13.977	Opt	0.03	13.977	0.01	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	2	38	10	290	Opt	0.04	295	0.01	0.0172
5	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	375	Opt	0.05	375	0	0
5	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	265	Opt	0.05	265	0	0
5	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	315	Opt	0.04	315	0	0
5	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	2	18	30	390	Opt	0.05	390	0	0
5	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	2	11	37	425	Opt	0.05	425	0	0
5	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	380	Opt	0.051	380	0	0
5	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	410	Opt	0.06	410	0	0
5	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375	Opt	0.05	375	0	0
5	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	0	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	350	Opt	0.04	350	0.01	0
5	0	0	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	465	Opt	0.05	465	0	0
5	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	1	5	44	465	Opt	0.05	465	0	0
5	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	460	Opt	0.05	460	0	0
5	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	500	Opt	0.04	500	0	0
5	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	290.42	Opt	0.06	295.37	0	0.017
5	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	375.24	Opt	0.05	375.26	0	5E-05
5	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	266.05	Opt	0.05	266.05	0	0
5	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	37	13	315.88	Opt	0.05	315.88	0	0
5	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	390.89	Opt	0.05	390.9	0	3E-05
5	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	425.73	Opt	0.05	425.74	0	2E-05
5	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	381.57	Opt	0.06	381.57	0	0
5	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	411.35	Opt	0.06	411.35	0	0
5	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.19	Opt	0.05	375.2	0.01	3E-05
5	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	350.6	Opt	0.05	350.6	0	0
5	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	465.2	Opt	0.05	465.21	0.01	3E-05
5	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	465.39	Opt	0.05	465.39	0	0
5	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	460.71	Opt	0.05	460.71	0	0
5	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	500.42	Opt	0.04	500.42	0	0
5	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	290.84	Opt	0.06	295.74	0	0.0168
5	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	375.48	Opt	0.05	375.52	0	9E-05
5	0	0	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	267.07	Opt	0.05	267.1	0	0.0001
5	0	0	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	37	13	316.76	Opt	0.051	316.76	0.01	0
5	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	391.79	Opt	0.05	391.81	0	5E-05
5	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	426.46	Opt	0.06	426.48	0	5E-05
5	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	383.06	Opt	0.07	383.14	0	0.0002
5	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	412.64	Opt	0.06	412.7	0	0.0002
5	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.38	Opt	0.05	375.4	0	5E-05
5	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	0	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	351.21	Opt	0.05	351.21	0	0
5	0	0	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	465.39	Opt	0.05	465.42	0	6E-05
5	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	465.78	Opt	0.04	465.78	0.01	0
5	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	461.42	Opt	0.05	461.42	0	0
5	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	500.84	Opt	0.03	500.84	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	290.62	Opt	0.06	295.77	0	0.0177
5	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	375.95	Opt	0.061	375.98	0	9E-05
5	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	265.85	Opt	0.05	265.9	0	0.0002
5	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	316.15	Opt	0.05	316.15	0.01	0
5	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	391.21	Opt	0.05	391.68	0	0.0012
5	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	426.48	Opt	0.06	426.88	0	0.0009
5	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	381.66	Opt	0.16	381.77	0	0.0003
5	0	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	411.91	Opt	0.18	412.02	0	0.0003
5	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.48	Opt	0.06	375.48	0	0
5	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	350.56	Opt	0.051	350.56	0.01	0
5	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	465.88	Opt	0.05	465.88	0	0
5	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	465.83	Opt	0.05	466.68	0	0.0006
5	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	461.11	Opt	0.05	461.19	0	0.0002
5	0	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	501.44	Opt	0.06	501.44	0	0
5	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	291.19	Opt	0.04	296.14	0	0.017
5	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	376.24	Opt	0.05	376.24	0	0
5	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	266.94	Opt	0.05	266.94	0	0
5	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	317.03	Opt	0.04	317.03	0.01	0
5	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	392.58	Opt	0.05	392.58	0	0
5	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	427.62	Opt	0.05	427.62	0	2E-06
5	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	383.34	Opt	0.05	383.34	0.01	0
5	0	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	413.37	Opt	0.051	413.37	0	0
5	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.69	Opt	0.04	375.69	0.01	0
5	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	351.16	Opt	0.05	351.16	0	0
5	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	466.09	Opt	0.04	466.09	0.01	4E-06
5	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	466.47	Opt	0.05	466.48	0.01	1E-05
5	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	461.9	Opt	0.05	461.9	0	0
5	0	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	501.86	Opt	0.03	501.86	0	0
5	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	291.61	Opt	0.05	296.51	0	0.0168
5	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	376.49	Opt	0.06	376.49	0	0
5	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	267.99	Opt	0.05	267.99	0	0
5	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	317.9	Opt	0.06	317.9	0	0
5	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	393.48	Opt	0.06	393.48	0	1E-05
5	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	428.35	Opt	0.061	428.36	0	3E-05
5	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	384.91	Opt	0.06	384.91	0	0
5	0	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	414.73	Opt	0.06	414.73	0	0
5	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.88	Opt	0.05	375.89	0	3E-05
5	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	351.77	Opt	0.05	351.77	0	0
5	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	466.29	Opt	0.05	466.3	0	3E-05
5	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	466.86	Opt	0.05	466.86	0	0
5	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	462.61	Opt	0.06	462.61	0	0
5	0	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	502.27	Opt	0.04	502.27	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	291.24	Opt	0.05	296.54	0	0.0182
5	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	376.89	Opt	0.05	376.96	0	0.0002
5	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	266.7	Opt	0.05	266.79	0	0.0003
5	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	317.3	Opt	0.051	317.3	0.01	0
5	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	392.41	Opt	0.06	393.35	0	0.0024
5	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	427.97	Opt	0.06	428.76	0.01	0.0018
5	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	383.32	Opt	0.17	383.54	0	0.0006
5	0	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	413.81	Opt	0.2	414.02	0	0.0005
5	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	375.97	Opt	0.06	375.97	0	0
5	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	351.12	Opt	0.05	351.12	0.01	0
5	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	466.77	Opt	0.051	466.77	0	0
5	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	466.65	Opt	0.05	467.17	0.01	0.0011
5	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	462.2	Opt	0.07	462.38	0	0.0004
5	0	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	502.88	Opt	0.04	502.88	0	0
5	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	291.9	Opt	0.05	296.91	0	0.0172
5	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	377.21	Opt	0.06	377.21	0	0
5	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	267.84	Opt	0.05	267.84	0	0
5	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	318.18	Opt	0.05	318.18	0	0
5	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	394.04	Opt	0.05	394.26	0.01	0.0005
5	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	429.32	Opt	0.06	429.5	0	0.0004
5	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	385.11	Opt	0.06	385.11	0	0
5	0	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	415.4	Opt	0.06	415.4	0	0
5	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	376.17	Opt	0.051	376.17	0.01	0
5	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	351.72	Opt	0.05	351.72	0.01	0
5	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	466.98	Opt	0.05	466.98	0	0
5	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	467.46	Opt	0.06	467.56	0	0.0002
5	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	463.09	Opt	0.05	463.09	0.01	0
5	0	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	503.29	Opt	0.03	503.29	0.01	0
5	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	292.37	Opt	0.05	297.28	0	0.0168
5	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	377.47	Opt	0.06	377.47	0	0
5	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	268.89	Opt	0.06	268.89	0	0
5	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	319.05	Opt	0.05	319.05	0	0
5	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	395.16	Opt	0.06	395.16	0	0
5	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	430.24	Opt	0.06	430.24	0	7E-06
5	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	386.68	Opt	0.061	386.68	0	0
5	0	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	416.75	Opt	0.06	416.75	0	0
5	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	376.37	Opt	0.05	376.37	0	0
5	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	352.33	Opt	0.05	352.33	0	0
5	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	467.18	Opt	0.06	467.19	0	1E-05
5	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	467.95	Opt	0.06	467.95	0	1E-05
5	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	463.8	Opt	0.05	463.8	0	0
5	0	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	503.71	Opt	0.04	503.71	0	0



Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	292.2	Opt	0.05	297.36	0.01	0.0177
5	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	377.72	Opt	0.05	377.76	0.01	9E-05
5	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	268.27	Opt	0.05	268.32	0	0.0002
5	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	318.76	Opt	0.05	318.76	0.01	0
5	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	394.68	Opt	0.061	395.15	0	0.0012
5	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	430.15	Opt	0.06	430.55	0	0.0009
5	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	385.97	Opt	0.16	386.1	0	0.0003
5	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	416.41	Opt	0.17	416.55	0	0.0003
5	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	377.27	Opt	0.06	377.27	0	0
5	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	353.31	Opt	0.05	353.31	0	0
5	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0.01,0.02]	0	7	43	468.85	Opt	0.05	468.85	0	9E-06
5	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	469.75	Opt	0.05	470.02	0	0.0006
5	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.021	0	0	0
5	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	466	Opt	0.06	466.1	0	0.0002
5	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	506.57	Opt	0.04	506.57	0	0
5	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	292.76	Opt	0.05	297.73	0.01	0.017
5	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	378.01	Opt	0.05	378.01	0	0
5	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	269.37	Opt	0.05	269.37	0	0
5	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	319.64	Opt	0.05	319.64	0	0
5	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	396.05	Opt	0.06	396.05	0	0
5	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	431.29	Opt	0.06	431.3	0	5E-06
5	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	387.67	Opt	0.06	387.67	0	0
5	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	417.9	Opt	0.06	417.9	0	0
5	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	377.48	Opt	0.06	377.48	0	0
5	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	353.91	Opt	0.061	353.91	0	0
5	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	469.06	Opt	0.05	469.06	0.01	9E-06
5	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	470.41	Opt	0.05	470.41	0.01	1E-05
5	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
5	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	466.8	Opt	0.06	466.8	0	0
5	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	506.99	Opt	0.04	506.99	0	0
5	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	293.18	Opt	0.06	298.1	0	0.0168
5	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	378.25	Opt	0.06	378.27	0	4E-05
5	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	270.42	Opt	0.06	270.42	0	0
5	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	320.52	Opt	0.05	320.52	0	0
5	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	396.94	Opt	0.06	396.95	0	2E-05
5	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	432.02	Opt	0.06	432.04	0.01	4E-05
5	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	389.24	Opt	0.06	389.24	0	0
5	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	419.26	Opt	0.051	419.26	0.01	0
5	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	377.66	Opt	0.05	377.68	0	4E-05
5	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	354.51	Opt	0.05	354.51	0	0
5	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	469.25	Opt	0.06	469.27	0	4E-05
5	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	470.8	Opt	0.05	470.8	0	0
5	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	467.51	Opt	0.06	467.51	0	0
5	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	507.41	Opt	0.04	507.41	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	292.82	Opt	0.06	298.13	0	0.0181
5	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	1	23	26	378.67	Opt	0.06	378.73	0.01	0.0002
5	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	1	45	4	269.12	Opt	0.05	269.22	0.01	0.0004
5	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	319.91	Opt	0.05	319.91	0	0
5	0.5	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	395.88	Opt	0.06	396.82	0.01	0.0024
5	0.5	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	431.63	Opt	0.071	432.43	0	0.0019
5	0.5	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	387.63	Opt	0.2	387.87	0	0.0006
5	0.5	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	418.32	Opt	0.24	418.55	0	0.0006
5	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	377.76	Opt	0.06	377.76	0	0
5	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	353.87	Opt	0.05	353.87	0	0
5	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	469.73	Opt	0.061	469.74	0	1E-05
5	0.5	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	470.58	Opt	0.06	471.1	0	0.0011
5	0.5	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	467.09	Opt	0.08	467.29	0	0.0004
5	0.5	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	508.01	Opt	0.04	508.01	0	0
5	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	293.47	Opt	0.06	298.5	0	0.0171
5	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	1	23	26	378.98	Opt	0.06	378.99	0	2E-05
5	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	270.27	Opt	0.05	270.27	0	0
5	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	320.79	Opt	0.05	320.79	0	0
5	0.5	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	397.5	Opt	0.05	397.72	0.01	0.0006
5	0.5	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	432.99	Opt	0.06	433.17	0	0.0004
5	0.5	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	389.41	Opt	0.06	389.44	0	6E-05
5	0.5	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	419.9	Opt	0.06	419.93	0	6E-05
5	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	377.96	Opt	0.051	377.96	0	0
5	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	354.47	Opt	0.05	354.47	0	0
5	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	469.94	Opt	0.05	469.94	0.01	0
5	0.5	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	471.39	Opt	0.06	471.5	0	0.0002
5	0.5	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	467.99	Opt	0.06	467.99	0	0
5	0.5	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	508.43	Opt	0.04	508.43	0.01	0
5	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	293.95	Opt	0.05	298.87	0	0.0167
5	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	379.25	Opt	0.06	379.25	0	0
5	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	271.32	Opt	0.05	271.32	0	0
5	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	321.67	Opt	0.05	321.67	0.01	0
5	0.5	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	398.63	Opt	0.06	398.63	0	0
5	0.5	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	433.91	Opt	0.061	433.92	0	9E-06
5	0.5	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	391.01	Opt	0.06	391.01	0	0
5	0.5	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	421.28	Opt	0.06	421.28	0	0
5	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	378.16	Opt	0.06	378.16	0	0
5	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	355.07	Opt	0.05	355.07	0	0
5	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	470.15	Opt	0.06	470.15	0	1E-05
5	0.5	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	471.88	Opt	0.06	471.89	0	2E-05
5	0.5	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	0.5	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	468.7	Opt	0.06	468.7	0	0
5	0.5	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	508.84	Opt	0.04	508.84	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	293.77	Opt	0.06	298.95	0	0.0176
5	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	379.49	Opt	0.06	379.53	0	0.0001
5	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	270.69	Opt	0.05	270.75	0	0.0002
5	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	321.38	Opt	0.061	321.38	0	0
5	1	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	398.14	Opt	0.06	398.61	0	0.0012
5	1	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	433.82	Opt	0.07	434.23	0	0.001
5	1	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	390.28	Opt	0.18	390.43	0	0.0004
5	1	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	420.92	Opt	0.24	421.08	0	0.0004
5	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.06	Opt	0.06	379.06	0	5E-06
5	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	1	1	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	356.05	Opt	0.051	356.05	0	0
5	1	1	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	471.82	Opt	0.06	471.82	0	1E-05
5	1	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	473.68	Opt	0.06	473.95	0	0.0006
5	1	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	1	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	470.87	Opt	0.06	471	0	0.0003
5	1	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	511.7	Opt	0.04	511.7	0.01	0
5	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	294.34	Opt	0.05	299.32	0	0.0169
5	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	379.79	Opt	0.06	379.79	0.01	2E-05
5	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	271.8	Opt	0.05	271.8	0	0
5	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	322.25	Opt	0.06	322.25	0	0
5	1	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	399.51	Opt	0.06	399.52	0	1E-05
5	1	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	434.97	Opt	0.06	434.97	0	7E-06
5	1	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	392	Opt	0.06	392	0	0
5	1	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	422.43	Opt	0.061	422.43	0.01	0
5	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.26	Opt	0.05	379.26	0	1E-05
5	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	356.65	Opt	0.05	356.65	0	0
5	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	472.03	Opt	0.05	472.03	0	8E-06
5	1	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	474.34	Opt	0.06	474.35	0	2E-05
5	1	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	1	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	471.71	Opt	0.06	471.71	0	0
5	1	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	512.12	Opt	0.04	512.12	0	0
5	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	294.76	Opt	0.06	299.69	0	0.0167
5	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	380.03	Opt	0.06	380.05	0.01	6E-05
5	1	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	272.85	Opt	0.05	272.85	0	0
5	1	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	323.13	Opt	0.06	323.13	0	0
5	1	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	400.41	Opt	0.061	400.42	0.01	3E-05
5	1	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	435.7	Opt	0.06	435.71	0	3E-05
5	1	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	393.51	Opt	0.06	393.57	0.01	0.0001
5	1	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	423.78	Opt	0.06	423.78	0	0
5	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.45	Opt	0.05	379.47	0	4E-05
5	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	357.26	Opt	0.06	357.26	0	0
5	1	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	472.22	Opt	0.05	472.24	0	4E-05
5	1	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	474.73	Opt	0.05	474.73	0	0
5	1	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
5	1	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	472.42	Opt	0.06	472.42	0	0
5	1	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	512.54	Opt	0.04	512.54	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
5	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	294.39	Opt	0.06	299.72	0	0.0181
5	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	380.41	Opt	0.061	380.51	0.01	0.0003
5	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	271.54	Opt	0.05	271.65	0	0.0004
5	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	322.53	Opt	0.05	322.53	0	0
5	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	399.34	Opt	0.07	400.29	0	0.0024
5	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	435.29	Opt	0.15	436.11	0	0.0019
5	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	391.94	Opt	0.21	392.2	0.01	0.0007
5	1	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	422.82	Opt	0.241	423.08	0	0.0006
5	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.55	Opt	0.06	379.55	0	0
5	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	356.61	Opt	0.06	356.61	0	0
5	1	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	472.7	Opt	0.06	472.7	0	1E-05
5	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	474.5	Opt	0.06	475.04	0	0.0011
5	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	471.97	Opt	0.08	472.19	0	0.0005
5	1	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	513.14	Opt	0.04	513.14	0	0
5	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	295.05	Opt	0.06	300.09	0	0.0171
5	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	1	23	26	380.76	Opt	0.06	380.77	0	3E-05
5	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	272.7	Opt	0.05	272.7	0	0
5	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	323.4	Opt	0.051	323.4	0	0
5	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	400.97	Opt	0.05	401.19	0.01	0.0006
5	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	436.66	Opt	0.06	436.85	0	0.0004
5	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	393.73	Opt	0.06	393.77	0	9E-05
5	1	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	424.42	Opt	0.06	424.46	0.01	9E-05
5	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.75	Opt	0.05	379.75	0	0
5	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	357.21	Opt	0.06	357.21	0	0
5	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	472.91	Opt	0.05	472.91	0.01	0
5	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	475.31	Opt	0.05	475.43	0	0.0003
5	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	472.87	Opt	0.06	472.9	0	6E-05
5	1	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	513.56	Opt	0.05	513.56	0	0
5	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	295.52	Opt	0.061	300.46	0	0.0167
5	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	381.03	Opt	0.06	381.03	0	0
5	1	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	273.75	Opt	0.05	273.75	0.01	0
5	1	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	324.28	Opt	0.05	324.28	0.01	0
5	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	402.1	Opt	0.06	402.1	0	0
5	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	437.59	Opt	0.06	437.59	0	1E-05
5	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	395.34	Opt	0.06	395.34	0	0
5	1	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	425.81	Opt	0.06	425.81	0	0
5	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	379.95	Opt	0.06	379.95	0	0
5	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	357.82	Opt	0.05	357.82	0	0
5	1	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	473.12	Opt	0.05	473.12	0	1E-05
5	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	475.81	Opt	0.061	475.82	0	2E-05
5	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
5	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	473.61	Opt	0.06	473.61	0	0
5	1	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	513.98	Opt	0.04	513.98	0.01	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	2	38	10	580	Opt	0.05	590	0	0.0172
10	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	750	Opt	0.06	750	0	0
10	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	530	Opt	0.06	530	0	0
10	0	0	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	630	Opt	0.06	630	0	0
10	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	2	18	30	780	Opt	0.05	780	0	0
10	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	2	11	37	850	Opt	0.05	850	0	0
10	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	760	Opt	0.05	760	0	0
10	0	0	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	820	Opt	0.06	820	0	0
10	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750	Opt	0.06	750	0	0
10	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	700	Opt	0.061	700	0	0
10	0	0	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0.01,0.02]	0	7	43	930	Opt	0.05	930	0.01	0
10	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	1	5	44	930	Opt	0.05	930	0	0
10	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	920	Opt	0.06	920	0	0
10	0	0	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1000	Opt	0.04	1000	0	0
10	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	580.42	Opt	0.06	590.37	0	0.0171
10	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	750.24	Opt	0.06	750.26	0.01	2E-05
10	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	531.05	Opt	0.05	531.05	0.01	0
10	0	0	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	630.88	Opt	0.05	630.88	0	0
10	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	780.89	Opt	0.06	780.9	0.01	1E-05
10	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	850.73	Opt	0.06	850.74	0	1E-05
10	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	761.57	Opt	0.061	761.57	0	0
10	0	0	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	821.35	Opt	0.06	821.35	0	0
10	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.19	Opt	0.06	750.2	0	2E-05
10	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	700.6	Opt	0.05	700.6	0	0
10	0	0	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	930.2	Opt	0.05	930.21	0.01	2E-05
10	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	930.37	Opt	0.06	930.39	0	2E-05
10	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	920.71	Opt	0.05	920.71	0	0
10	0	0	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1000.4	Opt	0.05	1000.4	0	0
10	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	580.84	Opt	0.06	590.74	0	0.017
10	0	0	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	750.48	Opt	0.06	750.52	0	5E-05
10	0	0	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	532.1	Opt	0.05	532.1	0	0
10	0	0	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	631.76	Opt	0.061	631.76	0	0
10	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	781.79	Opt	0.06	781.81	0	3E-05
10	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	851.46	Opt	0.06	851.48	0	2E-05
10	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	763.14	Opt	0.06	763.14	0	0
10	0	0	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	822.7	Opt	0.06	822.7	0	0
10	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.38	Opt	0.06	750.41	0	3E-05
10	0	0	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	0	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	701.21	Opt	0.06	701.21	0	0
10	0	0	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	930.39	Opt	0.06	930.42	0	3E-05
10	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	930.78	Opt	0.06	930.78	0	0
10	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	921.42	Opt	0.06	921.42	0	0
10	0	0	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1000.8	Opt	0.04	1000.8	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	580.66	Opt	0.051	590.77	0	0.0174
10	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	750.95	Opt	0.06	750.98	0.01	4E-05
10	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	530.9	Opt	0.05	530.9	0.01	0
10	0	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	631.15	Opt	0.05	631.15	0	0
10	0	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	781.21	Opt	0.06	781.68	0	0.0006
10	0	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	851.48	Opt	0.06	851.88	0	0.0005
10	0	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	761.68	Opt	0.06	761.77	0	0.0001
10	0	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	1	16	33	821.92	Opt	0.07	822.02	0	0.0001
10	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.48	Opt	0.06	750.48	0	0
10	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	700.56	Opt	0.05	700.56	0	0
10	0	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	930.88	Opt	0.05	930.88	0	0
10	0	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	930.83	Opt	0.061	931.08	0	0.0003
10	0	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	921.11	Opt	0.06	921.19	0	9E-05
10	0	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1001.4	Opt	0.04	1001.4	0	0
10	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	581.19	Opt	0.05	591.14	0.01	0.0171
10	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	751.24	Opt	0.06	751.24	0	0
10	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	531.94	Opt	0.06	531.94	0	0
10	0	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	632.03	Opt	0.06	632.03	0	0
10	0	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	2	18	30	782.65	Opt	0.06	782.58	0	-9E-05
10	0	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	852.62	Opt	0.06	852.62	0.01	1E-06
10	0	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	763.34	Opt	0.06	763.34	0	0
10	0	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	823.37	Opt	0.06	823.37	0	0
10	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.69	Opt	0.05	750.69	0	0
10	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	701.16	Opt	0.06	701.16	0	0
10	0	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	931.09	Opt	0.06	931.09	0	2E-06
10	0	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	1	5	44	931.52	Opt	0.06	931.48	0	-5E-05
10	0	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	921.9	Opt	0.06	921.9	0	0
10	0	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1001.9	Opt	0.05	1001.9	0	0
10	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	581.61	Opt	0.06	591.51	0	0.017
10	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	751.49	Opt	0.06	751.49	0	0
10	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	532.99	Opt	0.06	532.99	0	0
10	0	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	632.9	Opt	0.06	632.9	0	0
10	0	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	783.48	Opt	0.06	783.48	0	5E-06
10	0	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	853.35	Opt	0.06	853.36	0.01	2E-05
10	0	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	764.91	Opt	0.061	764.91	0	0
10	0	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	824.73	Opt	0.06	824.73	0	0
10	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.88	Opt	0.05	750.89	0	1E-05
10	0	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	0	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	701.77	Opt	0.06	701.77	0	0
10	0	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	931.29	Opt	0.06	931.3	0	2E-05
10	0	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	931.85	Opt	0.06	931.86	0.01	2E-05
10	0	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
10	0	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	922.61	Opt	0.05	922.61	0.01	0
10	0	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1002.3	Opt	0.04	1002.3	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	581.24	Opt	0.05	591.54	0.01	0.0177
10	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	751.89	Opt	0.06	751.96	0	8E-05
10	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	531.7	Opt	0.061	531.79	0	0.0002
10	0	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	632.3	Opt	0.05	632.3	0	0
10	0	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	782.43	Opt	0.05	783.35	0.01	0.0012
10	0	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	852.97	Opt	0.06	853.76	0	0.0009
10	0	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	763.32	Opt	0.16	763.54	0	0.0003
10	0	2	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	1	16	33	823.81	Opt	0.18	824.05	0.01	0.0003
10	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	750.97	Opt	0.06	750.97	0	0
10	0	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	701.12	Opt	0.05	701.12	0	0
10	0	2	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	931.77	Opt	0.051	931.77	0	0
10	0	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	931.65	Opt	0.05	932.17	0.01	0.0006
10	0	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0.01	0
10	0	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	922.21	Opt	0.06	922.38	0	0.0002
10	0	2	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1002.9	Opt	0.04	1002.9	0.01	0
10	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	581.9	Opt	0.05	591.91	0	0.0172
10	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	752.21	Opt	0.06	752.21	0	3E-06
10	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	532.84	Opt	0.06	532.84	0	0
10	0	2	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	37	13	633.18	Opt	0.06	633.18	0	0
10	0	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	784.04	Opt	0.06	784.26	0	0.0003
10	0	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	854.32	Opt	0.05	854.5	0.01	0.0002
10	0	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	765.11	Opt	0.06	765.11	0	0
10	0	2	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	825.4	Opt	0.061	825.4	0.01	0
10	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	751.17	Opt	0.05	751.17	0.01	0
10	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
10	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	701.72	Opt	0.05	701.72	0	0
10	0	2	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	931.98	Opt	0.05	931.98	0	0
10	0	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	932.46	Opt	0.05	932.56	0	0.0001
10	0	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	923.09	Opt	0.06	923.09	0	0
10	0	2	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1003.3	Opt	0.05	1003.3	0	0
10	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	582.37	Opt	0.06	592.28	0	0.017
10	0	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	752.47	Opt	0.07	752.47	0	0
10	0	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	533.89	Opt	0.05	533.89	0.01	0
10	0	2	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	37	13	634.05	Opt	0.06	634.05	0	0
10	0	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	785.16	Opt	0.071	785.16	0	0
10	0	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	855.24	Opt	0.07	855.24	0	4E-06
10	0	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	766.68	Opt	0.06	766.68	0	0
10	0	2	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	18	32	826.75	Opt	0.07	826.75	0	0
10	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	751.37	Opt	0.06	751.37	0.01	0
10	0	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0.01	0
10	0	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	702.33	Opt	0.06	702.33	0.01	0
10	0	2	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01,0.02]	0	7	43	932.18	Opt	0.07	932.19	0	5E-06
10	0	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	932.95	Opt	0.07	932.96	0	1E-05
10	0	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	923.8	Opt	0.06	923.8	0	0
10	0	2	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01,0.02]	0	0	50	1003.7	Opt	0.051	1003.7	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	582.23	Opt	0.07	592.36	0	0.0174
10	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	752.72	Opt	0.07	752.76	0.01	5E-05
10	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	533.27	Opt	0.07	533.32	0	1E-04
10	0.5	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	633.76	Opt	0.07	633.76	0	0
10	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	784.68	Opt	0.06	785.15	0.01	0.0006
10	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	4	7	39	855.15	Opt	0.07	855.55	0	0.0005
10	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	22	27	765.99	Opt	0.07	766.1	0	0.0001
10	0.5	1	0	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	1	16	33	826.43	Opt	0.07	826.55	0	0.0001
10	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	752.27	Opt	0.06	752.27	0	0
10	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	703.31	Opt	0.061	703.31	0	0
10	0.5	1	0	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	933.85	Opt	0.06	933.85	0	4E-06
10	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	934.75	Opt	0.06	935.02	0.01	0.0003
10	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0.01	0
10	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	1	6	43	926	Opt	0.06	926.1	0	0.0001
10	0.5	1	0	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1006.6	Opt	0.05	1006.6	0	0
10	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	582.76	Opt	0.06	592.73	0	0.0171
10	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	753.01	Opt	0.06	753.01	0.01	0
10	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	534.37	Opt	0.06	534.37	0	0
10	0.5	1	1.5	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	634.64	Opt	0.06	634.64	0	0
10	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	2	18	30	786.13	Opt	0.06	786.05	0	-1E-04
10	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	856.29	Opt	0.06	856.3	0.01	2E-06
10	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	767.67	Opt	0.061	767.67	0.01	0
10	0.5	1	1.5	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	827.9	Opt	0.06	827.9	0	0
10	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	752.48	Opt	0.06	752.48	0	0
10	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	703.91	Opt	0.06	703.91	0	0
10	0.5	1	1.5	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	934.06	Opt	0.05	934.06	0.01	4E-06
10	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	1	5	44	935.46	Opt	0.06	935.41	0	-5E-05
10	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	926.8	Opt	0.06	926.8	0	0
10	0.5	1	1.5	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1007	Opt	0.04	1007	0.01	0
10	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	583.19	Opt	0.06	593.1	0	0.017
10	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	0	25	25	753.25	Opt	0.06	753.27	0.01	2E-05
10	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	47	3	535.42	Opt	0.061	535.42	0	0
10	0.5	1	3	0.75	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	37	13	635.52	Opt	0.06	635.52	0	0
10	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	786.94	Opt	0.06	786.95	0.01	1E-05
10	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	0	15	35	857.02	Opt	0.06	857.04	0	2E-05
10	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	24	26	769.24	Opt	0.06	769.24	0	0
10	0.5	1	3	0.75	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	18	32	829.26	Opt	0.06	829.26	0	0
10	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	752.66	Opt	0.06	752.68	0	2E-05
10	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0,0.01]	0	30	20	704.51	Opt	0.06	704.51	0	0
10	0.5	1	3	0.85	[0,0.05]	[0,0.05]	[0.05,0.1]	[0.01,0.02]	0	7	43	934.25	Opt	0.06	934.27	0	2E-05
10	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	935.78	Opt	0.06	935.8	0.01	2E-05
10	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0,0.05]	[0.01,0.02]	50	0	0	0	Inf	0.01	0	0.01	0
10	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0,0.01]	0	8	42	927.51	Opt	0.06	927.51	0	0
10	0.5	1	3	0.85	[0.05,0.1]	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	0	0	50	1007.4	Opt	0.041	1007.4	0.01	0



Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	582.82	Opt	0.06	593.13	0	0.0177
10	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	753.67	Opt	0.07	753.73	0	9E-05
10	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	534.12	Opt	0.06	534.22	0	0.0002
10	0.5	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	634.91	Opt	0.06	634.91	0	0
10	0.5	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	785.89	Opt	0.06	786.82	0.01	0.0012
10	0.5	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	856.63	Opt	0.07	857.43	0	0.0009
10	0.5	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	767.63	Opt	0.2	767.87	0	0.0003
10	0.5	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	828.32	Opt	0.211	828.57	0	0.0003
10	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	752.76	Opt	0.06	752.76	0	0
10	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	703.87	Opt	0.06	703.87	0	0
10	0.5	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	934.73	Opt	0.06	934.74	0	6E-06
10	0.5	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	935.58	Opt	0.06	936.1	0	0.0006
10	0.5	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	927.1	Opt	0.06	927.29	0.01	0.0002
10	0.5	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1008	Opt	0.04	1008	0.01	0
10	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	583.47	Opt	0.06	593.5	0	0.0172
10	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	753.98	Opt	0.07	753.99	0	1E-05
10	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	535.27	Opt	0.061	535.27	0	0
10	0.5	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	635.79	Opt	0.06	635.79	0	0
10	0.5	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	787.5	Opt	0.07	787.72	0	0.0003
10	0.5	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	857.99	Opt	0.06	858.17	0.01	0.0002
10	0.5	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	769.41	Opt	0.09	769.44	0	3E-05
10	0.5	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	829.9	Opt	0.07	829.93	0.01	3E-05
10	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	752.96	Opt	0.06	752.96	0.01	0
10	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0.01	0
10	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	704.47	Opt	0.06	704.47	0	0
10	0.5	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	934.94	Opt	0.06	934.94	0.01	0
10	0.5	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	936.39	Opt	0.061	936.5	0	0.0001
10	0.5	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	927.99	Opt	0.07	927.99	0	0
10	0.5	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1008.4	Opt	0.06	1008.4	0	0
10	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	583.95	Opt	0.06	593.87	0	0.017
10	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	754.25	Opt	0.07	754.25	0	0
10	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	536.32	Opt	0.06	536.32	0	0
10	0.5	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	636.67	Opt	0.06	636.67	0.01	0
10	0.5	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	788.63	Opt	0.07	788.63	0	0
10	0.5	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	858.91	Opt	0.06	858.92	0.01	5E-06
10	0.5	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	771.01	Opt	0.06	771.01	0	0
10	0.5	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	831.28	Opt	0.061	831.28	0.01	0
10	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	753.16	Opt	0.06	753.16	0	0
10	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	705.07	Opt	0.06	705.07	0	0
10	0.5	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	935.15	Opt	0.06	935.15	0	6E-06
10	0.5	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	936.88	Opt	0.06	936.89	0.01	1E-05
10	0.5	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0.01	0
10	0.5	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	928.7	Opt	0.07	928.7	0	0
10	0.5	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1008.8	Opt	0.06	1008.8	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	583.81	Opt	0.07	593.95	0	0.0174
10	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	754.49	Opt	0.07	754.53	0	5E-05
10	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	535.69	Opt	0.06	535.75	0	0.0001
10	1	1	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	636.38	Opt	0.061	636.38	0	0
10	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	788.14	Opt	0.07	788.61	0	0.0006
10	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	858.82	Opt	0.07	859.23	0	0.0005
10	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	770.3	Opt	0.08	770.43	0	0.0002
10	1	1	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	830.95	Opt	0.07	831.08	0.01	0.0002
10	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.06	Opt	0.06	754.06	0	3E-06
10	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	706.05	Opt	0.06	706.05	0	0
10	1	1	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	936.82	Opt	0.06	936.82	0.01	5E-06
10	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	938.68	Opt	0.06	938.95	0	0.0003
10	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	930.89	Opt	0.07	931	0	0.0001
10	1	1	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1011.7	Opt	0.04	1011.7	0	0
10	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	584.34	Opt	0.08	594.32	0	0.0171
10	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	754.79	Opt	0.07	754.79	0	8E-06
10	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	536.8	Opt	0.06	536.8	0	0
10	1	1	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	637.25	Opt	0.06	637.25	0	0
10	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	789.51	Opt	0.06	789.52	0.01	5E-06
10	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	859.97	Opt	0.06	859.97	0.01	3E-06
10	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	772	Opt	0.06	772	0	0
10	1	1	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	832.43	Opt	0.06	832.43	0	0
10	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.26	Opt	0.07	754.26	0	5E-06
10	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	706.65	Opt	0.061	706.65	0	0
10	1	1	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	937.03	Opt	0.06	937.03	0.01	4E-06
10	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	1	5	44	939.39	Opt	0.06	939.35	0	-5E-05
10	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	931.71	Opt	0.06	931.71	0	0
10	1	1	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1012.1	Opt	0.04	1012.1	0	0
10	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	584.76	Opt	0.09	594.69	0	0.017
10	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	755.03	Opt	0.351	755.05	0	3E-05
10	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	537.85	Opt	0.06	537.85	0	0
10	1	1	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	638.13	Opt	0.06	638.13	0	0
10	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	790.41	Opt	0.07	790.42	0	2E-05
10	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	860.7	Opt	0.07	860.71	0	2E-05
10	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	773.57	Opt	0.06	773.57	0	0
10	1	1	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	833.78	Opt	0.06	833.78	0	0
10	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.45	Opt	0.05	754.47	0	2E-05
10	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	707.26	Opt	0.05	707.26	0.01	0
10	1	1	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	937.22	Opt	0.05	937.24	0	2E-05
10	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	939.71	Opt	0.071	939.73	0	2E-05
10	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	932.42	Opt	0.05	932.42	0.01	0
10	1	1	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1012.5	Opt	0.04	1012.5	0	0

Input Parameters									Output								
$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1$	$d_2$	$d_0$	$d_{-1}$	(0,0)	(1,0)	(1,1)	Opt obj	Status	Opt sol time	H obj	H sol time	H-Opt gap
10	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	5	32	13	584.39	Opt	0.05	594.72	0	0.0177
10	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	755.44	Opt	0.07	755.51	0	9E-05
10	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	1	45	4	536.54	Opt	0.06	536.65	0	0.0002
10	1	2	0	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	637.53	Opt	0.05	637.53	0	0
10	1	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	789.35	Opt	0.05	790.29	0	0.0012
10	1	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	860.3	Opt	0.06	861.11	0	0.0009
10	1	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	771.94	Opt	0.19	772.2	0	0.0003
10	1	2	0	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	832.83	Opt	0.181	833.1	0	0.0003
10	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.55	Opt	0.07	754.55	0	0
10	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.03	0	0	0
10	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	706.61	Opt	0.06	706.61	0.01	0
10	1	2	0	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	937.7	Opt	0.07	937.7	0	7E-06
10	1	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	939.5	Opt	0.08	940.04	0	0.0006
10	1	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	931.99	Opt	0.08	932.19	0	0.0002
10	1	2	0	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1013.1	Opt	0.06	1013.1	0	0
10	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	4	34	12	585.05	Opt	0.061	595.09	0	0.0172
10	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	1	23	26	755.76	Opt	0.07	755.77	0	2E-05
10	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	537.7	Opt	0.06	537.7	0	0
10	1	2	1.5	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	638.4	Opt	0.06	638.4	0	0
10	1	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	5	12	33	790.97	Opt	0.06	791.19	0	0.0003
10	1	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	4	7	39	861.66	Opt	0.07	861.85	0	0.0002
10	1	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	22	27	773.73	Opt	0.07	773.77	0	5E-05
10	1	2	1.5	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	1	16	33	834.42	Opt	0.07	834.46	0	5E-05
10	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.75	Opt	0.06	754.75	0	0
10	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	707.21	Opt	0.07	707.21	0	0
10	1	2	1.5	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	937.91	Opt	0.061	937.91	0	0
10	1	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	3	1	46	940.31	Opt	0.06	940.43	0	0.0001
10	1	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.01	0	0	0
10	1	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	1	6	43	932.87	Opt	0.06	932.9	0	3E-05
10	1	2	1.5	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1013.6	Opt	0.05	1013.6	0	0
10	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	1	40	9	585.52	Opt	0.06	595.46	0.01	0.017
10	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	0	25	25	756.03	Opt	0.06	756.03	0.01	0
10	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	47	3	538.75	Opt	0.06	538.75	0	0
10	1	2	3	0.75	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	37	13	639.28	Opt	0.06	639.28	0	0
10	1	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	22	28	792.1	Opt	0.07	792.1	0	0
10	1	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	0	15	35	862.59	Opt	0.07	862.59	0	7E-06
10	1	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	24	26	775.34	Opt	0.07	775.34	0	0
10	1	2	3	0.75	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	18	32	835.81	Opt	0.061	835.81	0	0
10	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01]	0	25	25	754.95	Opt	0.06	754.95	0	0
10	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.02	0	0	0
10	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01]	0	30	20	707.82	Opt	0.06	707.82	0	0
10	1	2	3	0.85	[0,0.05]	[0,0.05]	[0,0.05,0.1]	[0,0.01,0.02]	0	7	43	938.12	Opt	0.07	938.12	0	7E-06
10	1	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01]	0	7	43	940.81	Opt	0.07	940.83	0	1E-05
10	1	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05]	[0,0.01,0.02]	50	0	0	0	Inf	0.03	0	0	0
10	1	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01]	0	8	42	933.61	Opt	0.07	933.61	0	0
10	1	2	3	0.85	[0.05,0.1]	[0,0.05,0.1]	[0,0.05,0.1]	[0,0.01,0.02]	0	0	50	1014	Opt	0.06	1014	0	0

## Appendix I – Results for Multiple Pool Inventory Sharing with Dedicated Facilities

Exp #	Input Parameters										
	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
2	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
3	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
4	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
5	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
6	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
7	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
8	10	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
9	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
10	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
11	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
12	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
13	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
14	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
15	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
16	10	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
17	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
18	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
19	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
20	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
21	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
22	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
23	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
24	10	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
25	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
26	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
27	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
28	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
29	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
30	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
31	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
32	10	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
33	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
34	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
35	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
36	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
37	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
38	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
39	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
40	10	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
41	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
42	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
43	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
44	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
45	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
46	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
47	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
48	10	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1	0	10	0	0	105.1	0.7148	Opt	0.17	0	10	0	0	105.1	0.7148	0.01	0
2	0	10	0	0	105.1	0.714	Opt	0.201	0	10	0	3	109.6	0.7017	0.01	0.04283
3	0	8	2	0	126.1	0.7048	Opt	0.08	0	8	2	0	126.1	0.7048	0	0
4	0	8	2	0	126.1	0.7059	Opt	0.09	0	7	3	0	136.6	0.7144	0.01	0.08325
5	1	9	0	0	94.73	0.7276	Opt	0.08	1	9	0	0	94.73	0.7276	0	2.3E-05
6	1	9	0	0	94.74	0.7231	Opt	0.07	1	9	0	0	94.74	0.7111	0.01	3.6E-05
7	0	10	0	0	105.1	0.7378	Opt	0.09	0	10	0	0	105.1	0.7378	0.01	0
8	0	10	0	0	105.1	0.7358	Opt	0.08	0	10	0	0	105.1	0.7242	0.01	1.9E-05
9	0	7	3	0	136.6	0.7084	Opt	0.091	0	7	3	0	136.6	0.7084	0.01	0
10	0	7	3	0	136.7	0.7088	Opt	0.1	0	7	3	1	138.2	0.7005	0	0.01098
11	0	6	4	0	147.2	0.7106	Opt	0.09	0	6	4	0	147.2	0.7106	0	0
12	0	6	4	0	147.2	0.7105	Opt	0.11	0	6	4	0	147.2	0.7016	0.01	6.8E-06
13	0	8	2	0	126.2	0.7188	Opt	0.09	0	8	2	0	126.2	0.7188	0	0
14	0	8	2	0	126.2	0.7182	Opt	0.1	0	8	2	0	126.2	0.7105	0	1.6E-05
15	0	7	3	0	136.7	0.7222	Opt	0.1	0	7	3	0	136.7	0.7222	0	0
16	0	7	3	0	136.7	0.7218	Opt	0.141	0	7	3	0	136.7	0.7144	0.01	1.5E-05
17	0	9	1	0	115.6	0.7515	Opt	0.09	0	9	1	0	115.6	0.7515	0	0
18	0	9	1	1	117.1	0.7514	Opt	0.1	0	8	2	0	126.1	0.7577	0.01	0.07685
19	0	6	4	0	147.1	0.7541	Opt	0.09	0	6	4	0	147.1	0.7541	0	0
20	0	6	4	0	147.1	0.7539	Opt	0.09	0	5	5	0	157.6	0.7593	0.01	0.07138
21	0	10	0	0	105.1	0.7911	Opt	0.1	0	10	0	0	105.1	0.7911	0	0
22	0	10	0	0	105.1	0.7871	Opt	0.09	0	10	0	0	105.1	0.774	0	1.9E-05
23	0	9	1	0	115.6	0.7631	Opt	0.091	0	9	1	0	115.6	0.7631	0	0
24	0	9	1	0	115.6	0.7608	Opt	0.12	0	9	1	2	118.6	0.7507	0.01	0.02595
25	0	6	4	0	147.1	0.7508	Opt	0.09	0	6	4	0	147.1	0.7508	0	0
26	0	6	4	1	148.6	0.7503	Opt	0.1	0	5	5	0	157.6	0.7757	0	0.06049
27	0	4	6	0	168.1	0.7809	Opt	6.86	0	4	6	0	168.1	0.7809	0.01	0
28	0	5	5	5	165.1	0.7501	Opt	0.32	0	4	6	0	168.1	0.7691	0	0.01812
29	0	7	3	0	136.7	0.755	Opt	0.091	0	7	3	0	136.7	0.755	0	0
30	0	7	3	0	136.7	0.7539	Opt	0.09	0	6	4	0	147.2	0.7795	0.01	0.07671
31	0	6	4	0	147.2	0.7558	Opt	0.09	0	6	4	0	147.2	0.7558	0	0
32	0	6	4	0	147.2	0.7544	Opt	0.09	0	5	5	0	157.7	0.7753	0.01	0.07124
33	0	10	0	0	105.1	0.7148	Opt	0.1	0	10	0	0	105.1	0.7148	0	0
34	0	10	0	0	105.1	0.714	Opt	0.14	0	10	0	3	109.6	0.7017	0	0.04282
35	0	8	2	0	126.1	0.7048	Opt	0.09	0	8	2	0	126.1	0.7048	0	0
36	0	8	2	0	126.1	0.7059	Opt	0.101	0	7	3	0	136.6	0.7144	0	0.08321
37	1	9	0	0	94.89	0.7276	Opt	0.09	1	9	0	0	94.89	0.7276	0	4.6E-05
38	1	9	0	0	94.91	0.7231	Opt	0.09	1	9	0	0	94.91	0.7111	0	7.1E-05
39	0	10	0	0	105.2	0.7378	Opt	0.09	0	10	0	0	105.2	0.7378	0.01	0
40	0	10	0	0	105.2	0.7358	Opt	0.09	0	10	0	0	105.2	0.7242	0.01	2.9E-05
41	0	7	3	0	136.7	0.7084	Opt	0.1	0	7	3	0	136.7	0.7084	0	0
42	0	7	3	0	136.7	0.7088	Opt	0.1	0	7	3	1	138.2	0.7005	0.01	0.01099
43	0	6	4	0	147.2	0.7106	Opt	0.091	0	6	4	0	147.2	0.7106	0.01	0
44	0	6	4	0	147.2	0.7105	Opt	0.13	0	6	4	0	147.2	0.7016	0	1.4E-05
45	0	8	2	0	126.3	0.7188	Opt	0.1	0	8	2	0	126.3	0.7188	0	0
46	0	8	2	0	126.3	0.7182	Opt	0.09	0	8	2	0	126.3	0.7105	0	3.2E-05
47	0	7	3	0	136.8	0.7222	Opt	0.1	0	7	3	0	136.8	0.7222	0.01	0
48	0	7	3	0	136.8	0.7218	Opt	0.11	0	7	3	0	136.8	0.7144	0.01	2.9E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
49	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
50	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
51	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
52	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
53	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
54	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
55	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
56	10	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
57	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
58	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
59	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
60	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
61	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
62	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
63	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
64	10	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
65	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
66	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
67	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
68	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
69	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
70	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
71	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
72	10	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
73	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
74	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
75	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
76	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
77	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
78	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
79	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
80	10	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
81	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
82	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
83	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
84	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
85	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
86	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
87	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
88	10	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
89	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
90	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
91	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
92	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
93	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
94	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
95	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
96	10	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
49	0	9	1	0	115.6	0.7515	Opt	0.101	0	9	1	0	115.6	0.7515	0	0
50	0	9	1	1	117.1	0.7514	Opt	0.11	0	8	2	0	126.1	0.7577	0	0.07681
51	0	6	4	0	147.1	0.7541	Opt	0.09	0	6	4	0	147.1	0.7541	0	0
52	0	6	4	0	147.1	0.7539	Opt	0.1	0	5	5	0	157.6	0.7593	0	0.07137
53	0	10	0	0	105.2	0.7911	Opt	0.1	0	10	0	0	105.2	0.7911	0	0
54	0	10	0	0	105.2	0.7871	Opt	0.09	0	10	0	0	105.2	0.774	0.01	3.8E-05
55	0	9	1	0	115.7	0.7631	Opt	0.09	0	9	1	0	115.7	0.7631	0.01	0
56	0	9	1	0	115.7	0.7608	Opt	0.111	0	9	1	2	118.7	0.7507	0.01	0.02596
57	0	6	4	0	147.2	0.7508	Opt	0.09	0	6	4	0	147.2	0.7508	0.01	0
58	0	6	4	1	148.7	0.7503	Opt	0.11	0	5	5	0	157.7	0.7757	0	0.06042
59	0	4	6	0	168.2	0.7809	Opt	0.441	0	4	6	0	168.2	0.7809	0.01	0
60	0	5	5	5	165.2	0.75	Opt	1.962	0	4	6	0	168.2	0.7691	0	0.01807
61	0	7	3	0	136.8	0.755	Opt	0.09	0	7	3	0	136.8	0.755	0.01	0
62	0	7	3	0	136.8	0.7539	Opt	0.091	0	6	4	0	147.3	0.7795	0	0.07658
63	0	6	4	0	147.3	0.7558	Opt	0.1	0	6	4	0	147.3	0.7558	0.01	0
64	0	6	4	0	147.3	0.7544	Opt	0.1	0	5	5	0	157.8	0.7753	0	0.07111
65	0	10	0	0	105.1	0.7148	Opt	0.1	0	10	0	0	105.1	0.7148	0	0
66	0	10	0	0	105.1	0.714	Opt	0.17	0	10	0	3	109.6	0.7017	0	0.04282
67	0	8	2	0	126.1	0.7048	Opt	0.1	0	8	2	0	126.1	0.7048	0	0
68	0	8	2	0	126.1	0.7059	Opt	0.101	0	7	3	0	136.6	0.7144	0	0.08322
69	1	9	0	0	94.75	0.7276	Opt	0.09	1	9	0	0	94.75	0.7276	0.01	2.3E-05
70	1	9	0	0	94.76	0.7231	Opt	0.1	1	9	0	0	94.76	0.7111	0	3.6E-05
71	0	10	0	0	105.2	0.7378	Opt	0.1	0	10	0	0	105.2	0.7378	0	0
72	0	10	0	0	105.2	0.7358	Opt	0.1	0	10	0	0	105.2	0.7242	0.01	1.9E-05
73	0	7	3	0	136.7	0.7084	Opt	0.11	0	7	3	0	136.7	0.7084	0.01	0
74	0	7	3	0	136.7	0.7088	Opt	0.1	0	7	3	1	138.2	0.7005	0.01	0.01098
75	0	6	4	0	147.2	0.7106	Opt	0.11	0	6	4	0	147.2	0.7106	0.011	0
76	0	6	4	0	147.2	0.7105	Opt	0.1	0	6	4	0	147.2	0.7016	0.01	6.8E-06
77	0	8	2	0	126.3	0.7188	Opt	0.1	0	8	2	0	126.3	0.7188	0.01	0
78	0	8	2	0	126.3	0.7182	Opt	0.1	0	8	2	0	126.3	0.7105	0	1.6E-05
79	0	7	3	0	136.8	0.7222	Opt	0.1	0	7	3	0	136.8	0.7222	0.01	0
80	0	7	3	0	136.8	0.7218	Opt	0.141	0	7	3	0	136.8	0.7144	0.01	1.5E-05
81	0	9	1	0	115.6	0.7515	Opt	0.1	0	9	1	0	115.6	0.7515	0	0
82	0	9	1	1	117.1	0.7514	Opt	0.11	0	8	2	0	126.1	0.7577	0	0.07682
83	0	6	4	0	147.1	0.7541	Opt	0.09	0	6	4	0	147.1	0.7541	0.01	0
84	0	6	4	0	147.1	0.7539	Opt	0.1	0	5	5	0	157.6	0.7593	0	0.07136
85	0	10	0	0	105.1	0.7911	Opt	0.09	0	10	0	0	105.1	0.7911	0.01	0
86	0	10	0	0	105.2	0.7871	Opt	0.1	0	10	0	0	105.2	0.774	0.01	9.5E-06
87	0	9	1	0	115.7	0.7631	Opt	0.101	0	9	1	0	115.7	0.7631	0	0
88	0	9	1	0	115.7	0.7608	Opt	0.12	0	9	1	2	118.7	0.7507	0.01	0.02595
89	0	6	4	0	147.2	0.7508	Opt	0.09	0	6	4	0	147.2	0.7508	0	0
90	0	6	4	1	148.7	0.7503	Opt	0.11	0	5	5	0	157.7	0.7757	0.01	0.06044
91	0	4	6	0	168.2	0.7809	Opt	0.981	0	4	6	0	168.2	0.7809	0.01	0
92	0	5	5	5	165.2	0.7501	Opt	0.641	0	4	6	0	168.2	0.7691	0	0.01809
93	0	7	3	0	136.7	0.755	Opt	0.101	0	7	3	0	136.7	0.755	0	0
94	0	7	3	0	136.7	0.7539	Opt	0.1	0	6	4	0	147.2	0.7795	0	0.07665
95	0	6	4	0	147.2	0.7558	Opt	0.1	0	6	4	0	147.2	0.7558	0.01	0
96	0	6	4	0	147.2	0.7544	Opt	0.1	0	5	5	0	157.7	0.7753	0.01	0.07119

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
97	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
98	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
99	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
100	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
101	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
102	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
103	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
104	10	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
105	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
106	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
107	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
108	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
109	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
110	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
111	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
112	10	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
113	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
114	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
115	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
116	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
117	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
118	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
119	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
120	10	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
121	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
122	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
123	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
124	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
125	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
126	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
127	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
128	10	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
129	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
130	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
131	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
132	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
133	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
134	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
135	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
136	10	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
137	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
138	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
139	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
140	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
141	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
142	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
143	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
144	10	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
97	0	10	0	0	105.1	0.7148	Opt	0.1	0	10	0	0	105.1	0.7148	0	0
98	0	10	0	0	105.1	0.714	Opt	0.13	0	10	0	3	109.6	0.7017	0.01	0.04281
99	0	8	2	0	126.1	0.7048	Opt	0.1	0	8	2	0	126.1	0.7048	0	0
100	0	8	2	0	126.1	0.7059	Opt	0.111	0	7	3	0	136.6	0.7144	0	0.08318
101	1	9	0	0	94.91	0.7276	Opt	0.1	1	9	0	0	94.91	0.7276	0	4.6E-05
102	1	9	0	0	94.93	0.7231	Opt	0.1	1	9	0	0	94.92	0.7111	0.01	7.1E-05
103	0	10	0	0	105.2	0.7378	Opt	0.1	0	10	0	0	105.2	0.7378	0	0
104	0	10	0	0	105.2	0.7358	Opt	0.11	0	10	0	0	105.2	0.7242	0	2.9E-05
105	0	7	3	0	136.7	0.7084	Opt	0.1	0	7	3	0	136.7	0.7084	0	0
106	0	7	3	0	136.7	0.7088	Opt	0.111	0	7	3	1	138.2	0.7005	0	0.01098
107	0	6	4	0	147.2	0.7106	Opt	0.1	0	6	4	0	147.2	0.7106	0	0
108	0	6	4	0	147.2	0.7105	Opt	0.13	0	6	4	0	147.2	0.7016	0	2E-05
109	0	8	2	0	126.4	0.7188	Opt	0.1	0	8	2	0	126.4	0.7188	0	0
110	0	8	2	0	126.4	0.7182	Opt	0.11	0	8	2	0	126.4	0.7105	0.01	3.2E-05
111	0	7	3	0	136.8	0.7222	Opt	0.11	0	7	3	0	136.8	0.7222	0.01	0
112	0	7	3	0	136.9	0.7218	Opt	0.141	0	7	3	0	136.9	0.7144	0	2.2E-05
113	0	9	1	0	115.6	0.7515	Opt	0.1	0	9	1	0	115.6	0.7515	0	0
114	0	9	1	1	117.1	0.7514	Opt	0.11	0	8	2	0	126.1	0.7577	0.01	0.07679
115	0	6	4	0	147.1	0.7541	Opt	0.1	0	6	4	0	147.1	0.7541	0	0
116	0	6	4	0	147.1	0.7539	Opt	0.1	0	5	5	0	157.6	0.7593	0.01	0.07135
117	0	10	0	0	105.2	0.7911	Opt	0.11	0	10	0	0	105.2	0.7911	0	0
118	0	10	0	0	105.2	0.7871	Opt	0.1	0	10	0	0	105.2	0.774	0	2.9E-05
119	0	9	1	0	115.7	0.7631	Opt	0.111	0	9	1	0	115.7	0.7631	0	0
120	0	9	1	0	115.7	0.7608	Opt	0.13	0	9	1	2	118.7	0.7507	0	0.02594
121	0	6	4	0	147.2	0.7508	Opt	0.1	0	6	4	0	147.2	0.7508	0	0
122	0	6	4	1	148.7	0.7503	Opt	0.11	0	5	5	0	157.7	0.7757	0.01	0.06038
123	0	4	6	0	168.2	0.7809	Opt	0.251	0	4	6	0	168.2	0.7809	0.01	0
124	0	5	5	5	165.2	0.75	Opt	1.311	0	4	6	0	168.2	0.7691	0.01	0.01804
125	0	7	3	0	136.8	0.755	Opt	0.101	0	7	3	0	136.8	0.755	0	0
126	0	7	3	0	136.8	0.7539	Opt	0.1	0	6	4	0	147.3	0.7795	0.01	0.07653
127	0	6	4	0	147.3	0.7558	Opt	0.11	0	6	4	0	147.3	0.7558	0	0
128	0	6	4	0	147.3	0.7544	Opt	0.11	0	5	5	0	157.8	0.7753	0	0.07107
129	0	10	0	0	105.1	0.7148	Opt	0.1	0	10	0	0	105.1	0.7148	0.01	0
130	0	10	0	0	105.1	0.714	Opt	0.14	0	10	0	3	109.6	0.7017	0	0.0428
131	0	8	2	0	126.1	0.7048	Opt	0.101	0	8	2	0	126.1	0.7048	0	0
132	0	8	2	0	126.1	0.7059	Opt	0.11	0	7	3	0	136.6	0.7144	0.01	0.0832
133	1	9	0	0	94.8	0.7276	Opt	0.1	1	9	0	0	94.8	0.7276	0.01	2.3E-05
134	1	9	0	0	94.81	0.7231	Opt	0.11	1	9	0	0	94.81	0.7111	0	3.6E-05
135	0	10	0	0	105.2	0.7378	Opt	0.12	0	10	0	0	105.2	0.7378	0	0
136	0	10	0	0	105.2	0.7358	Opt	0.1	0	10	0	0	105.2	0.7242	0.01	1.9E-05
137	0	7	3	0	136.8	0.7084	Opt	0.111	0	7	3	0	136.8	0.7084	0.01	0
138	0	7	3	0	136.8	0.7088	Opt	0.12	0	7	3	1	138.3	0.7005	0.01	0.01098
139	0	6	4	0	147.3	0.7106	Opt	0.1	0	6	4	0	147.3	0.7106	0	0
140	0	6	4	0	147.3	0.7105	Opt	0.13	0	6	4	0	147.3	0.7016	0.01	6.8E-06
141	0	8	2	0	126.3	0.7188	Opt	0.1	0	8	2	0	126.3	0.7188	0	0
142	0	8	2	0	126.4	0.7182	Opt	0.11	0	8	2	0	126.4	0.7105	0	1.6E-05
143	0	7	3	0	136.8	0.7222	Opt	0.121	0	7	3	0	136.8	0.7222	0	0
144	0	7	3	0	136.9	0.7218	Opt	0.12	0	7	3	0	136.9	0.7144	0.01	7.3E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
145	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
146	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
147	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
148	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
149	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
150	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
151	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
152	10	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
153	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
154	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
155	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
156	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
157	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
158	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
159	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
160	10	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
161	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
162	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
163	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
164	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
165	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
166	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
167	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
168	10	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
169	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
170	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
171	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
172	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
173	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
174	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
175	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
176	10	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
177	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
178	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
179	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
180	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
181	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
182	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
183	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
184	10	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
185	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
186	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
187	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
188	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
189	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
190	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
191	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
192	10	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
145	0	9	1	0	115.6	0.7515	Opt	0.1	0	9	1	0	115.6	0.7515	0.01	0
146	0	9	1	1	117.1	0.7514	Opt	0.12	0	8	2	0	126.1	0.7577	0.01	0.07681
147	0	6	4	0	147.1	0.7541	Opt	0.11	0	6	4	0	147.1	0.7541	0	0
148	0	6	4	0	147.1	0.7539	Opt	0.1	0	5	5	0	157.6	0.7593	0	0.07135
149	0	10	0	0	105.2	0.7911	Opt	0.111	0	10	0	0	105.2	0.7911	0.01	0
150	0	10	0	0	105.2	0.7871	Opt	0.11	0	10	0	0	105.2	0.774	0	1.9E-05
151	0	9	1	0	115.7	0.7631	Opt	0.11	0	9	1	0	115.7	0.7631	0	0
152	0	9	1	0	115.7	0.7608	Opt	0.13	0	9	1	2	118.7	0.7507	0	0.02593
153	0	6	4	0	147.2	0.7508	Opt	0.1	0	6	4	0	147.2	0.7508	0.01	0
154	0	6	4	1	148.7	0.7503	Opt	0.12	0	5	5	0	157.7	0.7757	0.01	0.06044
155	0	4	6	0	168.2	0.7809	Opt	6.9	0	4	6	0	168.2	0.7809	0	0
156	0	5	5	5	165.3	0.7501	Opt	0.301	0	4	6	0	168.2	0.7691	0	0.0181
157	0	7	3	0	136.8	0.755	Opt	0.1	0	7	3	0	136.8	0.755	0.01	0
158	0	7	3	0	136.8	0.7539	Opt	0.1	0	6	4	0	147.3	0.7795	0.01	0.07663
159	0	6	4	0	147.3	0.7558	Opt	0.11	0	6	4	0	147.3	0.7558	0.01	0
160	0	6	4	0	147.3	0.7544	Opt	0.11	0	5	5	0	157.8	0.7753	0.01	0.07117
161	0	10	0	0	105.2	0.7148	Opt	0.111	0	10	0	0	105.2	0.7148	0	0
162	0	10	0	0	105.2	0.714	Opt	0.15	0	10	0	3	109.7	0.7017	0.01	0.0428
163	0	8	2	0	126.2	0.7048	Opt	0.11	0	8	2	0	126.2	0.7048	0	0
164	0	8	2	0	126.2	0.7059	Opt	0.12	0	7	3	0	136.7	0.7144	0.01	0.08316
165	1	9	0	0	94.96	0.7276	Opt	0.11	1	9	0	0	94.96	0.7276	0	4.6E-05
166	1	9	0	0	94.98	0.7231	Opt	0.11	1	9	0	0	94.98	0.7111	0	7.1E-05
167	0	10	0	0	105.3	0.7378	Opt	0.121	0	10	0	0	105.3	0.7378	0	0
168	0	10	0	0	105.3	0.7358	Opt	0.11	0	10	0	0	105.3	0.7242	0	2.8E-05
169	0	7	3	0	136.8	0.7084	Opt	0.12	0	7	3	0	136.8	0.7084	0.01	0
170	0	7	3	0	136.8	0.7088	Opt	0.13	0	7	3	1	138.3	0.7005	0	0.01098
171	0	6	4	0	147.3	0.7106	Opt	0.11	0	6	4	0	147.3	0.7106	0	0
172	0	6	4	0	147.3	0.7105	Opt	0.131	0	6	4	0	147.3	0.7016	0.01	1.4E-05
173	0	8	2	0	126.4	0.7188	Opt	0.11	0	8	2	0	126.4	0.7188	0	0
174	0	8	2	0	126.4	0.7159	Opt	0.13	0	8	2	0	126.5	0.7105	0	4.7E-05
175	0	7	3	0	136.9	0.7222	Opt	0.12	0	7	3	0	136.9	0.7222	0	0
176	0	7	3	0	136.9	0.7218	Opt	0.13	0	7	3	0	137	0.7144	0.01	2.9E-05
177	0	9	1	0	115.6	0.7515	Opt	0.11	0	9	1	0	115.6	0.7515	0.01	0
178	0	9	1	1	117.2	0.7514	Opt	0.121	0	8	2	0	126.2	0.7577	0	0.07677
179	0	6	4	0	147.1	0.7541	Opt	0.11	0	6	4	0	147.1	0.7541	0	0
180	0	6	4	0	147.2	0.7539	Opt	0.11	0	5	5	0	157.7	0.7593	0.01	0.07134
181	0	10	0	0	105.2	0.7911	Opt	0.12	0	10	0	0	105.2	0.7911	0	0
182	0	10	0	0	105.3	0.7871	Opt	0.12	0	10	0	0	105.3	0.774	0	3.8E-05
183	0	9	1	0	115.8	0.7631	Opt	0.12	0	9	1	0	115.8	0.7631	0	0
184	0	9	1	0	115.8	0.7608	Opt	0.141	0	9	1	2	118.8	0.7507	0	0.02593
185	0	6	4	0	147.3	0.7508	Opt	0.11	0	6	4	0	147.3	0.7508	0	0
186	0	6	4	1	148.8	0.7503	Opt	0.12	0	5	5	0	157.8	0.7757	0.01	0.06037
187	0	4	6	0	168.3	0.7809	Opt	0.461	0	4	6	0	168.3	0.7809	0.01	0
188	0	5	5	5	165.3	0.75	Opt	2.193	0	4	6	0	168.3	0.7691	0	0.01805
189	0	7	3	0	136.9	0.755	Opt	0.12	0	7	3	0	136.9	0.755	0	0
190	0	7	3	0	136.9	0.7539	Opt	0.11	0	6	4	0	147.4	0.7795	0	0.0765
191	0	6	4	0	147.4	0.7558	Opt	0.12	0	6	4	0	147.4	0.7558	0	0
192	0	6	4	0	147.4	0.7544	Opt	0.111	0	5	5	0	157.9	0.7753	0.01	0.07104

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
193	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
194	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
195	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
196	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
197	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
198	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
199	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
200	10	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
201	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
202	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
203	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
204	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
205	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
206	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
207	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
208	10	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
209	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
210	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
211	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
212	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
213	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
214	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
215	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
216	10	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
217	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
218	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
219	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
220	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
221	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
222	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
223	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
224	10	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
225	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
226	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
227	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
228	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
229	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
230	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
231	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
232	10	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
233	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
234	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
235	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
236	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
237	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
238	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
239	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
240	10	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
193	0	10	0	0	110.1	0.7148	Opt	0.11	0	10	0	0	110.1	0.7148	0.01	0
194	0	10	0	0	110.1	0.714	Opt	0.14	0	10	0	3	116.1	0.7017	0	0.05451
195	0	8	2	0	132.1	0.7048	Opt	0.12	0	8	2	0	132.1	0.7048	0	0
196	0	8	2	0	132.1	0.7059	Opt	0.12	0	7	3	0	143.1	0.7144	0	0.08326
197	1	9	0	0	99.23	0.7276	Opt	0.11	1	9	0	0	99.23	0.7276	0	2.2E-05
198	1	9	0	0	99.24	0.7231	Opt	0.111	1	9	0	0	99.24	0.7111	0.01	3.4E-05
199	0	10	0	0	110.1	0.7378	Opt	0.12	0	10	0	0	110.1	0.7378	0	0
200	0	10	0	0	110.1	0.7358	Opt	0.13	0	10	0	0	110.1	0.7242	0	1.8E-05
201	0	7	3	0	143.1	0.7084	Opt	0.12	0	7	3	0	143.1	0.7084	0	0
202	0	7	3	0	143.2	0.7088	Opt	0.13	0	7	3	1	145.2	0.7005	0	0.01397
203	0	6	4	0	154.2	0.7106	Opt	0.12	0	6	4	0	154.2	0.7106	0	0
204	0	6	4	0	154.2	0.7105	Opt	0.131	0	6	4	0	154.2	0.7016	0	6.5E-06
205	0	8	2	0	132.2	0.7188	Opt	0.12	0	8	2	0	132.2	0.7188	0	0
206	0	8	2	0	132.2	0.7182	Opt	0.13	0	8	2	0	132.2	0.7105	0	1.5E-05
207	0	7	3	0	143.2	0.7222	Opt	0.16	0	7	3	0	143.2	0.7222	0	0
208	0	7	3	0	143.2	0.7218	Opt	0.181	0	7	3	0	143.2	0.7144	0	1.4E-05
209	0	9	1	0	121.1	0.7515	Opt	0.12	0	9	1	0	121.1	0.7515	0	0
210	0	9	1	1	123.1	0.7514	Opt	0.13	0	8	2	0	132.1	0.7577	0	0.07311
211	0	6	4	0	154.1	0.7541	Opt	0.11	0	6	4	0	154.1	0.7541	0.01	0
212	0	6	4	0	154.1	0.7539	Opt	0.11	0	5	5	0	165.1	0.7593	0.01	0.07138
213	0	10	0	0	110.1	0.7911	Opt	0.12	0	10	0	0	110.1	0.7911	0.01	0
214	0	10	0	0	110.1	0.7871	Opt	0.121	0	10	0	0	110.1	0.774	0	1.8E-05
215	0	9	1	0	121.1	0.7631	Opt	0.12	0	9	1	0	121.1	0.7631	0	0
216	0	9	1	0	121.1	0.7608	Opt	0.13	0	9	1	2	125.1	0.7507	0	0.03303
217	0	6	4	0	154.1	0.7508	Opt	0.12	0	6	4	0	154.1	0.7508	0	0
218	0	6	4	1	156.1	0.7503	Opt	0.12	0	5	5	0	165.1	0.7757	0	0.05758
219	0	4	6	0	176.1	0.7809	Opt	0.681	0	4	6	0	176.1	0.7809	0.01	0
220	0	5	5	5	175.1	0.7501	Opt	2.234	0	4	6	0	176.1	0.7691	0	0.00566
221	0	7	3	0	143.2	0.755	Opt	0.11	0	7	3	0	143.2	0.755	0.01	0
222	0	7	3	0	143.2	0.7539	Opt	0.11	0	6	4	0	154.2	0.7795	0.01	0.07672
223	0	6	4	0	154.2	0.7558	Opt	0.12	0	6	4	0	154.2	0.7558	0.01	0
224	0	6	4	0	154.2	0.7544	Opt	0.12	0	5	5	0	165.2	0.7753	0	0.07125
225	0	10	0	0	110.1	0.7148	Opt	0.12	0	10	0	0	110.1	0.7148	0	0
226	0	10	0	0	110.1	0.714	Opt	0.131	0	10	0	3	116.1	0.7017	0	0.0545
227	0	8	2	0	132.1	0.7048	Opt	0.12	0	8	2	0	132.1	0.7048	0.01	0
228	0	8	2	0	132.1	0.7059	Opt	0.12	0	7	3	0	143.1	0.7144	0	0.08322
229	1	9	0	0	99.39	0.7276	Opt	0.12	1	9	0	0	99.39	0.7276	0.01	4.4E-05
230	1	9	0	0	99.41	0.7231	Opt	0.11	1	9	0	0	99.41	0.7111	0	6.7E-05
231	0	10	0	0	110.2	0.7378	Opt	0.12	0	10	0	0	110.2	0.7378	0	0
232	0	10	0	0	110.2	0.7358	Opt	0.131	0	10	0	0	110.2	0.7242	0	2.7E-05
233	0	7	3	0	143.2	0.7084	Opt	0.11	0	7	3	0	143.2	0.7084	0.01	0
234	0	7	3	0	143.2	0.7088	Opt	0.13	0	7	3	1	145.2	0.7005	0.01	0.01398
235	0	6	4	0	154.2	0.7106	Opt	0.12	0	6	4	0	154.2	0.7106	0	0
236	0	6	4	0	154.2	0.7105	Opt	0.13	0	6	4	0	154.2	0.7016	0	1.3E-05
237	0	8	2	0	132.3	0.7188	Opt	0.121	0	8	2	0	132.3	0.7188	0	0
238	0	8	2	0	132.3	0.7182	Opt	0.14	0	8	2	0	132.3	0.7105	0	3E-05
239	0	7	3	0	143.3	0.7222	Opt	0.15	0	7	3	0	143.3	0.7222	0	0
240	0	7	3	0	143.3	0.7218	Opt	0.13	0	7	3	0	143.3	0.7144	0	2.8E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
241	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
242	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
243	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
244	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
245	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
246	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
247	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
248	10	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
249	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
250	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
251	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
252	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
253	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
254	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
255	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
256	10	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
257	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
258	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
259	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
260	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
261	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
262	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
263	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
264	10	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
265	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
266	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
267	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
268	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
269	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
270	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
271	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
272	10	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
273	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
274	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
275	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
276	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
277	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
278	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
279	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
280	10	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
281	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
282	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
283	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
284	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
285	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
286	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
287	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
288	10	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
241	0	9	1	0	121.1	0.7515	Opt	0.12	0	9	1	0	121.1	0.7515	0.01	0
242	0	9	1	1	123.1	0.7514	Opt	0.131	0	8	2	0	132.1	0.7577	0	0.07307
243	0	6	4	0	154.1	0.7541	Opt	0.12	0	6	4	0	154.1	0.7541	0.01	0
244	0	6	4	0	154.1	0.7539	Opt	0.12	0	5	5	0	165.1	0.7593	0	0.07137
245	0	10	0	0	110.2	0.7911	Opt	0.13	0	10	0	0	110.2	0.7911	0	0
246	0	10	0	0	110.2	0.7871	Opt	0.13	0	10	0	0	110.2	0.774	0	3.6E-05
247	0	9	1	0	121.2	0.7631	Opt	0.12	0	9	1	0	121.2	0.7631	0	0
248	0	9	1	0	121.2	0.7608	Opt	0.131	0	9	1	2	125.2	0.7507	0.01	0.03303
249	0	6	4	0	154.2	0.7508	Opt	0.12	0	6	4	0	154.2	0.7508	0	0
250	0	6	4	1	156.2	0.7503	Opt	0.14	0	5	5	0	165.2	0.7757	0	0.05752
251	0	4	6	0	176.2	0.7809	Opt	0.611	0	4	6	0	176.2	0.7809	0	0
252	0	5	5	5	175.2	0.75	Opt	2.764	0	4	6	0	176.2	0.7691	0	0.00562
253	0	7	3	0	143.3	0.755	Opt	0.12	0	7	3	0	143.3	0.755	0	0
254	0	7	3	0	143.3	0.7539	Opt	0.12	0	6	4	0	154.3	0.7795	0.01	0.0766
255	0	6	4	0	154.3	0.7558	Opt	0.12	0	6	4	0	154.3	0.7558	0	0
256	0	6	4	0	154.3	0.7544	Opt	0.121	0	5	5	0	165.3	0.7753	0	0.07113
257	0	10	0	0	110.1	0.7148	Opt	0.12	0	10	0	0	110.1	0.7148	0.01	0
258	0	10	0	0	110.1	0.714	Opt	0.14	0	10	0	3	116.1	0.7017	0	0.05449
259	0	8	2	0	132.1	0.7048	Opt	0.12	0	8	2	0	132.1	0.7048	0.01	0
260	0	8	2	0	132.1	0.7059	Opt	0.12	0	7	3	0	143.1	0.7144	0.01	0.08323
261	1	9	0	0	99.25	0.7276	Opt	0.131	1	9	0	0	99.25	0.7276	0	2.2E-05
262	1	9	0	0	99.26	0.7231	Opt	0.12	1	9	0	0	99.26	0.7111	0	3.4E-05
263	0	10	0	0	110.2	0.7378	Opt	0.13	0	10	0	0	110.2	0.7378	0	0
264	0	10	0	0	110.2	0.7358	Opt	0.14	0	10	0	0	110.2	0.7242	0	1.8E-05
265	0	7	3	0	143.2	0.7084	Opt	0.12	0	7	3	0	143.2	0.7084	0	0
266	0	7	3	0	143.2	0.7088	Opt	0.13	0	7	3	1	145.2	0.7005	0.01	0.01397
267	0	6	4	0	154.2	0.7106	Opt	0.131	0	6	4	0	154.2	0.7106	0	0
268	0	6	4	0	154.2	0.7105	Opt	0.13	0	6	4	0	154.2	0.7016	0	6.5E-06
269	0	8	2	0	132.3	0.7188	Opt	0.12	0	8	2	0	132.3	0.7188	0.01	0
270	0	8	2	0	132.3	0.7182	Opt	0.14	0	8	2	0	132.3	0.7105	0	1.5E-05
271	0	7	3	0	143.3	0.7222	Opt	0.16	0	7	3	0	143.3	0.7222	0	0
272	0	7	3	0	143.3	0.7218	Opt	0.17	0	7	3	0	143.3	0.7144	0.011	1.4E-05
273	0	9	1	0	121.1	0.7515	Opt	0.12	0	9	1	0	121.1	0.7515	0.01	0
274	0	9	1	1	123.1	0.7514	Opt	0.15	0	8	2	0	132.1	0.7577	0	0.07307
275	0	6	4	0	154.1	0.7541	Opt	0.13	0	6	4	0	154.1	0.7541	0	0
276	0	6	4	0	154.1	0.7539	Opt	0.121	0	5	5	0	165.1	0.7593	0	0.07136
277	0	10	0	0	110.1	0.7911	Opt	0.13	0	10	0	0	110.1	0.7911	0.01	0
278	0	10	0	0	110.2	0.7871	Opt	0.13	0	10	0	0	110.2	0.774	0	9.1E-06
279	0	9	1	0	121.2	0.7631	Opt	0.13	0	9	1	0	121.2	0.7631	0	0
280	0	9	1	0	121.2	0.7608	Opt	0.14	0	9	1	2	125.2	0.7507	0	0.03302
281	0	6	4	0	154.2	0.7508	Opt	0.12	0	6	4	0	154.2	0.7508	0.01	0
282	0	6	4	1	156.2	0.7503	Opt	0.141	0	5	5	0	165.2	0.7757	0	0.05754
283	0	4	6	0	176.2	0.7809	Opt	1.121	0	4	6	0	176.2	0.7809	0.01	0
284	0	5	5	5	175.2	0.7501	Opt	0.932	0	4	6	0	176.2	0.7691	0	0.00564
285	0	7	3	0	143.2	0.755	Opt	0.13	0	7	3	0	143.2	0.755	0	0
286	0	7	3	0	143.2	0.7539	Opt	0.13	0	6	4	0	154.2	0.7795	0	0.07667
287	0	6	4	0	154.2	0.7558	Opt	0.12	0	6	4	0	154.2	0.7558	0.01	0
288	0	6	4	0	154.2	0.7544	Opt	0.12	0	5	5	0	165.2	0.7753	0.01	0.0712

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
289	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
290	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
291	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
292	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
293	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
294	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
295	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
296	10	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
297	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
298	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
299	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
300	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
301	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
302	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
303	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
304	10	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
305	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
306	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
307	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
308	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
309	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
310	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
311	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
312	10	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
313	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
314	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
315	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
316	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
317	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
318	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
319	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
320	10	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
321	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
322	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
323	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
324	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
325	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
326	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
327	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
328	10	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
329	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
330	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
331	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
332	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
333	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
334	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
335	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
336	10	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
289	0	10	0	0	110.1	0.7148	Opt	0.121	0	10	0	0	110.1	0.7148	0.01	0
290	0	10	0	0	110.1	0.714	Opt	0.13	0	10	0	3	116.1	0.7017	0.01	0.05449
291	0	8	2	0	132.1	0.7048	Opt	0.12	0	8	2	0	132.1	0.7048	0.01	0
292	0	8	2	0	132.1	0.7059	Opt	0.13	0	7	3	0	143.1	0.7144	0.01	0.08319
293	1	9	0	0	99.41	0.7276	Opt	0.13	1	9	0	0	99.41	0.7276	0	4.4E-05
294	1	9	0	0	99.43	0.7231	Opt	0.121	1	9	0	0	99.42	0.7111	0	6.7E-05
295	0	10	0	0	110.2	0.7378	Opt	0.13	0	10	0	0	110.2	0.7378	0.01	0
296	0	10	0	0	110.2	0.7358	Opt	0.13	0	10	0	0	110.2	0.7242	0	2.7E-05
297	0	7	3	0	143.2	0.7084	Opt	0.13	0	7	3	0	143.2	0.7084	0	0
298	0	7	3	0	143.2	0.7088	Opt	0.13	0	7	3	1	145.2	0.7005	0.01	0.01398
299	0	6	4	0	154.2	0.7106	Opt	0.12	0	6	4	0	154.2	0.7106	0.01	0
300	0	6	4	0	154.2	0.7105	Opt	0.181	0	6	4	0	154.2	0.7016	0	1.9E-05
301	0	8	2	0	132.4	0.7188	Opt	0.13	0	8	2	0	132.4	0.7188	0	0
302	0	8	2	0	132.4	0.7182	Opt	0.13	0	8	2	0	132.4	0.7105	0.01	3E-05
303	0	7	3	0	143.3	0.7222	Opt	0.16	0	7	3	0	143.3	0.7222	0.01	0
304	0	7	3	0	143.4	0.7218	Opt	0.171	0	7	3	0	143.4	0.7144	0	2.1E-05
305	0	9	1	0	121.1	0.7515	Opt	0.13	0	9	1	0	121.1	0.7515	0.01	0
306	0	9	1	1	123.1	0.7514	Opt	0.15	0	8	2	0	132.1	0.7577	0	0.07304
307	0	6	4	0	154.1	0.7541	Opt	0.13	0	6	4	0	154.1	0.7541	0	0
308	0	6	4	0	154.1	0.7539	Opt	0.13	0	5	5	0	165.1	0.7593	0	0.07135
309	0	10	0	0	110.2	0.7911	Opt	0.131	0	10	0	0	110.2	0.7911	0.01	0
310	0	10	0	0	110.2	0.7871	Opt	0.14	0	10	0	0	110.2	0.774	0.01	2.7E-05
311	0	9	1	0	121.2	0.7631	Opt	0.13	0	9	1	0	121.2	0.7631	0.01	0
312	0	9	1	0	121.2	0.7608	Opt	0.14	0	9	1	2	125.2	0.7507	0	0.03302
313	0	6	4	0	154.2	0.7508	Opt	0.13	0	6	4	0	154.2	0.7508	0	0
314	0	6	4	1	156.2	0.7503	Opt	0.141	0	5	5	0	165.2	0.7757	0.01	0.05748
315	0	4	6	0	176.2	0.7809	Opt	0.57	0	4	6	0	176.2	0.7809	0	0
316	0	5	5	5	175.2	0.75	Opt	1.893	0	4	6	0	176.2	0.7691	0.01	0.0056
317	0	7	3	0	143.3	0.755	Opt	0.13	0	7	3	0	143.3	0.755	0.01	0
318	0	7	3	0	143.3	0.7539	Opt	0.131	0	6	4	0	154.3	0.7795	0	0.07654
319	0	6	4	0	154.3	0.7558	Opt	0.14	0	6	4	0	154.3	0.7558	0	0
320	0	6	4	0	154.3	0.7544	Opt	0.13	0	5	5	0	165.3	0.7753	0	0.07108
321	0	10	0	0	110.1	0.7148	Opt	0.13	0	10	0	0	110.1	0.7148	0	0
322	0	10	0	0	110.1	0.714	Opt	0.15	0	10	0	3	116.1	0.7017	0.01	0.05448
323	0	8	2	0	132.1	0.7048	Opt	0.141	0	8	2	0	132.1	0.7048	0	0
324	0	8	2	0	132.1	0.7059	Opt	0.14	0	7	3	0	143.1	0.7144	0	0.08321
325	1	9	0	0	99.3	0.7276	Opt	0.14	1	9	0	0	99.3	0.7276	0	2.2E-05
326	1	9	0	0	99.31	0.7231	Opt	0.13	1	9	0	0	99.31	0.7111	0	3.4E-05
327	0	10	0	0	110.2	0.7378	Opt	0.13	0	10	0	0	110.2	0.7378	0.01	0
328	0	10	0	0	110.2	0.7358	Opt	0.141	0	10	0	0	110.2	0.7242	0.01	1.8E-05
329	0	7	3	0	143.3	0.7084	Opt	0.14	0	7	3	0	143.3	0.7084	0	0
330	0	7	3	0	143.3	0.7088	Opt	0.15	0	7	3	1	145.3	0.7005	0	0.01397
331	0	6	4	0	154.3	0.7106	Opt	0.13	0	6	4	0	154.3	0.7106	0.01	0
332	0	6	4	0	154.3	0.7105	Opt	0.14	0	6	4	0	154.3	0.7016	0.01	6.5E-06
333	0	8	2	0	132.3	0.7188	Opt	0.131	0	8	2	0	132.3	0.7188	0.01	0
334	0	8	2	0	132.4	0.7182	Opt	0.14	0	8	2	0	132.4	0.7105	0.01	1.5E-05
335	0	7	3	0	143.3	0.7222	Opt	0.17	0	7	3	0	143.3	0.7222	0.01	0
336	0	7	3	0	143.4	0.7218	Opt	0.19	0	7	3	0	143.4	0.7144	0.01	7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
337	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
338	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
339	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
340	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
341	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
342	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
343	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
344	10	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
345	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
346	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
347	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
348	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
349	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
350	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
351	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
352	10	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
353	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
354	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
355	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
356	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
357	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
358	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
359	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
360	10	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
361	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
362	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
363	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
364	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
365	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
366	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
367	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
368	10	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
369	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
370	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
371	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
372	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
373	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
374	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
375	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
376	10	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
377	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
378	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
379	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
380	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
381	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
382	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
383	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
384	10	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
337	0	9	1	0	121.1	0.7515	Opt	0.131	0	9	1	0	121.1	0.7515	0.01	0
338	0	9	1	1	123.1	0.7514	Opt	0.15	0	8	2	0	132.1	0.7577	0	0.07307
339	0	6	4	0	154.1	0.7541	Opt	0.13	0	6	4	0	154.1	0.7541	0.01	0
340	0	6	4	0	154.1	0.7539	Opt	0.14	0	5	5	0	165.1	0.7593	0	0.07135
341	0	10	0	0	110.2	0.7911	Opt	0.14	0	10	0	0	110.2	0.7911	0	0
342	0	10	0	0	110.2	0.7871	Opt	0.151	0	10	0	0	110.2	0.774	0	1.8E-05
343	0	9	1	0	121.2	0.7631	Opt	0.14	0	9	1	0	121.2	0.7631	0	0
344	0	9	1	0	121.2	0.7608	Opt	0.14	0	9	1	2	125.2	0.7507	0	0.03301
345	0	6	4	0	154.2	0.7508	Opt	0.13	0	6	4	0	154.2	0.7508	0.01	0
346	0	6	4	1	156.2	0.7503	Opt	0.15	0	5	5	0	165.2	0.7757	0	0.05754
347	0	4	6	0	176.2	0.7809	Opt	0.681	0	4	6	0	176.2	0.7809	0	0
348	0	5	5	5	175.3	0.7501	Opt	2.103	0	4	6	0	176.2	0.7691	0	0.00565
349	0	7	3	0	143.3	0.755	Opt	0.141	0	7	3	0	143.3	0.755	0	0
350	0	7	3	0	143.3	0.7539	Opt	0.13	0	6	4	0	154.3	0.7795	0	0.07665
351	0	6	4	0	154.3	0.7558	Opt	0.14	0	6	4	0	154.3	0.7558	0.01	0
352	0	6	4	0	154.3	0.7544	Opt	0.14	0	5	5	0	165.3	0.7753	0	0.07118
353	0	10	0	0	110.2	0.7148	Opt	0.14	0	10	0	0	110.2	0.7148	0	0
354	0	10	0	0	110.2	0.714	Opt	0.151	0	10	0	3	116.2	0.7017	0	0.05447
355	0	8	2	0	132.2	0.7048	Opt	0.15	0	8	2	0	132.2	0.7048	0	0
356	0	8	2	0	132.2	0.7059	Opt	0.14	0	7	3	0	143.2	0.7144	0	0.08317
357	1	9	0	0	99.46	0.7276	Opt	0.13	1	9	0	0	99.46	0.7276	0.01	4.4E-05
358	1	9	0	0	99.48	0.7231	Opt	0.131	1	9	0	0	99.48	0.7111	0.01	6.7E-05
359	0	10	0	0	110.3	0.7378	Opt	0.15	0	10	0	0	110.3	0.7378	0	0
360	0	10	0	0	110.3	0.7358	Opt	0.15	0	10	0	0	110.3	0.7242	0	2.7E-05
361	0	7	3	0	143.3	0.7084	Opt	0.13	0	7	3	0	143.3	0.7084	0.01	0
362	0	7	3	0	143.3	0.7088	Opt	0.14	0	7	3	1	145.3	0.7005	0.01	0.01397
363	0	6	4	0	154.3	0.7106	Opt	0.131	0	6	4	0	154.3	0.7106	0.01	0
364	0	6	4	0	154.3	0.7105	Opt	0.15	0	6	4	0	154.3	0.7016	0.01	1.3E-05
365	0	8	2	0	132.4	0.7188	Opt	0.15	0	8	2	0	132.4	0.7188	0	0
366	0	8	2	0	132.5	0.7182	Opt	0.15	0	8	2	0	132.5	0.7105	0	3E-05
367	0	7	3	0	143.4	0.7222	Opt	0.191	0	7	3	0	143.4	0.7222	0	0
368	0	7	3	0	143.4	0.7218	Opt	0.2	0	7	3	0	143.5	0.7144	0	2.8E-05
369	0	9	1	0	121.1	0.7515	Opt	0.14	0	9	1	0	121.1	0.7515	0	0
370	0	9	1	1	123.2	0.7514	Opt	0.16	0	8	2	0	132.2	0.7577	0	0.07303
371	0	6	4	0	154.1	0.7541	Opt	0.14	0	6	4	0	154.1	0.7541	0	0
372	0	6	4	0	154.2	0.7539	Opt	0.131	0	5	5	0	165.2	0.7593	0.01	0.07134
373	0	10	0	0	110.2	0.7911	Opt	0.15	0	10	0	0	110.2	0.7911	0	0
374	0	10	0	0	110.3	0.7871	Opt	0.14	0	10	0	0	110.3	0.774	0.01	3.6E-05
375	0	9	1	0	121.3	0.7631	Opt	0.14	0	9	1	0	121.3	0.7631	0	0
376	0	9	1	0	121.3	0.7608	Opt	0.15	0	9	1	2	125.3	0.7507	0	0.033
377	0	6	4	0	154.3	0.7508	Opt	0.131	0	6	4	0	154.3	0.7508	0.01	0
378	0	6	4	1	156.3	0.7503	Opt	0.15	0	5	5	0	165.3	0.7757	0.01	0.05747
379	0	4	6	0	176.3	0.7809	Opt	0.551	0	4	6	0	176.3	0.7809	0.01	0
380	0	5	5	5	175.3	0.75	Opt	6.379	0	4	6	0	176.3	0.7691	0	0.00561
381	0	7	3	0	143.4	0.755	Opt	0.14	0	7	3	0	143.4	0.755	0	0
382	0	7	3	0	143.4	0.7539	Opt	0.14	0	6	4	0	154.4	0.7795	0.01	0.07652
383	0	6	4	0	154.4	0.7558	Opt	0.141	0	6	4	0	154.4	0.7558	0	0
384	0	6	4	0	154.4	0.7544	Opt	0.14	0	5	5	0	165.4	0.7753	0.01	0.07106

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
385	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
386	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
387	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
388	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
389	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
390	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
391	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
392	10	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
393	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
394	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
395	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
396	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
397	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
398	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
399	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
400	10	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
401	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
402	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
403	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
404	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
405	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
406	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
407	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
408	10	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
409	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
410	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
411	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
412	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
413	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
414	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
415	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
416	10	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
417	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
418	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
419	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
420	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
421	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
422	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
423	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
424	10	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
425	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
426	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
427	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
428	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
429	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
430	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
431	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
432	10	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
385	0	10	0	0	105.1	0.7148	Opt	0.14	0	10	0	0	105.1	0.7148	0	0
386	0	10	0	0	105.1	0.714	Opt	0.15	0	10	0	3	112.6	0.7017	0.01	0.07138
387	0	8	2	0	126.1	0.7048	Opt	0.14	0	8	2	0	126.1	0.7048	0	0
388	0	8	2	0	126.1	0.7059	Opt	0.141	0	7	3	0	136.6	0.7144	0	0.08325
389	1	9	0	0	94.73	0.7276	Opt	0.14	1	9	0	0	94.73	0.7276	0.01	2.3E-05
390	1	9	0	0	94.74	0.7231	Opt	0.14	1	9	0	0	94.74	0.7111	0	3.6E-05
391	0	10	0	0	105.1	0.7378	Opt	0.14	0	10	0	0	105.1	0.7378	0.01	0
392	0	10	0	0	105.1	0.7358	Opt	0.15	0	10	0	0	105.1	0.7242	0	1.9E-05
393	0	7	3	0	136.6	0.7084	Opt	0.141	0	7	3	0	136.6	0.7084	0	0
394	0	7	3	0	136.7	0.7088	Opt	0.13	0	7	3	1	139.2	0.7005	0.01	0.01829
395	0	6	4	0	147.2	0.7106	Opt	0.15	0	6	4	0	147.2	0.7106	0.01	0
396	0	6	4	0	147.2	0.7105	Opt	0.17	0	6	4	0	147.2	0.7016	0	6.8E-06
397	0	8	2	0	126.2	0.7188	Opt	0.14	0	8	2	0	126.2	0.7188	0	0
398	0	8	2	0	126.2	0.7182	Opt	0.151	0	8	2	0	126.2	0.7105	0	1.6E-05
399	0	7	3	0	136.7	0.7222	Opt	0.18	0	7	3	0	136.7	0.7222	0.01	0
400	0	7	3	0	136.7	0.7218	Opt	0.17	0	7	3	0	136.7	0.7144	0	1.5E-05
401	0	9	1	0	115.6	0.7515	Opt	0.13	0	9	1	0	115.6	0.7515	0.01	0
402	0	9	1	1	118.1	0.7514	Opt	0.171	0	8	2	0	126.1	0.7577	0.01	0.06773
403	0	6	4	0	147.1	0.7541	Opt	0.14	0	6	4	0	147.1	0.7541	0.01	0
404	0	6	4	0	147.1	0.7539	Opt	0.14	0	5	5	0	157.6	0.7593	0.01	0.07138
405	0	10	0	0	105.1	0.7911	Opt	0.15	0	10	0	0	105.1	0.7911	0	0
406	0	10	0	0	105.1	0.7871	Opt	0.151	0	10	0	0	105.1	0.774	0	1.9E-05
407	0	9	1	0	115.6	0.7631	Opt	0.14	0	9	1	0	115.6	0.7631	0.01	0
408	0	9	1	0	115.6	0.7608	Opt	0.14	0	9	1	2	120.6	0.7507	0.01	0.04325
409	0	6	4	0	147.1	0.7508	Opt	0.14	0	6	4	0	147.1	0.7508	0.01	0
410	0	6	4	1	149.6	0.7503	Opt	0.16	0	5	5	0	157.6	0.7757	0	0.0534
411	0	4	6	0	168.1	0.7809	Opt	0.511	0	4	6	0	168.1	0.7809	0	0
412	0	4	6	0	168.1	0.7789	Opt	0.541	0	4	6	0	168.1	0.7691	0.01	0
413	0	7	3	0	136.7	0.755	Opt	0.14	0	7	3	0	136.7	0.755	0	0
414	0	7	3	0	136.7	0.7539	Opt	0.14	0	6	4	0	147.2	0.7795	0.01	0.07671
415	0	6	4	0	147.2	0.7558	Opt	0.141	0	6	4	0	147.2	0.7558	0.01	0
416	0	6	4	0	147.2	0.7544	Opt	0.15	0	5	5	0	157.7	0.7753	0	0.07124
417	0	10	0	0	105.1	0.7148	Opt	0.15	0	10	0	0	105.1	0.7148	0	0
418	0	10	0	0	105.1	0.714	Opt	0.15	0	10	0	3	112.6	0.7017	0	0.07136
419	0	8	2	0	126.1	0.7048	Opt	0.14	0	8	2	0	126.1	0.7048	0.01	0
420	0	8	2	0	126.1	0.7059	Opt	0.161	0	7	3	0	136.6	0.7144	0	0.08321
421	1	9	0	0	94.89	0.7276	Opt	0.15	1	9	0	0	94.89	0.7276	0	4.6E-05
422	1	9	0	0	94.91	0.7231	Opt	0.14	1	9	0	0	94.91	0.7111	0	7.1E-05
423	0	10	0	0	105.2	0.7378	Opt	0.15	0	10	0	0	105.2	0.7378	0.01	0
424	0	10	0	0	105.2	0.7358	Opt	0.141	0	10	0	0	105.2	0.7242	0.01	2.9E-05
425	0	7	3	0	136.7	0.7084	Opt	0.14	0	7	3	0	136.7	0.7084	0.01	0
426	0	7	3	0	136.7	0.7088	Opt	0.14	0	7	3	1	139.2	0.7005	0.01	0.0183
427	0	6	4	0	147.2	0.7106	Opt	0.15	0	6	4	0	147.2	0.7106	0.01	0
428	0	6	4	0	147.2	0.7105	Opt	0.16	0	6	4	0	147.2	0.7016	0	1.4E-05
429	0	8	2	0	126.3	0.7188	Opt	0.161	0	8	2	0	126.3	0.7188	0	0
430	0	8	2	0	126.3	0.7182	Opt	0.15	0	8	2	0	126.3	0.7105	0	3.2E-05
431	0	7	3	0	136.8	0.7222	Opt	0.18	0	7	3	0	136.8	0.7222	0.01	0
432	0	7	3	0	136.8	0.7218	Opt	0.15	0	7	3	0	136.8	0.7144	0.01	2.9E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
433	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
434	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
435	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
436	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
437	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
438	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
439	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
440	10	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
441	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
442	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
443	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
444	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
445	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
446	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
447	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
448	10	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
449	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
450	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
451	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
452	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
453	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
454	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
455	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
456	10	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
457	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
458	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
459	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
460	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
461	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
462	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
463	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
464	10	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
465	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
466	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
467	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
468	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
469	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
470	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
471	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
472	10	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
473	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
474	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
475	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
476	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
477	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
478	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
479	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
480	10	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
433	0	9	1	0	115.6	0.7515	Opt	0.141	0	9	1	0	115.6	0.7515	0.01	0
434	0	9	1	1	118.1	0.7514	Opt	0.17	0	8	2	0	126.1	0.7577	0.01	0.0677
435	0	6	4	0	147.1	0.7541	Opt	0.15	0	6	4	0	147.1	0.7541	0	0
436	0	6	4	0	147.1	0.7539	Opt	0.15	0	5	5	0	157.6	0.7593	0	0.07137
437	0	10	0	0	105.2	0.7911	Opt	0.151	0	10	0	0	105.2	0.7911	0	0
438	0	10	0	0	105.2	0.7871	Opt	0.15	0	10	0	0	105.2	0.774	0.01	3.8E-05
439	0	9	1	0	115.7	0.7631	Opt	0.14	0	9	1	0	115.7	0.7631	0.01	0
440	0	9	1	0	115.7	0.7608	Opt	0.15	0	9	1	2	120.7	0.7507	0.01	0.04325
441	0	6	4	0	147.2	0.7508	Opt	0.15	0	6	4	0	147.2	0.7508	0	0
442	0	6	4	1	149.7	0.7503	Opt	0.161	0	5	5	0	157.7	0.7757	0.01	0.05334
443	0	4	6	0	168.2	0.7809	Opt	0.28	0	4	6	0	168.2	0.7809	0	0
444	0	4	6	0	168.2	0.7789	Opt	2.333	0	4	6	0	168.2	0.7691	0	1.2E-05
445	0	7	3	0	136.8	0.755	Opt	0.151	0	7	3	0	136.8	0.755	0	0
446	0	7	3	0	136.8	0.7539	Opt	0.15	0	6	4	0	147.3	0.7795	0	0.07658
447	0	6	4	0	147.3	0.7558	Opt	0.15	0	6	4	0	147.3	0.7558	0	0
448	0	6	4	0	147.3	0.7544	Opt	0.15	0	5	5	0	157.8	0.7753	0	0.07111
449	0	10	0	0	105.1	0.7148	Opt	0.15	0	10	0	0	105.1	0.7148	0	0
450	0	10	0	0	105.1	0.714	Opt	0.16	0	10	0	3	112.6	0.7017	0.011	0.07136
451	0	8	2	0	126.1	0.7048	Opt	0.15	0	8	2	0	126.1	0.7048	0	0
452	0	8	2	0	126.1	0.7059	Opt	0.15	0	7	3	0	136.6	0.7144	0	0.08322
453	1	9	0	0	94.75	0.7276	Opt	0.15	1	9	0	0	94.75	0.7276	0.01	2.3E-05
454	1	9	0	0	94.76	0.7231	Opt	0.151	1	9	0	0	94.76	0.7111	0	3.6E-05
455	0	10	0	0	105.2	0.7378	Opt	0.17	0	10	0	0	105.2	0.7378	0	0
456	0	10	0	0	105.2	0.7358	Opt	0.16	0	10	0	0	105.2	0.7242	0	1.9E-05
457	0	7	3	0	136.7	0.7084	Opt	0.15	0	7	3	0	136.7	0.7084	0.01	0
458	0	7	3	0	136.7	0.7088	Opt	0.151	0	7	3	1	139.2	0.7005	0	0.0183
459	0	6	4	0	147.2	0.7106	Opt	0.15	0	6	4	0	147.2	0.7106	0.01	0
460	0	6	4	0	147.2	0.7105	Opt	0.16	0	6	4	0	147.2	0.7016	0	6.8E-06
461	0	8	2	0	126.3	0.7188	Opt	0.16	0	8	2	0	126.3	0.7188	0	0
462	0	8	2	0	126.3	0.7182	Opt	0.15	0	8	2	0	126.3	0.7105	0	1.6E-05
463	0	7	3	0	136.8	0.7222	Opt	0.191	0	7	3	0	136.8	0.7222	0.01	0
464	0	7	3	0	136.8	0.7218	Opt	0.17	0	7	3	0	136.8	0.7144	0	1.5E-05
465	0	9	1	0	115.6	0.7515	Opt	0.15	0	9	1	0	115.6	0.7515	0.01	0
466	0	9	1	1	118.1	0.7514	Opt	0.16	0	8	2	0	126.1	0.7577	0	0.0677
467	0	6	4	0	147.1	0.7541	Opt	0.151	0	6	4	0	147.1	0.7541	0.01	0
468	0	6	4	0	147.1	0.7539	Opt	0.15	0	5	5	0	157.6	0.7593	0.01	0.07136
469	0	10	0	0	105.1	0.7911	Opt	0.16	0	10	0	0	105.1	0.7911	0	0
470	0	10	0	0	105.2	0.7871	Opt	0.16	0	10	0	0	105.2	0.774	0	9.5E-06
471	0	9	1	0	115.7	0.7631	Opt	0.161	0	9	1	0	115.7	0.7631	0	0
472	0	9	1	0	115.7	0.7608	Opt	0.16	0	9	1	2	120.7	0.7507	0	0.04324
473	0	6	4	0	147.2	0.7508	Opt	0.15	0	6	4	0	147.2	0.7508	0	0
474	0	6	4	1	149.7	0.7503	Opt	0.16	0	5	5	0	157.7	0.7757	0.01	0.05335
475	0	4	6	0	168.2	0.7809	Opt	0.361	0	4	6	0	168.2	0.7809	0	0
476	0	4	6	0	168.2	0.7789	Opt	0.46	0	4	6	0	168.2	0.7691	0	5.9E-06
477	0	7	3	0	136.7	0.755	Opt	0.151	0	7	3	0	136.7	0.755	0	0
478	0	7	3	0	136.7	0.7539	Opt	0.15	0	6	4	0	147.2	0.7795	0.01	0.07665
479	0	6	4	0	147.2	0.7558	Opt	0.16	0	6	4	0	147.2	0.7558	0	0
480	0	6	4	0	147.2	0.7544	Opt	0.15	0	5	5	0	157.7	0.7753	0	0.07119

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
481	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
482	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
483	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
484	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
485	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
486	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
487	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
488	10	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
489	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
490	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
491	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
492	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
493	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
494	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
495	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
496	10	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
497	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
498	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
499	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
500	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
501	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
502	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
503	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
504	10	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
505	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
506	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
507	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
508	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
509	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
510	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
511	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
512	10	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
513	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
514	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
515	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
516	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
517	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
518	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
519	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
520	10	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
521	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
522	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
523	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
524	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
525	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
526	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
527	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
528	10	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
481	0	10	0	0	105.1	0.7148	Opt	0.151	0	10	0	0	105.1	0.7148	0.01	0
482	0	10	0	0	105.1	0.714	Opt	0.16	0	10	0	3	112.6	0.7017	0.01	0.07135
483	0	8	2	0	126.1	0.7048	Opt	0.16	0	8	2	0	126.1	0.7048	0	0
484	0	8	2	0	126.1	0.7059	Opt	0.16	0	7	3	0	136.6	0.7144	0	0.08318
485	1	9	0	0	94.91	0.7276	Opt	0.151	1	9	0	0	94.91	0.7276	0	4.6E-05
486	1	9	0	0	94.93	0.7231	Opt	0.15	1	9	0	0	94.92	0.7111	0.01	7.1E-05
487	0	10	0	0	105.2	0.7378	Opt	0.17	0	10	0	0	105.2	0.7378	0	0
488	0	10	0	0	105.2	0.7358	Opt	0.17	0	10	0	0	105.2	0.7242	0	2.9E-05
489	0	7	3	0	136.7	0.7084	Opt	0.15	0	7	3	0	136.7	0.7084	0	0
490	0	7	3	0	136.7	0.7088	Opt	0.151	0	7	3	1	139.2	0.7005	0.01	0.0183
491	0	6	4	0	147.2	0.7106	Opt	0.15	0	6	4	0	147.2	0.7106	0.01	0
492	0	6	4	0	147.2	0.7105	Opt	0.17	0	6	4	0	147.2	0.7016	0.01	2E-05
493	0	8	2	0	126.4	0.7188	Opt	0.16	0	8	2	0	126.4	0.7188	0	0
494	0	8	2	0	126.4	0.7182	Opt	0.171	0	8	2	0	126.4	0.7105	0	3.2E-05
495	0	7	3	0	136.8	0.7222	Opt	0.18	0	7	3	0	136.8	0.7222	0	0
496	0	7	3	0	136.9	0.7218	Opt	0.21	0	7	3	0	136.9	0.7144	0	2.2E-05
497	0	9	1	0	115.6	0.7515	Opt	0.16	0	9	1	0	115.6	0.7515	0	0
498	0	9	1	1	118.1	0.7514	Opt	0.171	0	8	2	0	126.1	0.7577	0	0.06767
499	0	6	4	0	147.1	0.7541	Opt	0.15	0	6	4	0	147.1	0.7541	0.01	0
500	0	6	4	0	147.1	0.7539	Opt	0.16	0	5	5	0	157.6	0.7593	0	0.07135
501	0	10	0	0	105.2	0.7911	Opt	0.17	0	10	0	0	105.2	0.7911	0	0
502	0	10	0	0	105.2	0.7871	Opt	0.171	0	10	0	0	105.2	0.774	0	2.9E-05
503	0	9	1	0	115.7	0.7631	Opt	0.16	0	9	1	0	115.7	0.7631	0	0
504	0	9	1	0	115.7	0.7608	Opt	0.17	0	9	1	2	120.7	0.7507	0	0.04323
505	0	6	4	0	147.2	0.7508	Opt	0.16	0	6	4	0	147.2	0.7508	0	0
506	0	6	4	1	149.7	0.7503	Opt	0.171	0	5	5	0	157.7	0.7757	0	0.05329
507	0	4	6	0	168.2	0.7809	Opt	0.31	0	4	6	0	168.2	0.7809	0	0
508	0	4	6	0	168.2	0.7789	Opt	2.253	0	4	6	0	168.2	0.7691	0	5.9E-06
509	0	7	3	0	136.8	0.755	Opt	0.16	0	7	3	0	136.8	0.755	0	0
510	0	7	3	0	136.8	0.7539	Opt	0.161	0	6	4	0	147.3	0.7795	0	0.07653
511	0	6	4	0	147.3	0.7558	Opt	0.15	0	6	4	0	147.3	0.7558	0.01	0
512	0	6	4	0	147.3	0.7544	Opt	0.15	0	5	5	0	157.8	0.7753	0.01	0.07107
513	0	10	0	0	105.1	0.7148	Opt	0.16	0	10	0	0	105.1	0.7148	0.01	0
514	0	10	0	0	105.1	0.714	Opt	0.181	0	10	0	3	112.6	0.7017	0	0.07133
515	0	8	2	0	126.1	0.7048	Opt	0.16	0	8	2	0	126.1	0.7048	0	0
516	0	8	2	0	126.1	0.7059	Opt	0.16	0	7	3	0	136.6	0.7144	0	0.0832
517	1	9	0	0	94.8	0.7276	Opt	0.16	1	9	0	0	94.8	0.7276	0.01	2.3E-05
518	1	9	0	0	94.81	0.7231	Opt	0.161	1	9	0	0	94.81	0.7111	0	3.6E-05
519	0	10	0	0	105.2	0.7378	Opt	0.17	0	10	0	0	105.2	0.7378	0	0
520	0	10	0	0	105.2	0.7358	Opt	0.16	0	10	0	0	105.2	0.7242	0	1.9E-05
521	0	7	3	0	136.8	0.7084	Opt	0.16	0	7	3	0	136.8	0.7084	0.01	0
522	0	7	3	0	136.8	0.7088	Opt	0.161	0	7	3	1	139.3	0.7005	0	0.01829
523	0	6	4	0	147.3	0.7106	Opt	0.16	0	6	4	0	147.3	0.7106	0.01	0
524	0	6	4	0	147.3	0.7105	Opt	0.17	0	6	4	0	147.3	0.7016	0.01	6.8E-06
525	0	8	2	0	126.3	0.7188	Opt	0.16	0	8	2	0	126.3	0.7188	0	0
526	0	8	2	0	126.4	0.7182	Opt	0.171	0	8	2	0	126.4	0.7105	0	1.6E-05
527	0	7	3	0	136.8	0.7222	Opt	0.2	0	7	3	0	136.8	0.7222	0.01	0
528	0	7	3	0	136.9	0.7218	Opt	0.19	0	7	3	0	136.9	0.7144	0	7.3E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
529	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
530	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
531	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
532	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
533	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
534	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
535	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
536	10	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
537	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
538	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
539	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
540	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
541	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
542	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
543	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
544	10	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
545	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
546	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
547	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
548	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
549	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
550	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
551	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
552	10	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
553	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
554	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
555	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
556	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
557	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
558	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
559	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
560	10	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
561	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
562	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
563	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
564	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
565	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
566	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
567	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
568	10	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
569	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
570	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
571	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
572	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
573	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
574	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
575	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
576	10	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
529	0	9	1	0	115.6	0.7515	Opt	0.16	0	9	1	0	115.6	0.7515	0	0
530	0	9	1	1	118.1	0.7514	Opt	0.171	0	8	2	0	126.1	0.7577	0.01	0.06769
531	0	6	4	0	147.1	0.7541	Opt	0.16	0	6	4	0	147.1	0.7541	0.01	0
532	0	6	4	0	147.1	0.7539	Opt	0.16	0	5	5	0	157.6	0.7593	0	0.07135
533	0	10	0	0	105.2	0.7911	Opt	0.17	0	10	0	0	105.2	0.7911	0	0
534	0	10	0	0	105.2	0.7871	Opt	0.161	0	10	0	0	105.2	0.774	0.01	1.9E-05
535	0	9	1	0	115.7	0.7631	Opt	0.17	0	9	1	0	115.7	0.7631	0	0
536	0	9	1	0	115.7	0.7608	Opt	0.16	0	9	1	2	120.7	0.7507	0	0.04322
537	0	6	4	0	147.2	0.7508	Opt	0.16	0	6	4	0	147.2	0.7508	0.01	0
538	0	6	4	1	149.7	0.7503	Opt	0.181	0	5	5	0	157.7	0.7757	0	0.05336
539	0	4	6	0	168.2	0.7809	Opt	0.731	0	4	6	0	168.2	0.7809	0	0
540	0	4	6	0	168.2	0.7789	Opt	0.55	0	4	6	0	168.2	0.7691	0.01	0
541	0	7	3	0	136.8	0.755	Opt	0.171	0	7	3	0	136.8	0.755	0	0
542	0	7	3	0	136.8	0.7539	Opt	0.16	0	6	4	0	147.3	0.7795	0	0.07663
543	0	6	4	0	147.3	0.7558	Opt	0.16	0	6	4	0	147.3	0.7558	0.01	0
544	0	6	4	0	147.3	0.7544	Opt	0.17	0	5	5	0	157.8	0.7753	0	0.07117
545	0	10	0	0	105.2	0.7148	Opt	0.161	0	10	0	0	105.2	0.7148	0	0
546	0	10	0	0	105.2	0.714	Opt	0.17	0	10	0	3	112.7	0.7017	0	0.07133
547	0	8	2	0	126.2	0.7048	Opt	0.16	0	8	2	0	126.2	0.7048	0.01	0
548	0	8	2	0	126.2	0.7059	Opt	0.16	0	7	3	0	136.7	0.7144	0.01	0.08316
549	1	9	0	0	94.96	0.7276	Opt	0.161	1	9	0	0	94.96	0.7276	0	4.6E-05
550	1	9	0	0	94.98	0.7231	Opt	0.16	1	9	0	0	94.98	0.7111	0.01	7.1E-05
551	0	10	0	0	105.3	0.7378	Opt	0.18	0	10	0	0	105.3	0.7378	0	0
552	0	10	0	0	105.3	0.7358	Opt	0.18	0	10	0	0	105.3	0.7242	0	2.8E-05
553	0	7	3	0	136.8	0.7084	Opt	0.171	0	7	3	0	136.8	0.7084	0	0
554	0	7	3	0	136.8	0.7088	Opt	0.17	0	7	3	1	139.3	0.7005	0	0.01829
555	0	6	4	0	147.3	0.7106	Opt	0.17	0	6	4	0	147.3	0.7106	0	0
556	0	6	4	0	147.3	0.7105	Opt	0.18	0	6	4	0	147.3	0.7016	0	1.4E-05
557	0	8	2	0	126.4	0.7188	Opt	0.171	0	8	2	0	126.4	0.7188	0.01	0
558	0	8	2	0	126.5	0.7182	Opt	0.17	0	8	2	0	126.5	0.7105	0	3.2E-05
559	0	7	3	0	136.9	0.7222	Opt	0.23	0	7	3	0	136.9	0.7222	0	0
560	0	7	3	0	136.9	0.7218	Opt	0.21	0	7	3	0	137	0.7144	0.01	2.9E-05
561	0	9	1	0	115.6	0.7515	Opt	0.171	0	9	1	0	115.6	0.7515	0	0
562	0	9	1	1	118.2	0.7514	Opt	0.19	0	8	2	0	126.2	0.7577	0	0.06766
563	0	6	4	0	147.1	0.7541	Opt	0.17	0	6	4	0	147.1	0.7541	0	0
564	0	6	4	0	147.2	0.7539	Opt	0.171	0	5	5	0	157.7	0.7593	0	0.07134
565	0	10	0	0	105.2	0.7911	Opt	0.17	0	10	0	0	105.2	0.7911	0	0
566	0	10	0	0	105.3	0.7871	Opt	0.18	0	10	0	0	105.3	0.774	0	3.8E-05
567	0	9	1	0	115.8	0.7631	Opt	0.16	0	9	1	0	115.8	0.7631	0.01	0
568	0	9	1	0	115.8	0.7608	Opt	0.171	0	9	1	2	120.8	0.7507	0.01	0.0432
569	0	6	4	0	147.3	0.7508	Opt	0.17	0	6	4	0	147.3	0.7508	0	0
570	0	6	4	1	149.8	0.7503	Opt	0.18	0	5	5	0	157.8	0.7757	0	0.05329
571	0	4	6	0	168.3	0.7809	Opt	0.3	0	4	6	0	168.3	0.7809	0	0
572	0	4	6	0	168.3	0.7789	Opt	3.065	0	4	6	0	168.3	0.7691	0.01	1.2E-05
573	0	7	3	0	136.9	0.755	Opt	0.16	0	7	3	0	136.9	0.755	0.01	0
574	0	7	3	0	136.9	0.7539	Opt	0.16	0	6	4	0	147.4	0.7795	0.01	0.0765
575	0	6	4	0	147.4	0.7558	Opt	0.161	0	6	4	0	147.4	0.7558	0.01	0
576	0	6	4	0	147.4	0.7544	Opt	0.17	0	5	5	0	157.9	0.7753	0	0.07104

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
577	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
578	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
579	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
580	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
581	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
582	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
583	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
584	10	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
585	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
586	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
587	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
588	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
589	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
590	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
591	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
592	10	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
593	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
594	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
595	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
596	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
597	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
598	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
599	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
600	10	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
601	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
602	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
603	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
604	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
605	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
606	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
607	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
608	10	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
609	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
610	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
611	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
612	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
613	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
614	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
615	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
616	10	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
617	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
618	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
619	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
620	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
621	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
622	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
623	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
624	10	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
577	0	10	0	0	110.1	0.7148	Opt	0.18	0	10	0	0	110.1	0.7148	0	0
578	0	10	0	0	110.1	0.714	Opt	0.18	0	10	0	3	119.1	0.7017	0	0.08177
579	0	8	2	0	132.1	0.7048	Opt	0.171	0	8	2	0	132.1	0.7048	0	0
580	0	8	2	0	132.1	0.7059	Opt	0.17	0	7	3	0	143.1	0.7144	0	0.08326
581	1	9	0	0	99.23	0.7276	Opt	0.17	1	9	0	0	99.23	0.7276	0	2.2E-05
582	1	9	0	0	99.24	0.7231	Opt	0.16	1	9	0	0	99.24	0.7111	0.01	3.4E-05
583	0	10	0	0	110.1	0.7378	Opt	0.171	0	10	0	0	110.1	0.7378	0	0
584	0	10	0	0	110.1	0.7358	Opt	0.17	0	10	0	0	110.1	0.7242	0.01	1.8E-05
585	0	7	3	0	143.1	0.7084	Opt	0.17	0	7	3	0	143.1	0.7084	0	0
586	0	7	3	0	143.2	0.7088	Opt	0.17	0	7	3	1	146.2	0.7005	0	0.02096
587	0	6	4	0	154.2	0.7106	Opt	0.181	0	6	4	0	154.2	0.7106	0	0
588	0	6	4	0	154.2	0.7105	Opt	0.19	0	6	4	0	154.2	0.7016	0	6.5E-06
589	0	8	2	0	132.2	0.7188	Opt	0.17	0	8	2	0	132.2	0.7188	0	0
590	0	8	2	0	132.2	0.7182	Opt	0.18	0	8	2	0	132.2	0.7105	0	1.5E-05
591	0	7	3	0	143.2	0.7222	Opt	0.201	0	7	3	0	143.2	0.7222	0	0
592	0	7	3	0	143.2	0.7218	Opt	0.21	0	7	3	0	143.2	0.7144	0.01	1.4E-05
593	0	9	1	0	121.1	0.7515	Opt	0.16	0	9	1	0	121.1	0.7515	0.01	0
594	0	9	1	1	124.1	0.7514	Opt	0.181	0	8	2	0	132.1	0.7577	0.01	0.06446
595	0	6	4	0	154.1	0.7541	Opt	0.17	0	6	4	0	154.1	0.7541	0	0
596	0	6	4	0	154.1	0.7539	Opt	0.16	0	5	5	0	165.1	0.7593	0.01	0.07138
597	0	10	0	0	110.1	0.7911	Opt	0.17	0	10	0	0	110.1	0.7911	0.01	0
598	0	10	0	0	110.1	0.7871	Opt	0.181	0	10	0	0	110.1	0.774	0	1.8E-05
599	0	9	1	0	121.1	0.7631	Opt	0.17	0	9	1	0	121.1	0.7631	0	0
600	0	9	1	0	121.1	0.7608	Opt	0.18	0	9	1	2	127.1	0.7507	0	0.04954
601	0	6	4	0	154.1	0.7508	Opt	0.17	0	6	4	0	154.1	0.7508	0	0
602	0	6	4	1	157.1	0.7503	Opt	0.191	0	5	5	0	165.1	0.7757	0	0.05085
603	0	4	6	0	176.1	0.7809	Opt	0.33	0	4	6	0	176.1	0.7809	0	0
604	0	4	6	0	176.1	0.7789	Opt	1.212	0	4	6	0	176.1	0.7691	0	0
605	0	7	3	0	143.2	0.755	Opt	0.17	0	7	3	0	143.2	0.755	0	0
606	0	7	3	0	143.2	0.7539	Opt	0.17	0	6	4	0	154.2	0.7795	0	0.07672
607	0	6	4	0	154.2	0.7558	Opt	0.17	0	6	4	0	154.2	0.7558	0	0
608	0	6	4	0	154.2	0.7544	Opt	0.181	0	5	5	0	165.2	0.7753	0	0.07125
609	0	10	0	0	110.1	0.7148	Opt	0.17	0	10	0	0	110.1	0.7148	0	0
610	0	10	0	0	110.1	0.714	Opt	0.17	0	10	0	3	119.1	0.7017	0.01	0.08175
611	0	8	2	0	132.1	0.7048	Opt	0.17	0	8	2	0	132.1	0.7048	0	0
612	0	8	2	0	132.1	0.7059	Opt	0.17	0	7	3	0	143.1	0.7144	0.011	0.08322
613	1	9	0	0	99.39	0.7276	Opt	0.17	1	9	0	0	99.39	0.7276	0	4.4E-05
614	1	9	0	0	99.41	0.7231	Opt	0.17	1	9	0	0	99.41	0.7111	0.01	6.7E-05
615	0	10	0	0	110.2	0.7378	Opt	0.181	0	10	0	0	110.2	0.7378	0	0
616	0	10	0	0	110.2	0.7358	Opt	0.18	0	10	0	0	110.2	0.7242	0	2.7E-05
617	0	7	3	0	143.2	0.7084	Opt	0.18	0	7	3	0	143.2	0.7084	0	0
618	0	7	3	0	143.2	0.7088	Opt	0.18	0	7	3	1	146.2	0.7005	0	0.02096
619	0	6	4	0	154.2	0.7106	Opt	0.181	0	6	4	0	154.2	0.7106	0	0
620	0	6	4	0	154.2	0.7105	Opt	0.19	0	6	4	0	154.2	0.7016	0	1.3E-05
621	0	8	2	0	132.3	0.7188	Opt	0.18	0	8	2	0	132.3	0.7188	0	0
622	0	8	2	0	132.3	0.7182	Opt	0.18	0	8	2	0	132.3	0.7105	0	3E-05
623	0	7	3	0	143.3	0.7222	Opt	0.201	0	7	3	0	143.3	0.7222	0	0
624	0	7	3	0	143.3	0.7218	Opt	0.19	0	7	3	0	143.3	0.7144	0	2.8E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
625	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
626	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
627	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
628	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
629	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
630	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
631	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
632	10	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
633	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
634	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
635	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
636	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
637	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
638	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
639	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
640	10	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
641	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
642	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
643	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
644	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
645	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
646	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
647	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
648	10	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
649	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
650	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
651	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
652	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
653	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
654	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
655	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
656	10	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
657	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
658	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
659	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
660	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
661	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
662	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
663	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
664	10	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
665	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
666	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
667	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
668	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
669	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
670	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
671	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
672	10	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
625	0	9	1	0	121.1	0.7515	Opt	0.18	0	9	1	0	121.1	0.7515	0	0
626	0	9	1	1	124.1	0.7514	Opt	0.19	0	8	2	0	132.1	0.7577	0	0.06442
627	0	6	4	0	154.1	0.7541	Opt	0.171	0	6	4	0	154.1	0.7541	0	0
628	0	6	4	0	154.1	0.7539	Opt	0.17	0	5	5	0	165.1	0.7593	0.01	0.07137
629	0	10	0	0	110.2	0.7911	Opt	0.18	0	10	0	0	110.2	0.7911	0	0
630	0	10	0	0	110.2	0.7871	Opt	0.17	0	10	0	0	110.2	0.774	0.01	3.6E-05
631	0	9	1	0	121.2	0.7631	Opt	0.171	0	9	1	0	121.2	0.7631	0.01	0
632	0	9	1	0	121.2	0.7608	Opt	0.18	0	9	1	2	127.2	0.7507	0.01	0.04953
633	0	6	4	0	154.2	0.7508	Opt	0.17	0	6	4	0	154.2	0.7508	0	0
634	0	6	4	1	157.2	0.7503	Opt	0.181	0	5	5	0	165.2	0.7757	0.01	0.05079
635	0	4	6	0	176.2	0.7809	Opt	0.5	0	4	6	0	176.2	0.7809	0.01	0
636	0	4	6	0	176.2	0.7789	Opt	0.611	0	4	6	0	176.2	0.7691	0	1.1E-05
637	0	7	3	0	143.3	0.755	Opt	0.18	0	7	3	0	143.3	0.755	0	0
638	0	7	3	0	143.3	0.7539	Opt	0.181	0	6	4	0	154.3	0.7795	0	0.0766
639	0	6	4	0	154.3	0.7558	Opt	0.17	0	6	4	0	154.3	0.7558	0	0
640	0	6	4	0	154.3	0.7544	Opt	0.17	0	5	5	0	165.3	0.7753	0.01	0.07113
641	0	10	0	0	110.1	0.7148	Opt	0.17	0	10	0	0	110.1	0.7148	0.01	0
642	0	10	0	0	110.1	0.714	Opt	0.191	0	10	0	3	119.1	0.7017	0	0.08174
643	0	8	2	0	132.1	0.7048	Opt	0.17	0	8	2	0	132.1	0.7048	0	0
644	0	8	2	0	132.1	0.7059	Opt	0.18	0	7	3	0	143.1	0.7144	0.01	0.08323
645	1	9	0	0	99.25	0.7276	Opt	0.17	1	9	0	0	99.25	0.7276	0	2.2E-05
646	1	9	0	0	99.26	0.7231	Opt	0.171	1	9	0	0	99.26	0.7111	0.01	3.4E-05
647	0	10	0	0	110.2	0.7378	Opt	0.18	0	10	0	0	110.2	0.7378	0.01	0
648	0	10	0	0	110.2	0.7358	Opt	0.18	0	10	0	0	110.2	0.7242	0	1.8E-05
649	0	7	3	0	143.2	0.7084	Opt	0.17	0	7	3	0	143.2	0.7084	0.01	0
650	0	7	3	0	143.2	0.7088	Opt	0.17	0	7	3	1	146.2	0.7005	0.011	0.02096
651	0	6	4	0	154.2	0.7106	Opt	0.17	0	6	4	0	154.2	0.7106	0.01	0
652	0	6	4	0	154.2	0.7105	Opt	0.19	0	6	4	0	154.2	0.7016	0.01	6.5E-06
653	0	8	2	0	132.3	0.7188	Opt	0.181	0	8	2	0	132.3	0.7188	0	0
654	0	8	2	0	132.3	0.7182	Opt	0.18	0	8	2	0	132.3	0.7105	0.01	1.5E-05
655	0	7	3	0	143.3	0.7222	Opt	0.21	0	7	3	0	143.3	0.7222	0	0
656	0	7	3	0	143.3	0.7218	Opt	0.21	0	7	3	0	143.3	0.7144	0	1.4E-05
657	0	9	1	0	121.1	0.7515	Opt	0.181	0	9	1	0	121.1	0.7515	0	0
658	0	9	1	1	124.1	0.7514	Opt	0.19	0	8	2	0	132.1	0.7577	0	0.06443
659	0	6	4	0	154.1	0.7541	Opt	0.18	0	6	4	0	154.1	0.7541	0.01	0
660	0	6	4	0	154.1	0.7539	Opt	0.181	0	5	5	0	165.1	0.7593	0	0.07136
661	0	10	0	0	110.1	0.7911	Opt	0.18	0	10	0	0	110.1	0.7911	0	0
662	0	10	0	0	110.2	0.7871	Opt	0.18	0	10	0	0	110.2	0.774	0	9.1E-06
663	0	9	1	0	121.2	0.7631	Opt	0.19	0	9	1	0	121.2	0.7631	0.01	0
664	0	9	1	0	121.2	0.7608	Opt	0.181	0	9	1	2	127.2	0.7507	0	0.04953
665	0	6	4	0	154.2	0.7508	Opt	0.17	0	6	4	0	154.2	0.7508	0.01	0
666	0	6	4	1	157.2	0.7503	Opt	0.19	0	5	5	0	165.2	0.7757	0.01	0.05081
667	0	4	6	0	176.2	0.7809	Opt	0.441	0	4	6	0	176.2	0.7809	0	0
668	0	4	6	0	176.2	0.7789	Opt	1.923	0	4	6	0	176.2	0.7691	0.01	5.7E-06
669	0	7	3	0	143.2	0.755	Opt	0.18	0	7	3	0	143.2	0.755	0	0
670	0	7	3	0	143.2	0.7539	Opt	0.18	0	6	4	0	154.2	0.7795	0	0.07667
671	0	6	4	0	154.2	0.7558	Opt	0.18	0	6	4	0	154.2	0.7558	0.01	0
672	0	6	4	0	154.2	0.7544	Opt	0.181	0	5	5	0	165.2	0.7753	0	0.0712

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
673	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
674	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
675	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
676	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
677	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
678	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
679	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
680	10	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
681	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
682	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
683	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
684	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
685	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
686	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
687	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
688	10	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
689	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
690	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
691	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
692	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
693	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
694	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
695	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
696	10	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
697	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
698	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
699	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
700	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
701	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
702	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
703	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
704	10	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
705	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
706	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
707	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
708	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
709	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
710	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
711	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
712	10	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
713	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
714	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
715	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
716	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
717	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
718	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
719	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
720	10	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
673	0	10	0	0	110.1	0.7148	Opt	0.18	0	10	0	0	110.1	0.7148	0	0
674	0	10	0	0	110.1	0.714	Opt	0.19	0	10	0	3	119.1	0.7017	0	0.08173
675	0	8	2	0	132.1	0.7048	Opt	0.18	0	8	2	0	132.1	0.7048	0	0
676	0	8	2	0	132.1	0.7059	Opt	0.181	0	7	3	0	143.1	0.7144	0.01	0.08319
677	1	9	0	0	99.41	0.7276	Opt	0.18	1	9	0	0	99.41	0.7276	0	4.4E-05
678	1	9	0	0	99.43	0.7231	Opt	0.18	1	9	0	0	99.42	0.7111	0.01	6.7E-05
679	0	10	0	0	110.2	0.7378	Opt	0.2	0	10	0	0	110.2	0.7378	0	0
680	0	10	0	0	110.2	0.7358	Opt	0.191	0	10	0	0	110.2	0.7242	0	2.7E-05
681	0	7	3	0	143.2	0.7084	Opt	0.18	0	7	3	0	143.2	0.7084	0.01	0
682	0	7	3	0	143.2	0.7088	Opt	0.18	0	7	3	1	146.2	0.7005	0	0.02096
683	0	6	4	0	154.2	0.7106	Opt	0.181	0	6	4	0	154.2	0.7106	0.01	0
684	0	6	4	0	154.2	0.7105	Opt	0.2	0	6	4	0	154.2	0.7016	0	1.9E-05
685	0	8	2	0	132.4	0.7188	Opt	0.19	0	8	2	0	132.4	0.7188	0	0
686	0	8	2	0	132.4	0.7182	Opt	0.19	0	8	2	0	132.4	0.7105	0	3E-05
687	0	7	3	0	143.3	0.7222	Opt	0.221	0	7	3	0	143.3	0.7222	0	0
688	0	7	3	0	143.4	0.7218	Opt	0.22	0	7	3	0	143.4	0.7144	0	2.1E-05
689	0	9	1	0	121.1	0.7515	Opt	0.18	0	9	1	0	121.1	0.7515	0.01	0
690	0	9	1	1	124.1	0.7514	Opt	0.201	0	8	2	0	132.1	0.7577	0	0.0644
691	0	6	4	0	154.1	0.7541	Opt	0.18	0	6	4	0	154.1	0.7541	0	0
692	0	6	4	0	154.1	0.7539	Opt	0.18	0	5	5	0	165.1	0.7593	0.01	0.07135
693	0	10	0	0	110.2	0.7911	Opt	0.19	0	10	0	0	110.2	0.7911	0	0
694	0	10	0	0	110.2	0.7871	Opt	0.191	0	10	0	0	110.2	0.774	0.01	2.7E-05
695	0	9	1	0	121.2	0.7631	Opt	0.19	0	9	1	0	121.2	0.7631	0	0
696	0	9	1	0	121.2	0.7608	Opt	0.19	0	9	1	2	127.2	0.7507	0	0.04952
697	0	6	4	0	154.2	0.7508	Opt	0.18	0	6	4	0	154.2	0.7508	0	0
698	0	6	4	1	157.2	0.7503	Opt	0.19	0	5	5	0	165.2	0.7757	0.011	0.05075
699	0	4	6	0	176.2	0.7809	Opt	0.33	0	4	6	0	176.2	0.7809	0.01	0
700	0	4	6	0	176.2	0.7789	Opt	0.922	0	4	6	0	176.2	0.7691	0	5.7E-06
701	0	7	3	0	143.3	0.755	Opt	0.18	0	7	3	0	143.3	0.755	0.01	0
702	0	7	3	0	143.3	0.7539	Opt	0.19	0	6	4	0	154.3	0.7795	0	0.07654
703	0	6	4	0	154.3	0.7558	Opt	0.18	0	6	4	0	154.3	0.7558	0	0
704	0	6	4	0	154.3	0.7544	Opt	0.181	0	5	5	0	165.3	0.7753	0.01	0.07108
705	0	10	0	0	110.1	0.7148	Opt	0.18	0	10	0	0	110.1	0.7148	0.01	0
706	0	10	0	0	110.1	0.714	Opt	0.2	0	10	0	3	119.1	0.7017	0	0.08172
707	0	8	2	0	132.1	0.7048	Opt	0.191	0	8	2	0	132.1	0.7048	0	0
708	0	8	2	0	132.1	0.7059	Opt	0.19	0	7	3	0	143.1	0.7144	0	0.08321
709	1	9	0	0	99.3	0.7276	Opt	0.19	1	9	0	0	99.3	0.7276	0	2.2E-05
710	1	9	0	0	99.31	0.7231	Opt	0.18	1	9	0	0	99.31	0.7111	0	3.4E-05
711	0	10	0	0	110.2	0.7378	Opt	0.191	0	10	0	0	110.2	0.7378	0.01	0
712	0	10	0	0	110.2	0.7358	Opt	0.19	0	10	0	0	110.2	0.7242	0	1.8E-05
713	0	7	3	0	143.3	0.7084	Opt	0.19	0	7	3	0	143.3	0.7084	0	0
714	0	7	3	0	143.3	0.7088	Opt	0.19	0	7	3	1	146.3	0.7005	0	0.02095
715	0	6	4	0	154.3	0.7106	Opt	0.201	0	6	4	0	154.3	0.7106	0	0
716	0	6	4	0	154.3	0.7105	Opt	0.21	0	6	4	0	154.3	0.7016	0	6.5E-06
717	0	8	2	0	132.3	0.7188	Opt	0.19	0	8	2	0	132.3	0.7188	0	0
718	0	8	2	0	132.4	0.7182	Opt	0.191	0	8	2	0	132.4	0.7105	0	1.5E-05
719	0	7	3	0	143.3	0.7222	Opt	0.21	0	7	3	0	143.3	0.7222	0.01	0
720	0	7	3	0	143.4	0.7218	Opt	0.23	0	7	3	0	143.4	0.7144	0.01	7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
721	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
722	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
723	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
724	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
725	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
726	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
727	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
728	10	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
729	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
730	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
731	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
732	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
733	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
734	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
735	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
736	10	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
737	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
738	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
739	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
740	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
741	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
742	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
743	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
744	10	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
745	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
746	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
747	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
748	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
749	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
750	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
751	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
752	10	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
753	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
754	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
755	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
756	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
757	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
758	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
759	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
760	10	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
761	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
762	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
763	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
764	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
765	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
766	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
767	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
768	10	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
721	0	9	1	0	121.1	0.7515	Opt	0.19	0	9	1	0	121.1	0.7515	0	0
722	0	9	1	1	124.1	0.7514	Opt	0.201	0	8	2	0	132.1	0.7577	0	0.06442
723	0	6	4	0	154.1	0.7541	Opt	0.19	0	6	4	0	154.1	0.7541	0.01	0
724	0	6	4	0	154.1	0.7539	Opt	0.19	0	5	5	0	165.1	0.7593	0	0.07135
725	0	10	0	0	110.2	0.7911	Opt	0.191	0	10	0	0	110.2	0.7911	0	0
726	0	10	0	0	110.2	0.7871	Opt	0.2	0	10	0	0	110.2	0.774	0	1.8E-05
727	0	9	1	0	121.2	0.7631	Opt	0.19	0	9	1	0	121.2	0.7631	0.01	0
728	0	9	1	0	121.2	0.7608	Opt	0.19	0	9	1	2	127.2	0.7507	0	0.0495
729	0	6	4	0	154.2	0.7508	Opt	0.191	0	6	4	0	154.2	0.7508	0	0
730	0	6	4	1	157.2	0.7503	Opt	0.21	0	5	5	0	165.2	0.7757	0	0.05082
731	0	4	6	0	176.2	0.7809	Opt	0.341	0	4	6	0	176.2	0.7809	0	0
732	0	4	6	0	176.2	0.7789	Opt	1.161	0	4	6	0	176.2	0.7691	0.01	0
733	0	7	3	0	143.3	0.755	Opt	0.19	0	7	3	0	143.3	0.755	0	0
734	0	7	3	0	143.3	0.7539	Opt	0.191	0	6	4	0	154.3	0.7795	0	0.07665
735	0	6	4	0	154.3	0.7558	Opt	0.19	0	6	4	0	154.3	0.7558	0.01	0
736	0	6	4	0	154.3	0.7544	Opt	0.19	0	5	5	0	165.3	0.7753	0	0.07118
737	0	10	0	0	110.2	0.7148	Opt	0.191	0	10	0	0	110.2	0.7148	0	0
738	0	10	0	0	110.2	0.714	Opt	0.2	0	10	0	3	119.2	0.7017	0.01	0.08171
739	0	8	2	0	132.2	0.7048	Opt	0.19	0	8	2	0	132.2	0.7048	0	0
740	0	8	2	0	132.2	0.7059	Opt	0.19	0	7	3	0	143.2	0.7144	0.01	0.08317
741	1	9	0	0	99.46	0.7276	Opt	0.191	1	9	0	0	99.46	0.7276	0	4.4E-05
742	1	9	0	0	99.48	0.7231	Opt	0.19	1	9	0	0	99.48	0.7111	0	6.7E-05
743	0	10	0	0	110.3	0.7378	Opt	0.2	0	10	0	0	110.3	0.7378	0.01	0
744	0	10	0	0	110.3	0.7358	Opt	0.191	0	10	0	0	110.3	0.7242	0.01	2.7E-05
745	0	7	3	0	143.3	0.7084	Opt	0.2	0	7	3	0	143.3	0.7084	0	0
746	0	7	3	0	143.3	0.7088	Opt	0.19	0	7	3	1	146.3	0.7005	0	0.02095
747	0	6	4	0	154.3	0.7106	Opt	0.19	0	6	4	0	154.3	0.7106	0.01	0
748	0	6	4	0	154.3	0.7105	Opt	0.211	0	6	4	0	154.3	0.7016	0.01	1.3E-05
749	0	8	2	0	132.4	0.7188	Opt	0.19	0	8	2	0	132.4	0.7188	0	0
750	0	8	2	0	132.5	0.7182	Opt	0.2	0	8	2	0	132.5	0.7105	0.01	3E-05
751	0	7	3	0	143.4	0.7222	Opt	0.221	0	7	3	0	143.4	0.7222	0	0
752	0	7	3	0	143.4	0.7218	Opt	0.25	0	7	3	0	143.5	0.7144	0	2.8E-05
753	0	9	1	0	121.1	0.7515	Opt	0.19	0	9	1	0	121.1	0.7515	0.01	0
754	0	9	1	1	124.2	0.7514	Opt	0.211	0	8	2	0	132.2	0.7577	0	0.06439
755	0	6	4	0	154.1	0.7541	Opt	0.19	0	6	4	0	154.1	0.7541	0	0
756	0	6	4	0	154.2	0.7539	Opt	0.2	0	5	5	0	165.2	0.7593	0	0.07134
757	0	10	0	0	110.2	0.7911	Opt	0.2	0	10	0	0	110.2	0.7911	0	0
758	0	10	0	0	110.3	0.7871	Opt	0.201	0	10	0	0	110.3	0.774	0	3.6E-05
759	0	9	1	0	121.3	0.7631	Opt	0.19	0	9	1	0	121.3	0.7631	0	0
760	0	9	1	0	121.3	0.7608	Opt	0.19	0	9	1	2	127.3	0.7507	0.01	0.04949
761	0	6	4	0	154.3	0.7508	Opt	0.191	0	6	4	0	154.3	0.7508	0.01	0
762	0	6	4	1	157.3	0.7503	Opt	0.21	0	5	5	0	165.3	0.7757	0	0.05075
763	0	4	6	0	176.3	0.7809	Opt	0.511	0	4	6	0	176.3	0.7809	0	0
764	0	4	6	0	176.3	0.7789	Opt	1.942	0	4	6	0	176.3	0.7691	0.01	1.1E-05
765	0	7	3	0	143.4	0.755	Opt	0.191	0	7	3	0	143.4	0.755	0	0
766	0	7	3	0	143.4	0.7539	Opt	0.19	0	6	4	0	154.4	0.7795	0	0.07652
767	0	6	4	0	154.4	0.7558	Opt	0.19	0	6	4	0	154.4	0.7558	0.01	0
768	0	6	4	0	154.4	0.7544	Opt	0.191	0	5	5	0	165.4	0.7753	0.01	0.07106

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
769	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
770	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
771	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
772	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
773	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
774	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
775	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
776	20	1	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
777	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
778	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
779	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
780	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
781	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
782	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
783	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
784	20	1	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
785	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
786	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
787	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
788	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
789	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
790	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
791	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
792	20	1	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
793	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
794	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
795	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
796	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
797	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
798	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
799	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
800	20	1	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
801	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
802	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
803	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
804	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
805	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
806	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
807	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
808	20	1	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
809	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
810	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
811	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
812	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
813	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
814	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
815	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
816	20	1	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
769	0	10	0	0	205.1	0.7148	Opt	0.22	0	10	0	0	205.1	0.7148	0	0
770	1	9	0	12	202.6	0.7004	Opt	0.3	0	10	0	3	209.6	0.7017	0	0.0343
771	0	8	2	0	246.1	0.7048	Opt	0.201	0	8	2	0	246.1	0.7048	0	0
772	0	9	1	13	245.1	0.7002	Opt	0.31	0	7	3	0	266.6	0.7144	0	0.0877
773	1	9	0	0	184.7	0.7276	Opt	0.2	1	9	0	0	184.7	0.7276	0.01	1.1E-05
774	1	9	0	0	184.7	0.7231	Opt	0.191	1	9	0	0	184.7	0.7111	0	1.6E-05
775	0	10	0	0	205.1	0.7378	Opt	0.21	0	10	0	0	205.1	0.7378	0	0
776	0	10	0	0	205.1	0.7358	Opt	0.2	0	10	0	0	205.1	0.7242	0	9.7E-06
777	0	7	3	0	266.6	0.7084	Opt	0.201	0	7	3	0	266.6	0.7084	0	0
778	0	7	3	0	266.7	0.7088	Opt	0.2	0	7	3	1	268.2	0.7005	0	0.00563
779	0	6	4	0	287.2	0.7106	Opt	0.23	0	6	4	0	287.2	0.7106	0	0
780	0	6	4	0	287.2	0.7105	Opt	0.2	0	6	4	0	287.2	0.7016	0	3.5E-06
781	0	8	2	0	246.2	0.7188	Opt	0.201	0	8	2	0	246.2	0.7188	0	0
782	0	8	2	0	246.2	0.7159	Opt	0.32	0	8	2	0	246.2	0.7105	0.01	1.2E-05
783	0	7	3	0	266.7	0.7222	Opt	0.241	0	7	3	0	266.7	0.7222	0	0
784	0	7	3	0	266.7	0.7218	Opt	0.22	0	7	3	0	266.7	0.7144	0	7.5E-06
785	0	9	1	0	225.6	0.7515	Opt	0.2	0	9	1	0	225.6	0.7515	0	0
786	0	9	1	1	227.1	0.7514	Opt	0.221	0	8	2	0	246.1	0.7577	0	0.08366
787	0	6	4	0	287.1	0.7541	Opt	0.2	0	6	4	0	287.1	0.7541	0	0
788	0	6	4	0	287.1	0.7539	Opt	0.38	0	5	5	0	307.6	0.7593	0	0.0714
789	0	10	0	0	205.1	0.7911	Opt	0.211	0	10	0	0	205.1	0.7911	0	0
790	0	10	0	0	205.1	0.7871	Opt	0.2	0	10	0	0	205.1	0.774	0.01	9.7E-06
791	0	9	1	0	225.6	0.7631	Opt	0.2	0	9	1	0	225.6	0.7631	0	0
792	0	9	1	0	225.6	0.7608	Opt	0.391	0	9	1	2	228.6	0.7507	0	0.0133
793	0	6	4	0	287.1	0.7508	Opt	0.2	0	6	4	0	287.1	0.7508	0	0
794	0	6	4	1	288.6	0.7503	Opt	0.2	0	5	5	0	307.6	0.7757	0.01	0.06579
795	0	4	6	0	328.1	0.7809	Opt	6.109	0	4	6	0	328.1	0.7809	0.01	0
796	0	5	5	5	315.1	0.7501	Opt	0.291	0	4	6	0	328.1	0.7691	0	0.04123
797	0	7	3	0	266.7	0.755	Opt	0.2	0	7	3	0	266.7	0.755	0	0
798	0	7	3	0	266.7	0.7539	Opt	0.2	0	6	4	0	287.2	0.7795	0.01	0.07681
799	0	6	4	0	287.2	0.7558	Opt	0.21	0	6	4	0	287.2	0.7558	0	0
800	0	6	4	0	287.2	0.7544	Opt	0.201	0	5	5	0	307.7	0.7753	0	0.07133
801	0	10	0	0	205.1	0.7148	Opt	0.22	0	10	0	0	205.1	0.7148	0.01	0
802	1	9	0	12	202.7	0.7001	Opt	0.311	0	10	0	3	209.6	0.7017	0	0.03401
803	0	8	2	0	246.1	0.7048	Opt	0.2	0	8	2	0	246.1	0.7048	0.01	0
804	0	9	1	13	245.1	0.7006	Opt	0.38	0	7	3	0	266.6	0.7144	0	0.08767
805	1	9	0	0	184.9	0.7276	Opt	0.201	1	9	0	0	184.9	0.7276	0.01	2.2E-05
806	1	9	0	0	184.9	0.7231	Opt	0.2	1	9	0	0	184.9	0.7111	0	3.8E-05
807	0	10	0	0	205.2	0.7378	Opt	0.22	0	10	0	0	205.2	0.7378	0.01	0
808	0	10	0	0	205.2	0.7358	Opt	0.211	0	10	0	0	205.2	0.7242	0	1.5E-05
809	0	7	3	0	266.7	0.7084	Opt	0.21	0	7	3	0	266.7	0.7084	0.01	0
810	0	7	3	0	266.7	0.7088	Opt	0.2	0	7	3	1	268.2	0.7005	0	0.00563
811	0	6	4	0	287.2	0.7058	Opt	0.321	0	6	4	0	287.2	0.7106	0.01	3.5E-06
812	0	6	4	0	287.2	0.7105	Opt	0.23	0	6	4	0	287.2	0.7016	0	7E-06
813	0	8	2	0	246.3	0.7188	Opt	0.2	0	8	2	0	246.3	0.7188	0.01	0
814	0	8	2	0	246.3	0.7159	Opt	0.341	0	8	2	0	246.3	0.7105	0.01	2.8E-05
815	0	7	3	0	266.8	0.7222	Opt	0.23	0	7	3	0	266.8	0.7222	0	0
816	0	7	3	0	266.8	0.7218	Opt	0.231	0	7	3	0	266.8	0.7144	0	1.5E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
817	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
818	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
819	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
820	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
821	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
822	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
823	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
824	20	1	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
825	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
826	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
827	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
828	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
829	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
830	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
831	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
832	20	1	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
833	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
834	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
835	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
836	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
837	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
838	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
839	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
840	20	1	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
841	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
842	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
843	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
844	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
845	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
846	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
847	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
848	20	1	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
849	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
850	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
851	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
852	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
853	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
854	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
855	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
856	20	1	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
857	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
858	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
859	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
860	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
861	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
862	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
863	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
864	20	1	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
817	0	9	1	0	225.6	0.7515	Opt	0.2	0	9	1	0	225.6	0.7515	0	0
818	0	9	1	1	227.1	0.7514	Opt	0.21	0	8	2	0	246.1	0.7577	0.01	0.08364
819	0	6	4	0	287.1	0.7541	Opt	0.2	0	6	4	0	287.1	0.7541	0.01	0
820	0	6	4	0	287.1	0.7539	Opt	0.401	0	5	5	0	307.6	0.7593	0	0.0714
821	0	10	0	0	205.2	0.7911	Opt	0.21	0	10	0	0	205.2	0.7911	0.01	0
822	0	10	0	0	205.2	0.7871	Opt	0.211	0	10	0	0	205.2	0.774	0	1.9E-05
823	0	9	1	0	225.7	0.7631	Opt	0.22	0	9	1	0	225.7	0.7631	0	0
824	0	9	1	0	225.7	0.7608	Opt	0.39	0	9	1	2	228.7	0.7507	0	0.01331
825	0	6	4	0	287.2	0.7508	Opt	0.211	0	6	4	0	287.2	0.7508	0	0
826	0	6	4	1	288.7	0.7503	Opt	0.21	0	5	5	0	307.7	0.7757	0	0.06576
827	0	4	6	0	328.2	0.7809	Opt	4.947	0	4	6	0	328.2	0.7809	0.01	0
828	0	5	5	5	315.2	0.7501	Opt	0.421	0	4	6	0	328.2	0.7691	0.01	0.0412
829	0	7	3	0	266.8	0.755	Opt	0.21	0	7	3	0	266.8	0.755	0	0
830	0	7	3	0	266.8	0.7539	Opt	0.21	0	6	4	0	287.3	0.7795	0	0.07675
831	0	6	4	0	287.3	0.7558	Opt	0.211	0	6	4	0	287.3	0.7558	0	0
832	0	6	4	0	287.3	0.7544	Opt	0.21	0	5	5	0	307.8	0.7753	0	0.07127
833	0	10	0	0	205.1	0.7148	Opt	0.21	0	10	0	0	205.1	0.7148	0	0
834	1	9	0	12	202.6	0.7002	Opt	0.351	0	10	0	3	209.6	0.7017	0	0.03431
835	0	8	2	0	246.1	0.7048	Opt	0.21	0	8	2	0	246.1	0.7048	0	0
836	0	9	1	13	245.1	0.7005	Opt	0.381	0	7	3	0	266.6	0.7144	0	0.08769
837	1	9	0	0	184.7	0.7276	Opt	0.21	1	9	0	0	184.7	0.7276	0	1.1E-05
838	1	9	0	0	184.8	0.7231	Opt	0.2	1	9	0	0	184.8	0.7111	0.01	1.6E-05
839	0	10	0	0	205.2	0.7378	Opt	0.201	0	10	0	0	205.2	0.7378	0.01	0
840	0	10	0	0	205.2	0.7358	Opt	0.21	0	10	0	0	205.2	0.7242	0.01	9.7E-06
841	0	7	3	0	266.7	0.7084	Opt	0.21	0	7	3	0	266.7	0.7084	0.01	0
842	0	7	3	0	266.7	0.7088	Opt	0.211	0	7	3	1	268.2	0.7005	0	0.00563
843	0	6	4	0	287.2	0.7106	Opt	0.23	0	6	4	0	287.2	0.7106	0	0
844	0	6	4	0	287.2	0.7105	Opt	0.21	0	6	4	0	287.2	0.7016	0	3.5E-06
845	0	8	2	0	246.3	0.7188	Opt	0.21	0	8	2	0	246.3	0.7188	0	0
846	0	8	2	0	246.3	0.7159	Opt	0.36	0	8	2	0	246.3	0.7105	0.011	1.2E-05
847	0	7	3	0	266.8	0.7222	Opt	0.24	0	7	3	0	266.8	0.7222	0	0
848	0	7	3	0	266.8	0.7218	Opt	0.251	0	7	3	0	266.8	0.7144	0	7.5E-06
849	0	9	1	0	225.6	0.7515	Opt	0.21	0	9	1	0	225.6	0.7515	0.01	0
850	0	9	1	1	227.1	0.7514	Opt	0.22	0	8	2	0	246.1	0.7577	0	0.08364
851	0	6	4	0	287.1	0.7541	Opt	0.201	0	6	4	0	287.1	0.7541	0.01	0
852	0	6	4	0	287.1	0.7539	Opt	0.37	0	5	5	0	307.6	0.7593	0.01	0.07139
853	0	10	0	0	205.1	0.7911	Opt	0.221	0	10	0	0	205.1	0.7911	0	0
854	0	10	0	0	205.2	0.7871	Opt	0.21	0	10	0	0	205.2	0.774	0	4.9E-06
855	0	9	1	0	225.7	0.7631	Opt	0.22	0	9	1	0	225.7	0.7631	0	0
856	0	9	1	0	225.7	0.7608	Opt	0.301	0	9	1	2	228.7	0.7507	0	0.0133
857	0	6	4	0	287.2	0.7508	Opt	0.21	0	6	4	0	287.2	0.7508	0	0
858	0	6	4	1	288.7	0.7503	Opt	0.22	0	5	5	0	307.7	0.7757	0	0.06577
859	0	4	6	0	328.2	0.7809	Opt	6.85	0	4	6	0	328.2	0.7809	0	0
860	0	5	5	5	315.2	0.7501	Opt	0.471	0	4	6	0	328.2	0.7691	0	0.04121
861	0	7	3	0	266.7	0.755	Opt	0.21	0	7	3	0	266.7	0.755	0	0
862	0	7	3	0	266.7	0.7539	Opt	0.21	0	6	4	0	287.2	0.7795	0.01	0.07678
863	0	6	4	0	287.2	0.7558	Opt	0.211	0	6	4	0	287.2	0.7558	0	0
864	0	6	4	0	287.2	0.7544	Opt	0.21	0	5	5	0	307.7	0.7753	0	0.07131

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
865	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
866	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
867	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
868	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
869	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
870	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
871	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
872	20	1	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
873	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
874	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
875	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
876	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
877	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
878	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
879	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
880	20	1	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
881	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
882	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
883	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
884	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
885	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
886	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
887	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
888	20	1	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
889	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
890	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
891	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
892	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
893	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
894	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
895	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
896	20	1	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
897	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
898	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
899	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
900	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
901	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
902	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
903	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
904	20	1	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
905	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
906	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
907	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
908	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
909	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
910	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
911	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
912	20	1	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
865	0	10	0	0	205.1	0.7148	Opt	0.21	0	10	0	0	205.1	0.7148	0.01	0
866	1	9	0	12	202.7	0.7001	Opt	0.331	0	10	0	3	209.6	0.7017	0	0.03403
867	0	8	2	0	246.1	0.7048	Opt	0.21	0	8	2	0	246.1	0.7048	0	0
868	0	9	1	13	245.1	0.7006	Opt	0.391	0	7	3	0	266.6	0.7144	0	0.08766
869	1	9	0	0	184.9	0.7276	Opt	0.21	1	9	0	0	184.9	0.7276	0	2.2E-05
870	1	9	0	0	184.9	0.7231	Opt	0.21	1	9	0	0	184.9	0.7111	0.01	3.8E-05
871	0	10	0	0	205.2	0.7378	Opt	0.211	0	10	0	0	205.2	0.7378	0	0
872	0	10	0	0	205.2	0.7358	Opt	0.22	0	10	0	0	205.2	0.7242	0.01	1.5E-05
873	0	7	3	0	266.7	0.7084	Opt	0.22	0	7	3	0	266.7	0.7084	0	0
874	0	7	3	0	266.7	0.7088	Opt	0.21	0	7	3	1	268.2	0.7005	0	0.00563
875	0	6	4	0	287.2	0.7106	Opt	0.211	0	6	4	0	287.2	0.7106	0.01	0
876	0	6	4	0	287.2	0.7105	Opt	0.23	0	6	4	0	287.2	0.7016	0	1E-05
877	0	8	2	0	246.4	0.7188	Opt	0.22	0	8	2	0	246.4	0.7188	0	0
878	0	8	2	0	246.4	0.7159	Opt	0.351	0	8	2	0	246.4	0.7105	0	2.4E-05
879	0	7	3	0	266.8	0.7222	Opt	0.25	0	7	3	0	266.8	0.7222	0	0
880	0	7	3	0	266.9	0.7218	Opt	0.261	0	7	3	0	266.9	0.7144	0	1.1E-05
881	0	9	1	0	225.6	0.7515	Opt	0.21	0	9	1	0	225.6	0.7515	0	0
882	0	9	1	1	227.1	0.7514	Opt	0.22	0	8	2	0	246.1	0.7577	0.01	0.08363
883	0	6	4	0	287.1	0.7541	Opt	0.211	0	6	4	0	287.1	0.7541	0.01	0
884	0	6	4	0	287.1	0.7539	Opt	0.41	0	5	5	0	307.6	0.7593	0	0.07139
885	0	10	0	0	205.2	0.7911	Opt	0.221	0	10	0	0	205.2	0.7911	0	0
886	0	10	0	0	205.2	0.7871	Opt	0.22	0	10	0	0	205.2	0.774	0	1.5E-05
887	0	9	1	0	225.7	0.7631	Opt	0.22	0	9	1	0	225.7	0.7631	0	0
888	0	9	1	0	225.7	0.7608	Opt	0.341	0	9	1	2	228.7	0.7507	0	0.0133
889	0	6	4	0	287.2	0.7508	Opt	0.21	0	6	4	0	287.2	0.7508	0	0
890	0	6	4	1	288.7	0.7503	Opt	0.22	0	5	5	0	307.7	0.7757	0.01	0.06573
891	0	4	6	0	328.2	0.7809	Opt	6.98	0	4	6	0	328.2	0.7809	0	0
892	0	5	5	5	315.2	0.7501	Opt	0.341	0	4	6	0	328.2	0.7691	0.01	0.04118
893	0	7	3	0	266.8	0.755	Opt	0.21	0	7	3	0	266.8	0.755	0.01	0
894	0	7	3	0	266.8	0.7539	Opt	0.22	0	6	4	0	287.3	0.7795	0	0.07672
895	0	6	4	0	287.3	0.7558	Opt	0.221	0	6	4	0	287.3	0.7558	0	0
896	0	6	4	0	287.3	0.7544	Opt	0.22	0	5	5	0	307.8	0.7753	0	0.07124
897	0	10	0	0	205.1	0.7148	Opt	0.23	0	10	0	0	205.1	0.7148	0	0
898	1	9	0	12	202.7	0.7004	Opt	0.331	0	10	0	3	209.6	0.7017	0.01	0.03431
899	0	8	2	0	246.1	0.7048	Opt	0.22	0	8	2	0	246.1	0.7048	0	0
900	0	9	1	13	245.1	0.7002	Opt	0.331	0	7	3	0	266.6	0.7144	0	0.08768
901	1	9	0	0	184.8	0.7276	Opt	0.21	1	9	0	0	184.8	0.7276	0.01	1.1E-05
902	1	9	0	0	184.8	0.7231	Opt	0.22	1	9	0	0	184.8	0.7111	0	2.2E-05
903	0	10	0	0	205.2	0.7378	Opt	0.231	0	10	0	0	205.2	0.7378	0.01	0
904	0	10	0	0	205.2	0.7358	Opt	0.22	0	10	0	0	205.2	0.7242	0	9.7E-06
905	0	7	3	0	266.8	0.7084	Opt	0.22	0	7	3	0	266.8	0.7084	0.01	0
906	0	7	3	0	266.8	0.7088	Opt	0.221	0	7	3	1	268.3	0.7005	0	0.00563
907	0	6	4	0	287.3	0.7106	Opt	0.24	0	6	4	0	287.3	0.7106	0	0
908	0	6	4	0	287.3	0.7105	Opt	0.22	0	6	4	0	287.3	0.7016	0.01	3.5E-06
909	0	8	2	0	246.3	0.7188	Opt	0.221	0	8	2	0	246.3	0.7188	0	0
910	0	8	2	0	246.4	0.7159	Opt	0.33	0	8	2	0	246.4	0.7105	0.01	8.1E-06
911	0	7	3	0	266.8	0.7222	Opt	0.271	0	7	3	0	266.8	0.7222	0	0
912	0	7	3	0	266.9	0.7218	Opt	0.24	0	7	3	0	266.9	0.7144	0	3.7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
913	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
914	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
915	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
916	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
917	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
918	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
919	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
920	20	1	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
921	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
922	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
923	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
924	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
925	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
926	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
927	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
928	20	1	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
929	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
930	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
931	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
932	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
933	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
934	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
935	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
936	20	1	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
937	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
938	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
939	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
940	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
941	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
942	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
943	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
944	20	1	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
945	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
946	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
947	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
948	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
949	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
950	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
951	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
952	20	1	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
953	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
954	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
955	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
956	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
957	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
958	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
959	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
960	20	1	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
913	0	9	1	0	225.6	0.7515	Opt	0.22	0	9	1	0	225.6	0.7515	0	0
914	0	9	1	1	227.1	0.7514	Opt	0.231	0	8	2	0	246.1	0.7577	0	0.08364
915	0	6	4	0	287.1	0.7541	Opt	0.21	0	6	4	0	287.1	0.7541	0.01	0
916	0	6	4	0	287.1	0.7539	Opt	0.34	0	5	5	0	307.6	0.7593	0.01	0.07139
917	0	10	0	0	205.2	0.7911	Opt	0.231	0	10	0	0	205.2	0.7911	0	0
918	0	10	0	0	205.2	0.7871	Opt	0.21	0	10	0	0	205.2	0.774	0.01	9.7E-06
919	0	9	1	0	225.7	0.7631	Opt	0.22	0	9	1	0	225.7	0.7631	0.01	0
920	0	9	1	0	225.7	0.7608	Opt	0.401	0	9	1	2	228.7	0.7507	0	0.0133
921	0	6	4	0	287.2	0.7508	Opt	0.22	0	6	4	0	287.2	0.7508	0.01	0
922	0	6	4	1	288.7	0.7503	Opt	0.231	0	5	5	0	307.7	0.7757	0	0.06577
923	0	4	6	0	328.2	0.7809	Opt	5.227	0	4	6	0	328.2	0.7809	0	0
924	0	5	5	5	315.3	0.7501	Opt	0.301	0	4	6	0	328.2	0.7691	0.01	0.04121
925	0	7	3	0	266.8	0.755	Opt	0.22	0	7	3	0	266.8	0.755	0	0
926	0	7	3	0	266.8	0.7539	Opt	0.22	0	6	4	0	287.3	0.7795	0.01	0.07677
927	0	6	4	0	287.3	0.7558	Opt	0.22	0	6	4	0	287.3	0.7558	0	0
928	0	6	4	0	287.3	0.7544	Opt	0.22	0	5	5	0	307.8	0.7753	0.011	0.0713
929	0	10	0	0	205.2	0.7148	Opt	0.24	0	10	0	0	205.2	0.7148	0	0
930	1	9	0	12	202.8	0.7004	Opt	0.331	0	10	0	3	209.7	0.7017	0	0.03403
931	0	8	2	0	246.2	0.7048	Opt	0.22	0	8	2	0	246.2	0.7048	0.01	0
932	0	9	1	13	245.2	0.7006	Opt	0.35	0	7	3	0	266.7	0.7144	0	0.08765
933	1	9	0	0	185	0.7276	Opt	0.211	1	9	0	0	185	0.7276	0.01	2.2E-05
934	1	9	0	0	185	0.7231	Opt	0.22	1	9	0	0	185	0.7111	0.01	3.8E-05
935	0	10	0	0	205.3	0.7378	Opt	0.24	0	10	0	0	205.3	0.7378	0	0
936	0	10	0	0	205.3	0.7358	Opt	0.221	0	10	0	0	205.3	0.7242	0	1.5E-05
937	0	7	3	0	266.8	0.7084	Opt	0.23	0	7	3	0	266.8	0.7084	0.01	0
938	0	7	3	0	266.8	0.7088	Opt	0.22	0	7	3	1	268.3	0.7005	0	0.00563
939	0	6	4	0	287.3	0.7058	Opt	0.351	0	6	4	0	287.3	0.7106	0	7E-06
940	0	6	4	0	287.3	0.7105	Opt	0.23	0	6	4	0	287.3	0.7016	0	7E-06
941	0	8	2	0	246.4	0.7188	Opt	0.221	0	8	2	0	246.4	0.7188	0.01	0
942	0	8	2	0	246.4	0.7159	Opt	0.33	0	8	2	0	246.5	0.7105	0.01	2.4E-05
943	0	7	3	0	266.9	0.7222	Opt	0.27	0	7	3	0	266.9	0.7222	0	0
944	0	7	3	0	266.9	0.7218	Opt	0.24	0	7	3	0	267	0.7144	0	1.5E-05
945	0	9	1	0	225.6	0.7515	Opt	0.22	0	9	1	0	225.6	0.7515	0.01	0
946	0	9	1	1	227.2	0.7514	Opt	0.241	0	8	2	0	246.2	0.7577	0	0.08362
947	0	6	4	0	287.1	0.7541	Opt	0.22	0	6	4	0	287.1	0.7541	0	0
948	0	6	4	0	287.2	0.7539	Opt	0.43	0	5	5	0	307.7	0.7593	0.01	0.07138
949	0	10	0	0	205.2	0.7911	Opt	0.231	0	10	0	0	205.2	0.7911	0.01	0
950	0	10	0	0	205.3	0.7871	Opt	0.22	0	10	0	0	205.3	0.774	0.01	1.9E-05
951	0	9	1	0	225.8	0.7631	Opt	0.23	0	9	1	0	225.8	0.7631	0	0
952	0	9	1	0	225.8	0.7608	Opt	0.421	0	9	1	2	228.8	0.7507	0	0.0133
953	0	6	4	0	287.3	0.7508	Opt	0.22	0	6	4	0	287.3	0.7508	0.01	0
954	0	6	4	1	288.8	0.7503	Opt	0.231	0	5	5	0	307.8	0.7757	0	0.06573
955	0	4	6	0	328.3	0.7809	Opt	5.508	0	4	6	0	328.3	0.7809	0.01	0
956	0	5	5	5	315.3	0.7501	Opt	0.31	0	4	6	0	328.3	0.7691	0	0.04118
957	0	7	3	0	266.9	0.755	Opt	0.23	0	7	3	0	266.9	0.755	0	0
958	0	7	3	0	266.9	0.7539	Opt	0.231	0	6	4	0	287.4	0.7795	0	0.07671
959	0	6	4	0	287.4	0.7558	Opt	0.23	0	6	4	0	287.4	0.7558	0	0
960	0	6	4	0	287.4	0.7544	Opt	0.23	0	5	5	0	307.9	0.7753	0	0.07123

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
961	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
962	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
963	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
964	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
965	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
966	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
967	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
968	20	1	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
969	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
970	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
971	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
972	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
973	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
974	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
975	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
976	20	1	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
977	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
978	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
979	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
980	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
981	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
982	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
983	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
984	20	1	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
985	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
986	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
987	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
988	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
989	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
990	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
991	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
992	20	1	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
993	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
994	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
995	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
996	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
997	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
998	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
999	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1000	20	1	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1001	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1002	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1003	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1004	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1005	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1006	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1007	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1008	20	1	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
961	0	10	0	0	210.1	0.7148	Opt	0.231	0	10	0	0	210.1	0.7148	0	0
962	0	10	0	0	210.1	0.714	Opt	0.28	0	10	0	3	216.1	0.7017	0	0.02857
963	0	8	2	0	252.1	0.7048	Opt	0.231	0	8	2	0	252.1	0.7048	0	0
964	0	8	2	0	252.1	0.7059	Opt	0.32	0	7	3	0	273.1	0.7144	0	0.08329
965	1	9	0	0	189.2	0.7276	Opt	0.23	1	9	0	0	189.2	0.7276	0	1.1E-05
966	1	9	0	0	189.2	0.7231	Opt	0.221	1	9	0	0	189.2	0.7111	0.01	1.6E-05
967	0	10	0	0	210.1	0.7378	Opt	0.22	0	10	0	0	210.1	0.7378	0	0
968	0	10	0	0	210.1	0.7358	Opt	0.23	0	10	0	0	210.1	0.7242	0.01	9.5E-06
969	0	7	3	0	273.1	0.7084	Opt	0.231	0	7	3	0	273.1	0.7084	0	0
970	0	7	3	0	273.2	0.7088	Opt	0.23	0	7	3	1	275.2	0.7005	0	0.00732
971	0	6	4	0	294.2	0.7106	Opt	0.23	0	6	4	0	294.2	0.7106	0	0
972	0	6	4	0	294.2	0.7105	Opt	0.231	0	6	4	0	294.2	0.7016	0	3.4E-06
973	0	8	2	0	252.2	0.7188	Opt	0.23	0	8	2	0	252.2	0.7188	0.01	0
974	0	8	2	0	252.2	0.7159	Opt	0.451	0	8	2	0	252.2	0.7105	0	1.2E-05
975	0	7	3	0	273.2	0.7222	Opt	0.25	0	7	3	0	273.2	0.7222	0	0
976	0	7	3	0	273.2	0.7218	Opt	0.24	0	7	3	0	273.2	0.7144	0.01	7.3E-06
977	0	9	1	0	231.1	0.7515	Opt	0.231	0	9	1	0	231.1	0.7515	0	0
978	0	9	1	1	233.1	0.7514	Opt	0.24	0	8	2	0	252.1	0.7577	0	0.08151
979	0	6	4	0	294.1	0.7541	Opt	0.23	0	6	4	0	294.1	0.7541	0	0
980	0	6	4	0	294.1	0.7539	Opt	0.241	0	5	5	0	315.1	0.7593	0	0.0714
981	0	10	0	0	210.1	0.7911	Opt	0.23	0	10	0	0	210.1	0.7911	0	0
982	0	10	0	0	210.1	0.7871	Opt	0.22	0	10	0	0	210.1	0.774	0.01	9.5E-06
983	0	9	1	0	231.1	0.7631	Opt	0.241	0	9	1	0	231.1	0.7631	0.01	0
984	0	9	1	0	231.1	0.7608	Opt	0.32	0	9	1	2	235.1	0.7507	0	0.01731
985	0	6	4	0	294.1	0.7508	Opt	0.231	0	6	4	0	294.1	0.7508	0	0
986	0	6	4	1	296.1	0.7503	Opt	0.24	0	5	5	0	315.1	0.7757	0	0.06413
987	0	4	6	0	336.1	0.7809	Opt	1.452	0	4	6	0	336.1	0.7809	0	0
988	0	5	5	5	325.1	0.7501	Opt	0.611	0	4	6	0	336.1	0.7691	0	0.03381
989	0	7	3	0	273.2	0.755	Opt	0.22	0	7	3	0	273.2	0.755	0.01	0
990	0	7	3	0	273.2	0.7539	Opt	0.231	0	6	4	0	294.2	0.7795	0.01	0.07682
991	0	6	4	0	294.2	0.7558	Opt	0.24	0	6	4	0	294.2	0.7558	0	0
992	0	6	4	0	294.2	0.7544	Opt	0.23	0	5	5	0	315.2	0.7753	0	0.07133
993	0	10	0	0	210.1	0.7148	Opt	0.231	0	10	0	0	210.1	0.7148	0	0
994	0	10	0	0	210.1	0.714	Opt	0.29	0	10	0	3	216.1	0.7017	0.01	0.02856
995	0	8	2	0	252.1	0.7048	Opt	0.23	0	8	2	0	252.1	0.7048	0.01	0
996	0	8	2	0	252.1	0.7059	Opt	0.251	0	7	3	0	273.1	0.7144	0.01	0.08327
997	1	9	0	0	189.4	0.7276	Opt	0.23	1	9	0	0	189.4	0.7276	0	2.1E-05
998	1	9	0	0	189.4	0.7231	Opt	0.23	1	9	0	0	189.4	0.7111	0	3.7E-05
999	0	10	0	0	210.2	0.7378	Opt	0.231	0	10	0	0	210.2	0.7378	0	0
###	0	10	0	0	210.2	0.7358	Opt	0.23	0	10	0	0	210.2	0.7242	0.01	1.4E-05
###	0	7	3	0	273.2	0.7084	Opt	0.23	0	7	3	0	273.2	0.7084	0.01	0
###	0	7	3	0	273.2	0.7088	Opt	0.231	0	7	3	1	275.2	0.7005	0.01	0.00733
###	0	6	4	0	294.2	0.7106	Opt	0.25	0	6	4	0	294.2	0.7106	0	0
###	0	6	4	0	294.2	0.7105	Opt	0.23	0	6	4	0	294.2	0.7016	0	6.8E-06
###	0	8	2	0	252.3	0.7188	Opt	0.241	0	8	2	0	252.3	0.7188	0	0
###	0	8	2	0	252.3	0.7159	Opt	0.39	0	8	2	0	252.3	0.7105	0	2.8E-05
###	0	7	3	0	273.3	0.7222	Opt	0.251	0	7	3	0	273.3	0.7222	0	0
###	0	7	3	0	273.3	0.7218	Opt	0.24	0	7	3	0	273.3	0.7144	0	1.5E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1009	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1010	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1011	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1012	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1013	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1014	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1015	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1016	20	1	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1017	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1018	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1019	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1020	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1021	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1022	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1023	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1024	20	1	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1025	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1026	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1027	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1028	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1029	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1030	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1031	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1032	20	1	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1033	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1034	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1035	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1036	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1037	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1038	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1039	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1040	20	1	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1041	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1042	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1043	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1044	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1045	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1046	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1047	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1048	20	1	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1049	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1050	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1051	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1052	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1053	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1054	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1055	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1056	20	1	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

Exp #	Output															H-Opt Gap
	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	
1009	0	9	1	0	231.1	0.7515	Opt	0.23	0	9	1	0	231.1	0.7515	0	0
1010	0	9	1	1	233.1	0.7514	Opt	0.241	0	8	2	0	252.1	0.7577	0.01	0.08149
1011	0	6	4	0	294.1	0.7541	Opt	0.24	0	6	4	0	294.1	0.7541	0	0
1012	0	6	4	0	294.1	0.7539	Opt	0.24	0	5	5	0	315.1	0.7593	0	0.0714
1013	0	10	0	0	210.2	0.7911	Opt	0.231	0	10	0	0	210.2	0.7911	0.01	0
1014	0	10	0	0	210.2	0.7871	Opt	0.24	0	10	0	0	210.2	0.774	0	1.9E-05
1015	0	9	1	0	231.2	0.7631	Opt	0.24	0	9	1	0	231.2	0.7631	0	0
1016	0	9	1	0	231.2	0.7608	Opt	0.311	0	9	1	2	235.2	0.7507	0	0.01731
1017	0	6	4	0	294.2	0.7508	Opt	0.24	0	6	4	0	294.2	0.7508	0	0
1018	0	6	4	1	296.2	0.7503	Opt	0.241	0	5	5	0	315.2	0.7757	0	0.06409
1019	0	4	6	0	336.2	0.7809	Opt	1.372	0	4	6	0	336.2	0.7809	0	0
1020	0	5	5	5	325.2	0.7501	Opt	0.6	0	4	6	0	336.2	0.7691	0.01	0.03378
1021	0	7	3	0	273.3	0.755	Opt	0.241	0	7	3	0	273.3	0.755	0	0
1022	0	7	3	0	273.3	0.7539	Opt	0.23	0	6	4	0	294.3	0.7795	0	0.07675
1023	0	6	4	0	294.3	0.7558	Opt	0.24	0	6	4	0	294.3	0.7558	0.01	0
1024	0	6	4	0	294.3	0.7544	Opt	0.241	0	5	5	0	315.3	0.7753	0	0.07127
1025	0	10	0	0	210.1	0.7148	Opt	0.23	0	10	0	0	210.1	0.7148	0	0
1026	0	10	0	0	210.1	0.714	Opt	0.301	0	10	0	3	216.1	0.7017	0.01	0.02856
1027	0	8	2	0	252.1	0.7048	Opt	0.23	0	8	2	0	252.1	0.7048	0.01	0
1028	0	8	2	0	252.1	0.7059	Opt	0.29	0	7	3	0	273.1	0.7144	0	0.08328
1029	1	9	0	0	189.2	0.7276	Opt	0.231	1	9	0	0	189.2	0.7276	0	1.1E-05
1030	1	9	0	0	189.3	0.7231	Opt	0.23	1	9	0	0	189.3	0.7111	0.01	1.6E-05
1031	0	10	0	0	210.2	0.7378	Opt	0.23	0	10	0	0	210.2	0.7378	0.01	0
1032	0	10	0	0	210.2	0.7358	Opt	0.231	0	10	0	0	210.2	0.7242	0.01	9.5E-06
1033	0	7	3	0	273.2	0.7084	Opt	0.24	0	7	3	0	273.2	0.7084	0.01	0
1034	0	7	3	0	273.2	0.7088	Opt	0.24	0	7	3	1	275.2	0.7005	0	0.00732
1035	0	6	4	0	294.2	0.7106	Opt	0.231	0	6	4	0	294.2	0.7106	0.01	0
1036	0	6	4	0	294.2	0.7105	Opt	0.23	0	6	4	0	294.2	0.7016	0.01	3.4E-06
1037	0	8	2	0	252.3	0.7188	Opt	0.24	0	8	2	0	252.3	0.7188	0	0
1038	0	8	2	0	252.3	0.7182	Opt	0.271	0	8	2	0	252.3	0.7105	0	7.9E-06
1039	0	7	3	0	273.3	0.7222	Opt	0.27	0	7	3	0	273.3	0.7222	0	0
1040	0	7	3	0	273.3	0.7218	Opt	0.281	0	7	3	0	273.3	0.7144	0	7.3E-06
1041	0	9	1	0	231.1	0.7515	Opt	0.24	0	9	1	0	231.1	0.7515	0	0
1042	0	9	1	1	233.1	0.7514	Opt	0.25	0	8	2	0	252.1	0.7577	0	0.08149
1043	0	6	4	0	294.1	0.7541	Opt	0.231	0	6	4	0	294.1	0.7541	0.01	0
1044	0	6	4	0	294.1	0.7539	Opt	0.24	0	5	5	0	315.1	0.7593	0.01	0.07139
1045	0	10	0	0	210.1	0.7911	Opt	0.24	0	10	0	0	210.1	0.7911	0.01	0
1046	0	10	0	0	210.2	0.7871	Opt	0.231	0	10	0	0	210.2	0.774	0	4.8E-06
1047	0	9	1	0	231.2	0.7631	Opt	0.24	0	9	1	0	231.2	0.7631	0.01	0
1048	0	9	1	0	231.2	0.7608	Opt	0.311	0	9	1	2	235.2	0.7507	0	0.01731
1049	0	6	4	0	294.2	0.7508	Opt	0.24	0	6	4	0	294.2	0.7508	0	0
1050	0	6	4	1	296.2	0.7503	Opt	0.25	0	5	5	0	315.2	0.7757	0	0.0641
1051	0	4	6	0	336.2	0.7809	Opt	6.6	0	4	6	0	336.2	0.7809	0.01	0
1052	0	5	5	5	325.2	0.7501	Opt	0.34	0	4	6	0	336.2	0.7691	0.01	0.03379
1053	0	7	3	0	273.2	0.755	Opt	0.231	0	7	3	0	273.2	0.755	0.01	0
1054	0	7	3	0	273.2	0.7539	Opt	0.23	0	6	4	0	294.2	0.7795	0.01	0.07679
1055	0	6	4	0	294.2	0.7558	Opt	0.24	0	6	4	0	294.2	0.7558	0.01	0
1056	0	6	4	0	294.2	0.7544	Opt	0.231	0	5	5	0	315.2	0.7753	0.01	0.07131

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1057	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1058	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1059	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1060	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1061	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1062	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1063	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1064	20	1	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1065	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1066	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1067	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1068	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1069	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1070	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1071	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1072	20	1	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1073	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1074	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1075	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1076	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1077	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1078	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1079	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1080	20	1	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1081	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1082	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1083	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1084	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1085	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1086	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1087	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1088	20	1	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1089	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1090	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1091	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1092	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1093	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1094	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1095	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1096	20	1	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1097	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1098	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1099	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1100	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1101	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1102	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1103	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1104	20	1	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



Exp #	Output															
	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1057	0	10	0	0	210.1	0.7148	Opt	0.24	0	10	0	0	210.1	0.7148	0.01	0
1058	0	10	0	0	210.1	0.714	Opt	0.361	0	10	0	3	216.1	0.7017	0	0.02856
1059	0	8	2	0	252.1	0.7048	Opt	0.25	0	8	2	0	252.1	0.7048	0	0
1060	0	8	2	0	252.1	0.7053	Opt	0.31	0	7	3	0	273.1	0.7144	0	0.08326
1061	1	9	0	0	189.4	0.7276	Opt	0.241	1	9	0	0	189.4	0.7276	0	2.1E-05
1062	1	9	0	0	189.4	0.7231	Opt	0.24	1	9	0	0	189.4	0.7111	0	3.7E-05
1063	0	10	0	0	210.2	0.7378	Opt	0.24	0	10	0	0	210.2	0.7378	0.01	0
1064	0	10	0	0	210.2	0.7358	Opt	0.241	0	10	0	0	210.2	0.7242	0	1.4E-05
1065	0	7	3	0	273.2	0.7084	Opt	0.25	0	7	3	0	273.2	0.7084	0.01	0
1066	0	7	3	0	273.2	0.7088	Opt	0.25	0	7	3	1	275.2	0.7005	0.01	0.00733
1067	0	6	4	0	294.2	0.7106	Opt	0.24	0	6	4	0	294.2	0.7106	0.011	0
1068	0	6	4	0	294.2	0.7105	Opt	0.25	0	6	4	0	294.2	0.7016	0.01	1E-05
1069	0	8	2	0	252.4	0.7188	Opt	0.241	0	8	2	0	252.4	0.7188	0	0
1070	0	8	2	0	252.4	0.7159	Opt	0.36	0	8	2	0	252.4	0.7105	0.01	2.4E-05
1071	0	7	3	0	273.3	0.7222	Opt	0.281	0	7	3	0	273.3	0.7222	0	0
1072	0	7	3	0	273.4	0.7218	Opt	0.3	0	7	3	0	273.4	0.7144	0	1.1E-05
1073	0	9	1	0	231.1	0.7515	Opt	0.24	0	9	1	0	231.1	0.7515	0.01	0
1074	0	9	1	1	233.1	0.7514	Opt	0.261	0	8	2	0	252.1	0.7577	0	0.08147
1075	0	6	4	0	294.1	0.7541	Opt	0.24	0	6	4	0	294.1	0.7541	0	0
1076	0	6	4	0	294.1	0.7539	Opt	0.25	0	5	5	0	315.1	0.7593	0	0.07139
1077	0	10	0	0	210.2	0.7911	Opt	0.241	0	10	0	0	210.2	0.7911	0.01	0
1078	0	10	0	0	210.2	0.7871	Opt	0.24	0	10	0	0	210.2	0.774	0.01	1.4E-05
1079	0	9	1	0	231.2	0.7631	Opt	0.25	0	9	1	0	231.2	0.7631	0	0
1080	0	9	1	0	231.2	0.7608	Opt	0.331	0	9	1	2	235.2	0.7507	0	0.01731
1081	0	6	4	0	294.2	0.7508	Opt	0.24	0	6	4	0	294.2	0.7508	0	0
1082	0	6	4	1	296.2	0.7503	Opt	0.251	0	5	5	0	315.2	0.7757	0.01	0.06407
1083	0	4	6	0	336.2	0.7809	Opt	2.353	0	4	6	0	336.2	0.7809	0	0
1084	0	5	5	5	325.2	0.7501	Opt	0.491	0	4	6	0	336.2	0.7691	0.01	0.03376
1085	0	7	3	0	273.3	0.755	Opt	0.25	0	7	3	0	273.3	0.755	0	0
1086	0	7	3	0	273.3	0.7539	Opt	0.24	0	6	4	0	294.3	0.7795	0	0.07672
1087	0	6	4	0	294.3	0.7558	Opt	0.251	0	6	4	0	294.3	0.7558	0.01	0
1088	0	6	4	0	294.3	0.7544	Opt	0.25	0	5	5	0	315.3	0.7753	0	0.07125
1089	0	10	0	0	210.1	0.7148	Opt	0.251	0	10	0	0	210.1	0.7148	0	0
1090	0	10	0	0	210.1	0.714	Opt	0.28	0	10	0	3	216.1	0.7017	0	0.02855
1091	0	8	2	0	252.1	0.7048	Opt	0.25	0	8	2	0	252.1	0.7048	0	0
1092	0	8	2	0	252.1	0.7059	Opt	0.351	0	7	3	0	273.1	0.7144	0	0.08327
1093	1	9	0	0	189.3	0.7276	Opt	0.24	1	9	0	0	189.3	0.7276	0	1.1E-05
1094	1	9	0	0	189.3	0.7231	Opt	0.241	1	9	0	0	189.3	0.7111	0.01	2.1E-05
1095	0	10	0	0	210.2	0.7378	Opt	0.25	0	10	0	0	210.2	0.7378	0	0
1096	0	10	0	0	210.2	0.7358	Opt	0.25	0	10	0	0	210.2	0.7242	0	9.5E-06
1097	0	7	3	0	273.3	0.7084	Opt	0.251	0	7	3	0	273.3	0.7084	0	0
1098	0	7	3	0	273.3	0.7088	Opt	0.25	0	7	3	1	275.3	0.7005	0	0.00732
1099	0	6	4	0	294.3	0.7106	Opt	0.25	0	6	4	0	294.3	0.7106	0	0
1100	0	6	4	0	294.3	0.7105	Opt	0.251	0	6	4	0	294.3	0.7016	0	3.4E-06
1101	0	8	2	0	252.3	0.7188	Opt	0.25	0	8	2	0	252.3	0.7188	0.01	0
1102	0	8	2	0	252.4	0.7159	Opt	0.461	0	8	2	0	252.4	0.7105	0	7.9E-06
1103	0	7	3	0	273.3	0.7222	Opt	0.27	0	7	3	0	273.3	0.7222	0.01	0
1104	0	7	3	0	273.4	0.7218	Opt	0.261	0	7	3	0	273.4	0.7144	0.01	3.7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1105	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1106	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1107	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1108	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1109	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1110	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1111	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1112	20	1	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1113	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1114	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1115	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1116	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1117	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1118	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1119	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1120	20	1	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1121	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1122	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1123	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1124	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1125	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1126	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1127	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1128	20	1	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1129	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1130	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1131	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1132	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1133	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1134	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1135	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1136	20	1	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1137	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1138	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1139	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1140	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1141	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1142	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1143	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1144	20	1	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1145	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1146	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1147	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1148	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1149	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1150	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1151	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1152	20	1	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1105	0	9	1	0	231.1	0.7515	Opt	0.24	0	9	1	0	231.1	0.7515	0	0
1106	0	9	1	1	233.1	0.7514	Opt	0.26	0	8	2	0	252.1	0.7577	0	0.08149
1107	0	6	4	0	294.1	0.7541	Opt	0.241	0	6	4	0	294.1	0.7541	0.01	0
1108	0	6	4	0	294.1	0.7539	Opt	0.26	0	5	5	0	315.1	0.7593	0	0.07139
1109	0	10	0	0	210.2	0.7911	Opt	0.25	0	10	0	0	210.2	0.7911	0	0
1110	0	10	0	0	210.2	0.7871	Opt	0.251	0	10	0	0	210.2	0.774	0	9.5E-06
1111	0	9	1	0	231.2	0.7631	Opt	0.26	0	9	1	0	231.2	0.7631	0	0
1112	0	9	1	0	231.2	0.7608	Opt	0.341	0	9	1	2	235.2	0.7507	0	0.0173
1113	0	6	4	0	294.2	0.7508	Opt	0.24	0	6	4	0	294.2	0.7508	0.01	0
1114	0	6	4	1	296.2	0.7503	Opt	0.25	0	5	5	0	315.2	0.7757	0.01	0.06411
1115	0	4	6	0	336.2	0.7809	Opt	1.743	0	4	6	0	336.2	0.7809	0.01	0
1116	0	5	5	5	325.3	0.7501	Opt	0.631	0	4	6	0	336.2	0.7691	0.01	0.03379
1117	0	7	3	0	273.3	0.755	Opt	0.25	0	7	3	0	273.3	0.755	0	0
1118	0	7	3	0	273.3	0.7539	Opt	0.25	0	6	4	0	294.3	0.7795	0.01	0.07678
1119	0	6	4	0	294.3	0.7558	Opt	0.251	0	6	4	0	294.3	0.7558	0	0
1120	0	6	4	0	294.3	0.7544	Opt	0.24	0	5	5	0	315.3	0.7753	0.01	0.0713
1121	0	10	0	0	210.2	0.7148	Opt	0.251	0	10	0	0	210.2	0.7148	0.01	0
1122	0	10	0	0	210.2	0.714	Opt	0.32	0	10	0	3	216.2	0.7017	0	0.02855
1123	0	8	2	0	252.2	0.7048	Opt	0.25	0	8	2	0	252.2	0.7048	0.01	0
1124	0	8	2	0	252.2	0.7053	Opt	0.331	0	7	3	0	273.2	0.7144	0	0.08325
1125	1	9	0	0	189.5	0.7276	Opt	0.25	1	9	0	0	189.5	0.7276	0	2.1E-05
1126	1	9	0	0	189.5	0.7231	Opt	0.261	1	9	0	0	189.5	0.7111	0	3.7E-05
1127	0	10	0	0	210.3	0.7378	Opt	0.25	0	10	0	0	210.3	0.7378	0	0
1128	0	10	0	0	210.3	0.7358	Opt	0.25	0	10	0	0	210.3	0.7242	0.01	1.4E-05
1129	0	7	3	0	273.3	0.7084	Opt	0.271	0	7	3	0	273.3	0.7084	0	0
1130	0	7	3	0	273.3	0.7088	Opt	0.25	0	7	3	1	275.3	0.7005	0	0.00732
1131	0	6	4	0	294.3	0.7106	Opt	0.26	0	6	4	0	294.3	0.7106	0.01	0
1132	0	6	4	0	294.3	0.7105	Opt	0.261	0	6	4	0	294.3	0.7016	0	6.8E-06
1133	0	8	2	0	252.4	0.7188	Opt	0.25	0	8	2	0	252.4	0.7188	0	0
1134	0	8	2	0	252.4	0.7159	Opt	0.491	0	8	2	0	252.5	0.7105	0.01	2.4E-05
1135	0	7	3	0	273.4	0.7222	Opt	0.29	0	7	3	0	273.4	0.7222	0	0
1136	0	7	3	0	273.4	0.7218	Opt	0.261	0	7	3	0	273.5	0.7144	0.01	1.5E-05
1137	0	9	1	0	231.1	0.7515	Opt	0.25	0	9	1	0	231.1	0.7515	0	0
1138	0	9	1	1	233.2	0.7514	Opt	0.27	0	8	2	0	252.2	0.7577	0	0.08146
1139	0	6	4	0	294.1	0.7541	Opt	0.251	0	6	4	0	294.1	0.7541	0	0
1140	0	6	4	0	294.2	0.7539	Opt	0.26	0	5	5	0	315.2	0.7593	0.01	0.07138
1141	0	10	0	0	210.2	0.7911	Opt	0.261	0	10	0	0	210.2	0.7911	0	0
1142	0	10	0	0	210.3	0.7871	Opt	0.25	0	10	0	0	210.3	0.774	0	1.9E-05
1143	0	9	1	0	231.3	0.7631	Opt	0.25	0	9	1	0	231.3	0.7631	0.01	0
1144	0	9	1	0	231.3	0.7608	Opt	0.351	0	9	1	2	235.3	0.7507	0	0.0173
1145	0	6	4	0	294.3	0.7508	Opt	0.25	0	6	4	0	294.3	0.7508	0	0
1146	0	6	4	1	296.3	0.7503	Opt	0.261	0	5	5	0	315.3	0.7757	0.01	0.06407
1147	0	4	6	0	336.3	0.7809	Opt	1.291	0	4	6	0	336.3	0.7809	0	0
1148	0	5	5	5	325.3	0.7501	Opt	0.631	0	4	6	0	336.3	0.7691	0.01	0.03377
1149	0	7	3	0	273.4	0.755	Opt	0.251	0	7	3	0	273.4	0.755	0	0
1150	0	7	3	0	273.4	0.7539	Opt	0.25	0	6	4	0	294.4	0.7795	0.01	0.07671
1151	0	6	4	0	294.4	0.7558	Opt	0.25	0	6	4	0	294.4	0.7558	0.01	0
1152	0	6	4	0	294.4	0.7544	Opt	0.25	0	5	5	0	315.4	0.7753	0.011	0.07124

Exp #	Input Parameters										
	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^g$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1153	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1154	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1155	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1156	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1157	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1158	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1159	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1160	20	2	0.5	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1161	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1162	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1163	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1164	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1165	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1166	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1167	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1168	20	2	0.5	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1169	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1170	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1171	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1172	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1173	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1174	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1175	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1176	20	2	0.5	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1177	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1178	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1179	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1180	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1181	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1182	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1183	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1184	20	2	0.5	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1185	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1186	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1187	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1188	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1189	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1190	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1191	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1192	20	2	0.5	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1193	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1194	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1195	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1196	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1197	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1198	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1199	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1200	20	2	0.5	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1153	0	10	0	0	205.1	0.7148	Opt	0.26	0	10	0	0	205.1	0.7148	0	0
1154	0	10	0	0	205.1	0.714	Opt	0.301	0	10	0	3	212.6	0.7017	0	0.03658
1155	0	8	2	0	246.1	0.7048	Opt	0.26	0	8	2	0	246.1	0.7048	0	0
1156	0	8	2	0	246.1	0.7059	Opt	0.28	0	7	3	0	266.6	0.7144	0	0.08329
1157	1	9	0	0	184.7	0.7276	Opt	0.251	1	9	0	0	184.7	0.7276	0.01	1.1E-05
1158	1	9	0	0	184.7	0.7231	Opt	0.25	1	9	0	0	184.7	0.7111	0	1.6E-05
1159	0	10	0	0	205.1	0.7378	Opt	0.271	0	10	0	0	205.1	0.7378	0.01	0
1160	0	10	0	0	205.1	0.7358	Opt	0.25	0	10	0	0	205.1	0.7242	0	9.7E-06
1161	0	7	3	0	266.6	0.7084	Opt	0.26	0	7	3	0	266.6	0.7084	0.01	0
1162	0	7	3	0	266.7	0.7088	Opt	0.251	0	7	3	1	269.2	0.7005	0.01	0.00938
1163	0	6	4	0	287.2	0.7106	Opt	0.26	0	6	4	0	287.2	0.7106	0	0
1164	0	6	4	0	287.2	0.7105	Opt	0.26	0	6	4	0	287.2	0.7016	0	3.5E-06
1165	0	8	2	0	246.2	0.7188	Opt	0.261	0	8	2	0	246.2	0.7188	0	0
1166	0	8	2	0	246.2	0.7182	Opt	0.26	0	8	2	0	246.2	0.7105	0	8.1E-06
1167	0	7	3	0	266.7	0.7222	Opt	0.291	0	7	3	0	266.7	0.7222	0.01	0
1168	0	7	3	0	266.7	0.7218	Opt	0.36	0	7	3	0	266.7	0.7144	0	7.5E-06
1169	0	9	1	0	225.6	0.7515	Opt	0.251	0	9	1	0	225.6	0.7515	0.01	0
1170	0	9	1	1	228.1	0.7514	Opt	0.26	0	8	2	0	246.1	0.7577	0.01	0.07891
1171	0	6	4	0	287.1	0.7541	Opt	0.25	0	6	4	0	287.1	0.7541	0.01	0
1172	0	6	4	0	287.1	0.7539	Opt	0.261	0	5	5	0	307.6	0.7593	0	0.0714
1173	0	10	0	0	205.1	0.7911	Opt	0.25	0	10	0	0	205.1	0.7911	0.01	0
1174	0	10	0	0	205.1	0.7871	Opt	0.25	0	10	0	0	205.1	0.774	0.01	9.7E-06
1175	0	9	1	0	225.6	0.7631	Opt	0.261	0	9	1	0	225.6	0.7631	0	0
1176	0	9	1	0	225.6	0.7608	Opt	0.31	0	9	1	2	230.6	0.7507	0	0.02216
1177	0	6	4	0	287.1	0.7508	Opt	0.251	0	6	4	0	287.1	0.7508	0.01	0
1178	0	6	4	1	289.6	0.7503	Opt	0.26	0	5	5	0	307.6	0.7757	0.01	0.06211
1179	0	4	6	0	328.1	0.7809	Opt	2.193	0	4	6	0	328.1	0.7809	0.01	0
1180	0	5	5	5	320.1	0.7501	Opt	0.431	0	4	6	0	328.1	0.7691	0	0.02496
1181	0	7	3	0	266.7	0.755	Opt	0.26	0	7	3	0	266.7	0.755	0	0
1182	0	7	3	0	266.7	0.7539	Opt	0.261	0	6	4	0	287.2	0.7795	0	0.07681
1183	0	6	4	0	287.2	0.7558	Opt	0.26	0	6	4	0	287.2	0.7558	0.01	0
1184	0	6	4	0	287.2	0.7544	Opt	0.26	0	5	5	0	307.7	0.7753	0	0.07133
1185	0	10	0	0	205.1	0.7148	Opt	0.261	0	10	0	0	205.1	0.7148	0	0
1186	0	10	0	0	205.1	0.714	Opt	0.29	0	10	0	3	212.6	0.7017	0	0.03657
1187	0	8	2	0	246.1	0.7048	Opt	0.26	0	8	2	0	246.1	0.7048	0	0
1188	0	8	2	0	246.1	0.7059	Opt	0.271	0	7	3	0	266.6	0.7144	0.01	0.08327
1189	1	9	0	0	184.9	0.7276	Opt	0.25	1	9	0	0	184.9	0.7276	0.01	2.2E-05
1190	1	9	0	0	184.9	0.7231	Opt	0.251	1	9	0	0	184.9	0.7111	0.01	3.8E-05
1191	0	10	0	0	205.2	0.7378	Opt	0.27	0	10	0	0	205.2	0.7378	0.01	0
1192	0	10	0	0	205.2	0.7358	Opt	0.27	0	10	0	0	205.2	0.7242	0	1.5E-05
1193	0	7	3	0	266.7	0.7084	Opt	0.271	0	7	3	0	266.7	0.7084	0	0
1194	0	7	3	0	266.7	0.7088	Opt	0.25	0	7	3	1	269.2	0.7005	0.01	0.00938
1195	0	6	4	0	287.2	0.7106	Opt	0.261	0	6	4	0	287.2	0.7106	0.01	0
1196	0	6	4	0	287.2	0.7105	Opt	0.26	0	6	4	0	287.2	0.7016	0	7E-06
1197	0	8	2	0	246.3	0.7188	Opt	0.26	0	8	2	0	246.3	0.7188	0.01	0
1198	0	8	2	0	246.3	0.7159	Opt	0.351	0	8	2	0	246.3	0.7105	0	2.8E-05
1199	0	7	3	0	266.8	0.7222	Opt	0.29	0	7	3	0	266.8	0.7222	0.01	0
1200	0	7	3	0	266.8	0.7218	Opt	0.271	0	7	3	0	266.8	0.7144	0	1.5E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1201	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1202	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1203	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1204	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1205	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1206	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1207	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1208	20	2	0.5	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1209	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1210	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1211	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1212	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1213	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1214	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1215	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1216	20	2	0.5	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1217	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1218	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1219	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1220	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1221	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1222	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1223	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1224	20	2	0.5	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1225	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1226	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1227	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1228	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1229	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1230	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1231	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1232	20	2	0.5	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1233	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1234	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1235	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1236	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1237	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1238	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1239	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1240	20	2	0.5	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1241	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1242	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1243	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1244	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1245	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1246	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1247	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1248	20	2	0.5	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1201	0	9	1	0	225.6	0.7515	Opt	0.26	0	9	1	0	225.6	0.7515	0	0
1202	0	9	1	1	228.1	0.7514	Opt	0.27	0	8	2	0	246.1	0.7577	0.01	0.07889
1203	0	6	4	0	287.1	0.7541	Opt	0.251	0	6	4	0	287.1	0.7541	0.01	0
1204	0	6	4	0	287.1	0.7539	Opt	0.26	0	5	5	0	307.6	0.7593	0.01	0.0714
1205	0	10	0	0	205.2	0.7911	Opt	0.271	0	10	0	0	205.2	0.7911	0	0
1206	0	10	0	0	205.2	0.7871	Opt	0.26	0	10	0	0	205.2	0.774	0	1.9E-05
1207	0	9	1	0	225.7	0.7631	Opt	0.26	0	9	1	0	225.7	0.7631	0.01	0
1208	0	9	1	0	225.7	0.7608	Opt	0.311	0	9	1	2	230.7	0.7507	0	0.02217
1209	0	6	4	0	287.2	0.7508	Opt	0.26	0	6	4	0	287.2	0.7508	0	0
1210	0	6	4	1	289.7	0.7503	Opt	0.271	0	5	5	0	307.7	0.7757	0	0.06208
1211	0	4	6	0	328.2	0.7809	Opt	2.383	0	4	6	0	328.2	0.7809	0.01	0
1212	0	5	5	5	320.2	0.7501	Opt	0.681	0	4	6	0	328.2	0.7691	0	0.02494
1213	0	7	3	0	266.8	0.755	Opt	0.26	0	7	3	0	266.8	0.755	0	0
1214	0	7	3	0	266.8	0.7539	Opt	0.271	0	6	4	0	287.3	0.7795	0	0.07675
1215	0	6	4	0	287.3	0.7558	Opt	0.26	0	6	4	0	287.3	0.7558	0	0
1216	0	6	4	0	287.3	0.7544	Opt	0.26	0	5	5	0	307.8	0.7753	0.01	0.07127
1217	0	10	0	0	205.1	0.7148	Opt	0.261	0	10	0	0	205.1	0.7148	0	0
1218	0	10	0	0	205.1	0.714	Opt	0.3	0	10	0	3	212.6	0.7017	0.01	0.03657
1219	0	8	2	0	246.1	0.7048	Opt	0.271	0	8	2	0	246.1	0.7048	0	0
1220	0	8	2	0	246.1	0.7059	Opt	0.28	0	7	3	0	266.6	0.7144	0	0.08328
1221	1	9	0	0	184.7	0.7276	Opt	0.26	1	9	0	0	184.7	0.7276	0	1.1E-05
1222	1	9	0	0	184.8	0.7231	Opt	0.261	1	9	0	0	184.8	0.7111	0	1.6E-05
1223	0	10	0	0	205.2	0.7378	Opt	0.27	0	10	0	0	205.2	0.7378	0	0
1224	0	10	0	0	205.2	0.7358	Opt	0.271	0	10	0	0	205.2	0.7242	0	9.7E-06
1225	0	7	3	0	266.7	0.7084	Opt	0.27	0	7	3	0	266.7	0.7084	0.01	0
1226	0	7	3	0	266.7	0.7088	Opt	0.27	0	7	3	1	269.2	0.7005	0	0.00938
1227	0	6	4	0	287.2	0.7106	Opt	0.281	0	6	4	0	287.2	0.7106	0	0
1228	0	6	4	0	287.2	0.7105	Opt	0.28	0	6	4	0	287.2	0.7016	0	3.5E-06
1229	0	8	2	0	246.3	0.7188	Opt	0.271	0	8	2	0	246.3	0.7188	0	0
1230	0	8	2	0	246.3	0.7182	Opt	0.28	0	8	2	0	246.3	0.7105	0	8.1E-06
1231	0	7	3	0	266.8	0.7222	Opt	0.31	0	7	3	0	266.8	0.7222	0	0
1232	0	7	3	0	266.8	0.7218	Opt	0.351	0	7	3	0	266.8	0.7144	0	7.5E-06
1233	0	9	1	0	225.6	0.7515	Opt	0.26	0	9	1	0	225.6	0.7515	0	0
1234	0	9	1	1	228.1	0.7514	Opt	0.271	0	8	2	0	246.1	0.7577	0.01	0.07889
1235	0	6	4	0	287.1	0.7541	Opt	0.26	0	6	4	0	287.1	0.7541	0.01	0
1236	0	6	4	0	287.1	0.7539	Opt	0.261	0	5	5	0	307.6	0.7593	0.01	0.07139
1237	0	10	0	0	205.1	0.7911	Opt	0.26	0	10	0	0	205.1	0.7911	0.01	0
1238	0	10	0	0	205.2	0.7871	Opt	0.27	0	10	0	0	205.2	0.774	0	4.9E-06
1239	0	9	1	0	225.7	0.7631	Opt	0.271	0	9	1	0	225.7	0.7631	0	0
1240	0	9	1	0	225.7	0.7608	Opt	0.31	0	9	1	2	230.7	0.7507	0	0.02216
1241	0	6	4	0	287.2	0.7508	Opt	0.261	0	6	4	0	287.2	0.7508	0	0
1242	0	6	4	1	289.7	0.7503	Opt	0.27	0	5	5	0	307.7	0.7757	0.01	0.06209
1243	0	4	6	0	328.2	0.7809	Opt	2.233	0	4	6	0	328.2	0.7809	0	0
1244	0	5	5	5	320.2	0.7501	Opt	1.232	0	4	6	0	328.2	0.7691	0	0.02495
1245	0	7	3	0	266.7	0.755	Opt	0.26	0	7	3	0	266.7	0.755	0.01	0
1246	0	7	3	0	266.7	0.7539	Opt	0.261	0	6	4	0	287.2	0.7795	0.01	0.07678
1247	0	6	4	0	287.2	0.7558	Opt	0.27	0	6	4	0	287.2	0.7558	0.01	0
1248	0	6	4	0	287.2	0.7544	Opt	0.27	0	5	5	0	307.7	0.7753	0	0.07131

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1249	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1250	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1251	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1252	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1253	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1254	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1255	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1256	20	2	0.5	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1257	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1258	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1259	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1260	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1261	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1262	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1263	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1264	20	2	0.5	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1265	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1266	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1267	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1268	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1269	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1270	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1271	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1272	20	2	0.5	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1273	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1274	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1275	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1276	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1277	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1278	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1279	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1280	20	2	0.5	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1281	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1282	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1283	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1284	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1285	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1286	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1287	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1288	20	2	0.5	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1289	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1290	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1291	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1292	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1293	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1294	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1295	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1296	20	2	0.5	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1249	0	10	0	0	205.1	0.7148	Opt	0.271	0	10	0	0	205.1	0.7148	0	0
1250	0	10	0	0	205.1	0.714	Opt	0.31	0	10	0	3	212.6	0.7017	0.01	0.03657
1251	0	8	2	0	246.1	0.7048	Opt	0.271	0	8	2	0	246.1	0.7048	0.01	0
1252	0	8	2	0	246.1	0.7059	Opt	0.29	0	7	3	0	266.6	0.7144	0	0.08326
1253	1	9	0	0	184.9	0.7276	Opt	0.271	1	9	0	0	184.9	0.7276	0	2.2E-05
1254	1	9	0	0	184.9	0.7231	Opt	0.27	1	9	0	0	184.9	0.7111	0	3.8E-05
1255	0	10	0	0	205.2	0.7378	Opt	0.28	0	10	0	0	205.2	0.7378	0	0
1256	0	10	0	0	205.2	0.7358	Opt	0.281	0	10	0	0	205.2	0.7242	0.01	1.5E-05
1257	0	7	3	0	266.7	0.7084	Opt	0.28	0	7	3	0	266.7	0.7084	0	0
1258	0	7	3	0	266.7	0.7088	Opt	0.281	0	7	3	1	269.2	0.7005	0	0.00938
1259	0	6	4	0	287.2	0.7106	Opt	0.27	0	6	4	0	287.2	0.7106	0	0
1260	0	6	4	0	287.2	0.7105	Opt	0.26	0	6	4	0	287.2	0.7016	0.01	1E-05
1261	0	8	2	0	246.4	0.7188	Opt	0.271	0	8	2	0	246.4	0.7188	0.01	0
1262	0	8	2	0	246.4	0.7182	Opt	0.29	0	8	2	0	246.4	0.7105	0	1.6E-05
1263	0	7	3	0	266.8	0.7222	Opt	0.311	0	7	3	0	266.8	0.7222	0	0
1264	0	7	3	0	266.9	0.7218	Opt	0.32	0	7	3	0	266.9	0.7144	0.01	1.1E-05
1265	0	9	1	0	225.6	0.7515	Opt	0.26	0	9	1	0	225.6	0.7515	0.01	0
1266	0	9	1	1	228.1	0.7514	Opt	0.281	0	8	2	0	246.1	0.7577	0.01	0.07888
1267	0	6	4	0	287.1	0.7541	Opt	0.26	0	6	4	0	287.1	0.7541	0.01	0
1268	0	6	4	0	287.1	0.7539	Opt	0.271	0	5	5	0	307.6	0.7593	0.01	0.07139
1269	0	10	0	0	205.2	0.7911	Opt	0.27	0	10	0	0	205.2	0.7911	0	0
1270	0	10	0	0	205.2	0.7871	Opt	0.27	0	10	0	0	205.2	0.774	0	1.5E-05
1271	0	9	1	0	225.7	0.7631	Opt	0.271	0	9	1	0	225.7	0.7631	0	0
1272	0	9	1	0	225.7	0.7608	Opt	0.31	0	9	1	2	230.7	0.7507	0.01	0.02216
1273	0	6	4	0	287.2	0.7508	Opt	0.271	0	6	4	0	287.2	0.7508	0.01	0
1274	0	6	4	1	289.7	0.7503	Opt	0.27	0	5	5	0	307.7	0.7757	0	0.06206
1275	0	4	6	0	328.2	0.7809	Opt	2.384	0	4	6	0	328.2	0.7809	0.01	0
1276	0	5	5	5	320.2	0.7501	Opt	1.251	0	4	6	0	328.2	0.7691	0.01	0.02492
1277	0	7	3	0	266.8	0.755	Opt	0.271	0	7	3	0	266.8	0.755	0	0
1278	0	7	3	0	266.8	0.7539	Opt	0.27	0	6	4	0	287.3	0.7795	0.01	0.07672
1279	0	6	4	0	287.3	0.7558	Opt	0.281	0	6	4	0	287.3	0.7558	0	0
1280	0	6	4	0	287.3	0.7544	Opt	0.28	0	5	5	0	307.8	0.7753	0	0.07124
1281	0	10	0	0	205.1	0.7148	Opt	0.27	0	10	0	0	205.1	0.7148	0	0
1282	0	10	0	0	205.1	0.714	Opt	0.351	0	10	0	3	212.6	0.7017	0	0.03656
1283	0	8	2	0	246.1	0.7048	Opt	0.28	0	8	2	0	246.1	0.7048	0	0
1284	0	8	2	0	246.1	0.7059	Opt	0.301	0	7	3	0	266.6	0.7144	0	0.08327
1285	1	9	0	0	184.8	0.7276	Opt	0.27	1	9	0	0	184.8	0.7276	0	1.1E-05
1286	1	9	0	0	184.8	0.7231	Opt	0.27	1	9	0	0	184.8	0.7111	0	2.2E-05
1287	0	10	0	0	205.2	0.7378	Opt	0.291	0	10	0	0	205.2	0.7378	0.01	0
1288	0	10	0	0	205.2	0.7358	Opt	0.27	0	10	0	0	205.2	0.7242	0	9.7E-06
1289	0	7	3	0	266.8	0.7084	Opt	0.281	0	7	3	0	266.8	0.7084	0.01	0
1290	0	7	3	0	266.8	0.7088	Opt	0.27	0	7	3	1	269.3	0.7005	0.01	0.00938
1291	0	6	4	0	287.3	0.7106	Opt	0.281	0	6	4	0	287.3	0.7106	0	0
1292	0	6	4	0	287.3	0.7105	Opt	0.27	0	6	4	0	287.3	0.7016	0	3.5E-06
1293	0	8	2	0	246.3	0.7188	Opt	0.27	0	8	2	0	246.3	0.7188	0.01	0
1294	0	8	2	0	246.4	0.7182	Opt	0.281	0	8	2	0	246.4	0.7105	0	8.1E-06
1295	0	7	3	0	266.8	0.7222	Opt	0.31	0	7	3	0	266.8	0.7222	0.01	0
1296	0	7	3	0	266.9	0.7218	Opt	0.371	0	7	3	0	266.9	0.7144	0.01	3.7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1297	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1298	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1299	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1300	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1301	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1302	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1303	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1304	20	2	0.5	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1305	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1306	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1307	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1308	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1309	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1310	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1311	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1312	20	2	0.5	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1313	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1314	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1315	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1316	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1317	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1318	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1319	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1320	20	2	0.5	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1321	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1322	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1323	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1324	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1325	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1326	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1327	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1328	20	2	0.5	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1329	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1330	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1331	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1332	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1333	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1334	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1335	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1336	20	2	0.5	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1337	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1338	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1339	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1340	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1341	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1342	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1343	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1344	20	2	0.5	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1297	0	9	1	0	225.6	0.7515	Opt	0.28	0	9	1	0	225.6	0.7515	0	0
1298	0	9	1	1	228.1	0.7514	Opt	0.291	0	8	2	0	246.1	0.7577	0	0.07889
1299	0	6	4	0	287.1	0.7541	Opt	0.28	0	6	4	0	287.1	0.7541	0	0
1300	0	6	4	0	287.1	0.7539	Opt	0.28	0	5	5	0	307.6	0.7593	0	0.07139
1301	0	10	0	0	205.2	0.7911	Opt	0.281	0	10	0	0	205.2	0.7911	0	0
1302	0	10	0	0	205.2	0.7871	Opt	0.28	0	10	0	0	205.2	0.774	0	9.7E-06
1303	0	9	1	0	225.7	0.7631	Opt	0.271	0	9	1	0	225.7	0.7631	0	0
1304	0	9	1	0	225.7	0.7608	Opt	0.33	0	9	1	2	230.7	0.7507	0.01	0.02216
1305	0	6	4	0	287.2	0.7508	Opt	0.27	0	6	4	0	287.2	0.7508	0	0
1306	0	6	4	1	289.7	0.7503	Opt	0.281	0	5	5	0	307.7	0.7757	0.01	0.06209
1307	0	4	6	0	328.2	0.7809	Opt	2.974	0	4	6	0	328.2	0.7809	0.01	0
1308	0	5	5	5	320.3	0.7501	Opt	0.451	0	4	6	0	328.2	0.7691	0	0.02495
1309	0	7	3	0	266.8	0.755	Opt	0.27	0	7	3	0	266.8	0.755	0	0
1310	0	7	3	0	266.8	0.7539	Opt	0.271	0	6	4	0	287.3	0.7795	0.01	0.07677
1311	0	6	4	0	287.3	0.7558	Opt	0.28	0	6	4	0	287.3	0.7558	0.01	0
1312	0	6	4	0	287.3	0.7544	Opt	0.27	0	5	5	0	307.8	0.7753	0	0.0713
1313	0	10	0	0	205.2	0.7148	Opt	0.281	0	10	0	0	205.2	0.7148	0.01	0
1314	0	10	0	0	205.2	0.714	Opt	0.32	0	10	0	3	212.7	0.7017	0	0.03656
1315	0	8	2	0	246.2	0.7048	Opt	0.281	0	8	2	0	246.2	0.7048	0	0
1316	0	8	2	0	246.2	0.7059	Opt	0.3	0	7	3	0	266.7	0.7144	0.01	0.08325
1317	1	9	0	0	185	0.7276	Opt	0.28	1	9	0	0	185	0.7276	0	2.2E-05
1318	1	9	0	0	185	0.7231	Opt	0.281	1	9	0	0	185	0.7111	0	3.8E-05
1319	0	10	0	0	205.3	0.7378	Opt	0.3	0	10	0	0	205.3	0.7378	0	0
1320	0	10	0	0	205.3	0.7358	Opt	0.291	0	10	0	0	205.3	0.7242	0	1.5E-05
1321	0	7	3	0	266.8	0.7084	Opt	0.29	0	7	3	0	266.8	0.7084	0	0
1322	0	7	3	0	266.8	0.7088	Opt	0.271	0	7	3	1	269.3	0.7005	0.01	0.00938
1323	0	6	4	0	287.3	0.7106	Opt	0.28	0	6	4	0	287.3	0.7106	0.01	0
1324	0	6	4	0	287.3	0.7105	Opt	0.28	0	6	4	0	287.3	0.7016	0	7E-06
1325	0	8	2	0	246.4	0.7188	Opt	0.281	0	8	2	0	246.4	0.7188	0.01	0
1326	0	8	2	0	246.5	0.7182	Opt	0.29	0	8	2	0	246.5	0.7105	0	1.6E-05
1327	0	7	3	0	266.9	0.7222	Opt	0.321	0	7	3	0	266.9	0.7222	0	0
1328	0	7	3	0	266.9	0.7218	Opt	0.29	0	7	3	0	267	0.7144	0	1.5E-05
1329	0	9	1	0	225.6	0.7515	Opt	0.271	0	9	1	0	225.6	0.7515	0.01	0
1330	0	9	1	1	228.2	0.7514	Opt	0.29	0	8	2	0	246.2	0.7577	0.01	0.07887
1331	0	6	4	0	287.1	0.7541	Opt	0.28	0	6	4	0	287.1	0.7541	0	0
1332	0	6	4	0	287.2	0.7539	Opt	0.281	0	5	5	0	307.7	0.7593	0	0.07138
1333	0	10	0	0	205.2	0.7911	Opt	0.28	0	10	0	0	205.2	0.7911	0.01	0
1334	0	10	0	0	205.3	0.7871	Opt	0.281	0	10	0	0	205.3	0.774	0	1.9E-05
1335	0	9	1	0	225.8	0.7631	Opt	0.28	0	9	1	0	225.8	0.7631	0.01	0
1336	0	9	1	0	225.8	0.7608	Opt	0.33	0	9	1	2	230.8	0.7507	0	0.02215
1337	0	6	4	0	287.3	0.7508	Opt	0.281	0	6	4	0	287.3	0.7508	0	0
1338	0	6	4	1	289.8	0.7503	Opt	0.29	0	5	5	0	307.8	0.7757	0.01	0.06205
1339	0	4	6	0	328.3	0.7809	Opt	2.384	0	4	6	0	328.3	0.7809	0	0
1340	0	5	5	5	320.3	0.7501	Opt	0.44	0	4	6	0	328.3	0.7691	0.01	0.02493
1341	0	7	3	0	266.9	0.755	Opt	0.281	0	7	3	0	266.9	0.755	0	0
1342	0	7	3	0	266.9	0.7539	Opt	0.28	0	6	4	0	287.4	0.7795	0	0.07671
1343	0	6	4	0	287.4	0.7558	Opt	0.291	0	6	4	0	287.4	0.7558	0	0
1344	0	6	4	0	287.4	0.7544	Opt	0.28	0	5	5	0	307.9	0.7753	0.01	0.07123

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1345	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1346	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1347	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1348	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1349	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1350	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1351	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1352	20	2	1	0.05	0.075	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1353	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1354	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1355	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1356	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1357	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1358	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1359	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1360	20	2	1	0.05	0.075	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1361	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1362	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1363	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1364	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1365	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1366	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1367	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1368	20	2	1	0.05	0.075	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1369	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1370	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1371	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1372	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1373	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1374	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1375	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1376	20	2	1	0.05	0.075	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1377	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1378	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1379	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1380	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1381	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1382	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1383	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1384	20	2	1	0.05	0.075	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1385	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1386	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1387	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1388	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1389	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1390	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1391	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1392	20	2	1	0.05	0.075	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1345	0	10	0	0	210.1	0.7148	Opt	0.28	0	10	0	0	210.1	0.7148	0	0
1346	0	10	0	0	210.1	0.714	Opt	0.331	0	10	0	3	219.1	0.7017	0	0.04285
1347	0	8	2	0	252.1	0.7048	Opt	0.28	0	8	2	0	252.1	0.7048	0.01	0
1348	0	8	2	0	252.1	0.7059	Opt	0.301	0	7	3	0	273.1	0.7144	0	0.08329
1349	1	9	0	0	189.2	0.7276	Opt	0.28	1	9	0	0	189.2	0.7276	0	1.1E-05
1350	1	9	0	0	189.2	0.7231	Opt	0.271	1	9	0	0	189.2	0.7111	0.01	1.6E-05
1351	0	10	0	0	210.1	0.7378	Opt	0.3	0	10	0	0	210.1	0.7378	0.01	0
1352	0	10	0	0	210.1	0.7358	Opt	0.28	0	10	0	0	210.1	0.7242	0	9.5E-06
1353	0	7	3	0	273.1	0.7084	Opt	0.291	0	7	3	0	273.1	0.7084	0.01	0
1354	0	7	3	0	273.2	0.7088	Opt	0.3	0	7	3	1	276.2	0.7005	0	0.01098
1355	0	6	4	0	294.2	0.7106	Opt	0.281	0	6	4	0	294.2	0.7106	0	0
1356	0	6	4	0	294.2	0.7105	Opt	0.31	0	6	4	0	294.2	0.7016	0.01	3.4E-06
1357	0	8	2	0	252.2	0.7188	Opt	0.281	0	8	2	0	252.2	0.7188	0	0
1358	0	8	2	0	252.2	0.7159	Opt	0.3	0	8	2	0	252.2	0.7105	0.01	1.2E-05
1359	0	7	3	0	273.2	0.7222	Opt	0.32	0	7	3	0	273.2	0.7222	0	0
1360	0	7	3	0	273.2	0.7218	Opt	0.311	0	7	3	0	273.2	0.7144	0	7.3E-06
1361	0	9	1	0	231.1	0.7515	Opt	0.28	0	9	1	0	231.1	0.7515	0	0
1362	0	9	1	1	234.1	0.7514	Opt	0.301	0	8	2	0	252.1	0.7577	0.01	0.07689
1363	0	6	4	0	294.1	0.7541	Opt	0.28	0	6	4	0	294.1	0.7541	0	0
1364	0	6	4	0	294.1	0.7539	Opt	0.291	0	5	5	0	315.1	0.7593	0	0.0714
1365	0	10	0	0	210.1	0.7911	Opt	0.3	0	10	0	0	210.1	0.7911	0	0
1366	0	10	0	0	210.1	0.7871	Opt	0.29	0	10	0	0	210.1	0.774	0	9.5E-06
1367	0	9	1	0	231.1	0.7631	Opt	0.291	0	9	1	0	231.1	0.7631	0	0
1368	0	9	1	0	231.1	0.7608	Opt	0.31	0	9	1	2	237.1	0.7507	0	0.02596
1369	0	6	4	0	294.1	0.7508	Opt	0.281	0	6	4	0	294.1	0.7508	0.01	0
1370	0	6	4	1	297.1	0.7503	Opt	0.3	0	5	5	0	315.1	0.7757	0	0.06055
1371	0	4	6	0	336.1	0.7809	Opt	0.551	0	4	6	0	336.1	0.7809	0	0
1372	0	5	5	5	330.1	0.7501	Opt	0.471	0	4	6	0	336.1	0.7691	0.01	0.01815
1373	0	7	3	0	273.2	0.755	Opt	0.29	0	7	3	0	273.2	0.755	0.01	0
1374	0	7	3	0	273.2	0.7539	Opt	0.29	0	6	4	0	294.2	0.7795	0	0.07682
1375	0	6	4	0	294.2	0.7558	Opt	0.291	0	6	4	0	294.2	0.7558	0	0
1376	0	6	4	0	294.2	0.7544	Opt	0.29	0	5	5	0	315.2	0.7753	0.01	0.07133
1377	0	10	0	0	210.1	0.7148	Opt	0.281	0	10	0	0	210.1	0.7148	0	0
1378	0	10	0	0	210.1	0.714	Opt	0.33	0	10	0	3	219.1	0.7017	0.01	0.04284
1379	0	8	2	0	252.1	0.7048	Opt	0.291	0	8	2	0	252.1	0.7048	0	0
1380	0	8	2	0	252.1	0.7059	Opt	0.29	0	7	3	0	273.1	0.7144	0	0.08327
1381	1	9	0	0	189.4	0.7276	Opt	0.28	1	9	0	0	189.4	0.7276	0.01	2.1E-05
1382	1	9	0	0	189.4	0.7231	Opt	0.291	1	9	0	0	189.4	0.7111	0	3.7E-05
1383	0	10	0	0	210.2	0.7378	Opt	0.3	0	10	0	0	210.2	0.7378	0.01	0
1384	0	10	0	0	210.2	0.7358	Opt	0.301	0	10	0	0	210.2	0.7242	0	1.4E-05
1385	0	7	3	0	273.2	0.7084	Opt	0.3	0	7	3	0	273.2	0.7084	0	0
1386	0	7	3	0	273.2	0.7088	Opt	0.301	0	7	3	1	276.2	0.7005	0	0.01099
1387	0	6	4	0	294.2	0.7106	Opt	0.29	0	6	4	0	294.2	0.7106	0	0
1388	0	6	4	0	294.2	0.7105	Opt	0.3	0	6	4	0	294.2	0.7016	0	6.8E-06
1389	0	8	2	0	252.3	0.7188	Opt	0.291	0	8	2	0	252.3	0.7188	0	0
1390	0	8	2	0	252.3	0.7182	Opt	0.29	0	8	2	0	252.3	0.7105	0	1.6E-05
1391	0	7	3	0	273.3	0.7222	Opt	0.301	0	7	3	0	273.3	0.7222	0.01	0
1392	0	7	3	0	273.3	0.7218	Opt	0.31	0	7	3	0	273.3	0.7144	0	1.5E-05

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1393	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1394	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1395	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1396	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1397	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1398	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1399	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1400	20	2	1	0.05	0.075	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1401	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1402	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1403	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1404	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1405	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1406	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1407	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1408	20	2	1	0.05	0.075	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1409	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1410	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1411	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1412	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1413	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1414	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1415	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1416	20	2	1	0.05	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1417	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1418	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1419	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1420	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1421	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1422	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1423	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1424	20	2	1	0.05	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1425	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1426	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1427	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1428	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1429	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1430	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1431	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1432	20	2	1	0.05	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1433	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1434	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1435	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1436	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1437	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1438	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1439	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1440	20	2	1	0.05	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1393	0	9	1	0	231.1	0.7515	Opt	0.281	0	9	1	0	231.1	0.7515	0.01	0
1394	0	9	1	1	234.1	0.7514	Opt	0.3	0	8	2	0	252.1	0.7577	0.01	0.07687
1395	0	6	4	0	294.1	0.7541	Opt	0.29	0	6	4	0	294.1	0.7541	0	0
1396	0	6	4	0	294.1	0.7539	Opt	0.291	0	5	5	0	315.1	0.7593	0	0.0714
1397	0	10	0	0	210.2	0.7911	Opt	0.3	0	10	0	0	210.2	0.7911	0.01	0
1398	0	10	0	0	210.2	0.7871	Opt	0.281	0	10	0	0	210.2	0.774	0.01	1.9E-05
1399	0	9	1	0	231.2	0.7631	Opt	0.28	0	9	1	0	231.2	0.7631	0.01	0
1400	0	9	1	0	231.2	0.7608	Opt	0.321	0	9	1	2	237.2	0.7507	0.01	0.02597
1401	0	6	4	0	294.2	0.7508	Opt	0.29	0	6	4	0	294.2	0.7508	0	0
1402	0	6	4	1	297.2	0.7503	Opt	0.301	0	5	5	0	315.2	0.7757	0	0.06051
1403	0	4	6	0	336.2	0.7809	Opt	7.05	0	4	6	0	336.2	0.7809	0	0
1404	0	5	5	5	330.2	0.75	Opt	2.003	0	4	6	0	336.2	0.7691	0.01	0.01813
1405	0	7	3	0	273.3	0.755	Opt	0.29	0	7	3	0	273.3	0.755	0	0
1406	0	7	3	0	273.3	0.7539	Opt	0.29	0	6	4	0	294.3	0.7795	0.01	0.07675
1407	0	6	4	0	294.3	0.7558	Opt	0.291	0	6	4	0	294.3	0.7558	0	0
1408	0	6	4	0	294.3	0.7544	Opt	0.29	0	5	5	0	315.3	0.7753	0.01	0.07127
1409	0	10	0	0	210.1	0.7148	Opt	0.291	0	10	0	0	210.1	0.7148	0.01	0
1410	0	10	0	0	210.1	0.714	Opt	0.33	0	10	0	3	219.1	0.7017	0	0.04284
1411	0	8	2	0	252.1	0.7048	Opt	0.291	0	8	2	0	252.1	0.7048	0	0
1412	0	8	2	0	252.1	0.7059	Opt	0.29	0	7	3	0	273.1	0.7144	0.01	0.08328
1413	1	9	0	0	189.2	0.7276	Opt	0.29	1	9	0	0	189.2	0.7276	0	1.1E-05
1414	1	9	0	0	189.3	0.7231	Opt	0.291	1	9	0	0	189.3	0.7111	0	1.6E-05
1415	0	10	0	0	210.2	0.7378	Opt	0.29	0	10	0	0	210.2	0.7378	0.01	0
1416	0	10	0	0	210.2	0.7358	Opt	0.301	0	10	0	0	210.2	0.7242	0	9.5E-06
1417	0	7	3	0	273.2	0.7084	Opt	0.31	0	7	3	0	273.2	0.7084	0	0
1418	0	7	3	0	273.2	0.7088	Opt	0.311	0	7	3	1	276.2	0.7005	0	0.01098
1419	0	6	4	0	294.2	0.7106	Opt	0.31	0	6	4	0	294.2	0.7106	0	0
1420	0	6	4	0	294.2	0.7105	Opt	0.31	0	6	4	0	294.2	0.7016	0	3.4E-06
1421	0	8	2	0	252.3	0.7188	Opt	0.301	0	8	2	0	252.3	0.7188	0	0
1422	0	8	2	0	252.3	0.7182	Opt	0.3	0	8	2	0	252.3	0.7105	0	7.9E-06
1423	0	7	3	0	273.3	0.7222	Opt	0.321	0	7	3	0	273.3	0.7222	0.01	0
1424	0	7	3	0	273.3	0.7218	Opt	0.37	0	7	3	0	273.3	0.7144	0.01	7.3E-06
1425	0	9	1	0	231.1	0.7515	Opt	0.291	0	9	1	0	231.1	0.7515	0.01	0
1426	0	9	1	1	234.1	0.7514	Opt	0.31	0	8	2	0	252.1	0.7577	0	0.07687
1427	0	6	4	0	294.1	0.7541	Opt	0.291	0	6	4	0	294.1	0.7541	0	0
1428	0	6	4	0	294.1	0.7539	Opt	0.3	0	5	5	0	315.1	0.7593	0	0.07139
1429	0	10	0	0	210.1	0.7911	Opt	0.291	0	10	0	0	210.1	0.7911	0	0
1430	0	10	0	0	210.2	0.7871	Opt	0.29	0	10	0	0	210.2	0.774	0.01	4.8E-06
1431	0	9	1	0	231.2	0.7631	Opt	0.29	0	9	1	0	231.2	0.7631	0.01	0
1432	0	9	1	0	231.2	0.7608	Opt	0.321	0	9	1	2	237.2	0.7507	0	0.02596
1433	0	6	4	0	294.2	0.7508	Opt	0.29	0	6	4	0	294.2	0.7508	0	0
1434	0	6	4	1	297.2	0.7503	Opt	0.301	0	5	5	0	315.2	0.7757	0.01	0.06052
1435	0	4	6	0	336.2	0.7809	Opt	1.482	0	4	6	0	336.2	0.7809	0.01	0
1436	0	5	5	5	330.2	0.7501	Opt	0.881	0	4	6	0	336.2	0.7691	0	0.01814
1437	0	7	3	0	273.2	0.755	Opt	0.301	0	7	3	0	273.2	0.755	0	0
1438	0	7	3	0	273.2	0.7539	Opt	0.29	0	6	4	0	294.2	0.7795	0.01	0.07679
1439	0	6	4	0	294.2	0.7558	Opt	0.3	0	6	4	0	294.2	0.7558	0	0
1440	0	6	4	0	294.2	0.7544	Opt	0.301	0	5	5	0	315.2	0.7753	0	0.07131

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1441	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1442	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1443	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1444	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1445	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1446	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1447	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1448	20	2	1	0.05	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1449	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1450	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1451	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1452	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1453	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1454	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1455	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1456	20	2	1	0.05	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1457	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1458	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1459	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1460	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1461	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1462	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1463	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1464	20	2	1	0.05	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1465	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1466	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1467	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1468	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1469	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1470	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1471	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1472	20	2	1	0.05	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1473	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1474	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1475	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1476	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1477	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1478	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1479	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1480	20	2	1	0.1	0.15	1	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1481	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1482	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1483	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1484	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1485	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1486	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1487	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1488	20	2	1	0.1	0.15	1	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]



	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1441	0	10	0	0	210.1	0.7148	Opt	0.3	0	10	0	0	210.1	0.7148	0	0
1442	0	10	0	0	210.1	0.714	Opt	0.341	0	10	0	3	219.1	0.7017	0	0.04284
1443	0	8	2	0	252.1	0.7048	Opt	0.3	0	8	2	0	252.1	0.7048	0	0
1444	0	8	2	0	252.1	0.7059	Opt	0.301	0	7	3	0	273.1	0.7144	0	0.08326
1445	1	9	0	0	189.4	0.7276	Opt	0.29	1	9	0	0	189.4	0.7276	0.01	2.1E-05
1446	1	9	0	0	189.4	0.7231	Opt	0.301	1	9	0	0	189.4	0.7111	0	3.7E-05
1447	0	10	0	0	210.2	0.7378	Opt	0.3	0	10	0	0	210.2	0.7378	0	0
1448	0	10	0	0	210.2	0.7358	Opt	0.3	0	10	0	0	210.2	0.7242	0	1.4E-05
1449	0	7	3	0	273.2	0.7084	Opt	0.301	0	7	3	0	273.2	0.7084	0.01	0
1450	0	7	3	0	273.2	0.7088	Opt	0.3	0	7	3	1	276.2	0.7005	0	0.01099
1451	0	6	4	0	294.2	0.7106	Opt	0.291	0	6	4	0	294.2	0.7106	0.01	0
1452	0	6	4	0	294.2	0.7105	Opt	0.32	0	6	4	0	294.2	0.7016	0.01	1E-05
1453	0	8	2	0	252.4	0.7188	Opt	0.291	0	8	2	0	252.4	0.7188	0	0
1454	0	8	2	0	252.4	0.7182	Opt	0.31	0	8	2	0	252.4	0.7105	0.01	1.6E-05
1455	0	7	3	0	273.3	0.7222	Opt	0.31	0	7	3	0	273.3	0.7222	0	0
1456	0	7	3	0	273.4	0.7218	Opt	0.331	0	7	3	0	273.4	0.7144	0	1.1E-05
1457	0	9	1	0	231.1	0.7515	Opt	0.29	0	9	1	0	231.1	0.7515	0.01	0
1458	0	9	1	1	234.1	0.7514	Opt	0.311	0	8	2	0	252.1	0.7577	0.01	0.07685
1459	0	6	4	0	294.1	0.7541	Opt	0.3	0	6	4	0	294.1	0.7541	0	0
1460	0	6	4	0	294.1	0.7539	Opt	0.301	0	5	5	0	315.1	0.7593	0	0.07139
1461	0	10	0	0	210.2	0.7911	Opt	0.3	0	10	0	0	210.2	0.7911	0	0
1462	0	10	0	0	210.2	0.7871	Opt	0.301	0	10	0	0	210.2	0.774	0.01	1.4E-05
1463	0	9	1	0	231.2	0.7631	Opt	0.3	0	9	1	0	231.2	0.7631	0	0
1464	0	9	1	0	231.2	0.7608	Opt	0.33	0	9	1	2	237.2	0.7507	0	0.02596
1465	0	6	4	0	294.2	0.7508	Opt	0.301	0	6	4	0	294.2	0.7508	0	0
1466	0	6	4	1	297.2	0.7503	Opt	0.31	0	5	5	0	315.2	0.7757	0	0.06049
1467	0	4	6	0	336.2	0.7809	Opt	0.511	0	4	6	0	336.2	0.7809	0.01	0
1468	0	5	5	5	330.2	0.7501	Opt	0.541	0	4	6	0	336.2	0.7691	0	0.01811
1469	0	7	3	0	273.3	0.755	Opt	0.3	0	7	3	0	273.3	0.755	0.01	0
1470	0	7	3	0	273.3	0.7539	Opt	0.301	0	6	4	0	294.3	0.7795	0	0.07672
1471	0	6	4	0	294.3	0.7558	Opt	0.3	0	6	4	0	294.3	0.7558	0	0
1472	0	6	4	0	294.3	0.7544	Opt	0.301	0	5	5	0	315.3	0.7753	0.01	0.07125
1473	0	10	0	0	210.1	0.7148	Opt	0.3	0	10	0	0	210.1	0.7148	0	0
1474	0	10	0	0	210.1	0.714	Opt	0.361	0	10	0	3	219.1	0.7017	0	0.04283
1475	0	8	2	0	252.1	0.7048	Opt	0.3	0	8	2	0	252.1	0.7048	0	0
1476	0	8	2	0	252.1	0.7059	Opt	0.31	0	7	3	0	273.1	0.7144	0	0.08327
1477	1	9	0	0	189.3	0.7276	Opt	0.301	1	9	0	0	189.3	0.7276	0	1.1E-05
1478	1	9	0	0	189.3	0.7231	Opt	0.3	1	9	0	0	189.3	0.7111	0.01	2.1E-05
1479	0	10	0	0	210.2	0.7378	Opt	0.311	0	10	0	0	210.2	0.7378	0	0
1480	0	10	0	0	210.2	0.7358	Opt	0.3	0	10	0	0	210.2	0.7242	0	9.5E-06
1481	0	7	3	0	273.3	0.7084	Opt	0.311	0	7	3	0	273.3	0.7084	0.01	0
1482	0	7	3	0	273.3	0.7088	Opt	0.32	0	7	3	1	276.3	0.7005	0	0.01098
1483	0	6	4	0	294.3	0.7106	Opt	0.311	0	6	4	0	294.3	0.7106	0	0
1484	0	6	4	0	294.3	0.7105	Opt	0.33	0	6	4	0	294.3	0.7016	0	3.4E-06
1485	0	8	2	0	252.3	0.7188	Opt	0.301	0	8	2	0	252.3	0.7188	0	0
1486	0	8	2	0	252.4	0.7159	Opt	0.32	0	8	2	0	252.4	0.7105	0	7.9E-06
1487	0	7	3	0	273.3	0.7222	Opt	0.33	0	7	3	0	273.3	0.7222	0.01	0
1488	0	7	3	0	273.4	0.7218	Opt	0.331	0	7	3	0	273.4	0.7144	0.01	3.7E-06

	Input Parameters										
Exp #	$f$	$\hat{f}$	$h$	$c^{in}$	$c^{out}$	$c^e$	$\alpha$	$d_1, d_2$	$d_0$	$d_{-1}$	$\hat{d}$
1489	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1490	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1491	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1492	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1493	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1494	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1495	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1496	20	2	1	0.1	0.15	1	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1497	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1498	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1499	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1500	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1501	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1502	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1503	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1504	20	2	1	0.1	0.15	1	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1505	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1506	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1507	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1508	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1509	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1510	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1511	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1512	20	2	1	0.1	0.15	2	0.7	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1513	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1514	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1515	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1516	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1517	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1518	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1519	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1520	20	2	1	0.1	0.15	2	0.7	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1521	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0,0.001]
1522	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0,0.01]	[0.001,0.002]
1523	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0,0.001]
1524	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1525	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0,0.001]
1526	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1527	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1528	20	2	1	0.1	0.15	2	0.75	[0,0.05]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]
1529	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0,0.001]
1530	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0,0.01]	[0.001,0.002]
1531	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0,0.001]
1532	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0,0.05]	[0.01,0.02]	[0.001,0.002]
1533	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0,0.001]
1534	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0,0.01]	[0.001,0.002]
1535	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0,0.001]
1536	20	2	1	0.1	0.15	2	0.75	[0.05,0.1]	[0.05,0.1]	[0.01,0.02]	[0.001,0.002]

	Output															
Exp #	Opt (0,0)	Opt (1,0)	Opt (1,1)	Opt # ded	Opt cost	Opt service	Opt status	Opt solTime	H (0,0)	H (1,0)	H (1,1)	H # ded	H cost	H service	H solTime	H-Opt Gap
1489	0	9	1	0	231.1	0.7515	Opt	0.3	0	9	1	0	231.1	0.7515	0	0
1490	0	9	1	1	234.1	0.7514	Opt	0.311	0	8	2	0	252.1	0.7577	0.01	0.07687
1491	0	6	4	0	294.1	0.7541	Opt	0.3	0	6	4	0	294.1	0.7541	0	0
1492	0	6	4	0	294.1	0.7539	Opt	0.301	0	5	5	0	315.1	0.7593	0.01	0.07139
1493	0	10	0	0	210.2	0.7911	Opt	0.31	0	10	0	0	210.2	0.7911	0	0
1494	0	10	0	0	210.2	0.7871	Opt	0.301	0	10	0	0	210.2	0.774	0.01	9.5E-06
1495	0	9	1	0	231.2	0.7631	Opt	0.31	0	9	1	0	231.2	0.7631	0	0
1496	0	9	1	0	231.2	0.7608	Opt	0.331	0	9	1	2	237.2	0.7507	0	0.02595
1497	0	6	4	0	294.2	0.7508	Opt	0.3	0	6	4	0	294.2	0.7508	0.01	0
1498	0	6	4	1	297.2	0.7503	Opt	0.32	0	5	5	0	315.2	0.7757	0.01	0.06053
1499	0	4	6	0	336.2	0.7809	Opt	0.581	0	4	6	0	336.2	0.7809	0	0
1500	0	5	5	5	330.3	0.7501	Opt	0.501	0	4	6	0	336.2	0.7691	0.01	0.01814
1501	0	7	3	0	273.3	0.755	Opt	0.31	0	7	3	0	273.3	0.755	0	0
1502	0	7	3	0	273.3	0.7539	Opt	0.3	0	6	4	0	294.3	0.7795	0.011	0.07678
1503	0	6	4	0	294.3	0.7558	Opt	0.31	0	6	4	0	294.3	0.7558	0.01	0
1504	0	6	4	0	294.3	0.7544	Opt	0.311	0	5	5	0	315.3	0.7753	0	0.0713
1505	0	10	0	0	210.2	0.7148	Opt	0.3	0	10	0	0	210.2	0.7148	0	0
1506	0	10	0	0	210.2	0.714	Opt	0.361	0	10	0	3	219.2	0.7017	0.01	0.04283
1507	0	8	2	0	252.2	0.7048	Opt	0.3	0	8	2	0	252.2	0.7048	0.01	0
1508	0	8	2	0	252.2	0.7059	Opt	0.321	0	7	3	0	273.2	0.7144	0	0.08325
1509	1	9	0	0	189.5	0.7276	Opt	0.31	1	9	0	0	189.5	0.7276	0	2.1E-05
1510	1	9	0	0	189.5	0.7231	Opt	0.311	1	9	0	0	189.5	0.7111	0	3.7E-05
1511	0	10	0	0	210.3	0.7378	Opt	0.32	0	10	0	0	210.3	0.7378	0	0
1512	0	10	0	0	210.3	0.7358	Opt	0.311	0	10	0	0	210.3	0.7242	0	1.4E-05
1513	0	7	3	0	273.3	0.7084	Opt	0.31	0	7	3	0	273.3	0.7084	0.01	0
1514	0	7	3	0	273.3	0.7088	Opt	0.32	0	7	3	1	276.3	0.7005	0.01	0.01098
1515	0	6	4	0	294.3	0.7106	Opt	0.311	0	6	4	0	294.3	0.7106	0	0
1516	0	6	4	0	294.3	0.7105	Opt	0.33	0	6	4	0	294.3	0.7016	0	6.8E-06
1517	0	8	2	0	252.4	0.7188	Opt	0.311	0	8	2	0	252.4	0.7188	0	0
1518	0	8	2	0	252.5	0.7182	Opt	0.32	0	8	2	0	252.5	0.7105	0	1.6E-05
1519	0	7	3	0	273.4	0.7222	Opt	0.321	0	7	3	0	273.4	0.7222	0	0
1520	0	7	3	0	273.4	0.7218	Opt	0.33	0	7	3	0	273.5	0.7144	0	1.5E-05
1521	0	9	1	0	231.1	0.7515	Opt	0.301	0	9	1	0	231.1	0.7515	0.01	0
1522	0	9	1	1	234.2	0.7514	Opt	0.32	0	8	2	0	252.2	0.7577	0.01	0.07685
1523	0	6	4	0	294.1	0.7541	Opt	0.301	0	6	4	0	294.1	0.7541	0	0
1524	0	6	4	0	294.2	0.7539	Opt	0.3	0	5	5	0	315.2	0.7593	0.01	0.07138
1525	0	10	0	0	210.2	0.7911	Opt	0.32	0	10	0	0	210.2	0.7911	0.01	0
1526	0	10	0	0	210.3	0.7871	Opt	0.311	0	10	0	0	210.3	0.774	0	1.9E-05
1527	0	9	1	0	231.3	0.7631	Opt	0.3	0	9	1	0	231.3	0.7631	0.01	0
1528	0	9	1	0	231.3	0.7608	Opt	0.331	0	9	1	2	237.3	0.7507	0.01	0.02595
1529	0	6	4	0	294.3	0.7508	Opt	0.3	0	6	4	0	294.3	0.7508	0	0
1530	0	6	4	1	297.3	0.7503	Opt	0.321	0	5	5	0	315.3	0.7757	0.01	0.06049
1531	0	4	6	0	336.3	0.7809	Opt	7.26	0	4	6	0	336.3	0.7809	0	0
1532	0	5	5	5	330.3	0.7501	Opt	0.541	0	4	6	0	336.3	0.7691	0.01	0.01812
1533	0	7	3	0	273.4	0.755	Opt	0.31	0	7	3	0	273.4	0.755	0	0
1534	0	7	3	0	273.4	0.7539	Opt	0.311	0	6	4	0	294.4	0.7795	0	0.07671
1535	0	6	4	0	294.4	0.7558	Opt	0.31	0	6	4	0	294.4	0.7558	0	0
1536	0	6	4	0	294.4	0.7544	Opt	0.311	0	5	5	0	315.4	0.7753	0.01	0.07124

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